

Accelerated Integral Equation Methods for the Comprehensive Electromagnetic Analysis of MRI Systems

Jorge Fernandez Villena

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www.rle.mit.edu/cpg

♦ pTx project consortium



Wald Group @ Martinos Center

Larry Wald

Bastien Guerin



MRI group @ RLE, MIT

Elfar Adalsteinsson

Filiz Yetisir



MIT+Madrid initiative

Yigitcan Eryaman

Joaquin Herraiz

Emanuele Schiavi

Adrian Martin



Siemens Group @ Erlangen

Michael Hamm

CPG @ RLE, MIT

Jacob White

Luca Daniel

Thanos Polimeridis

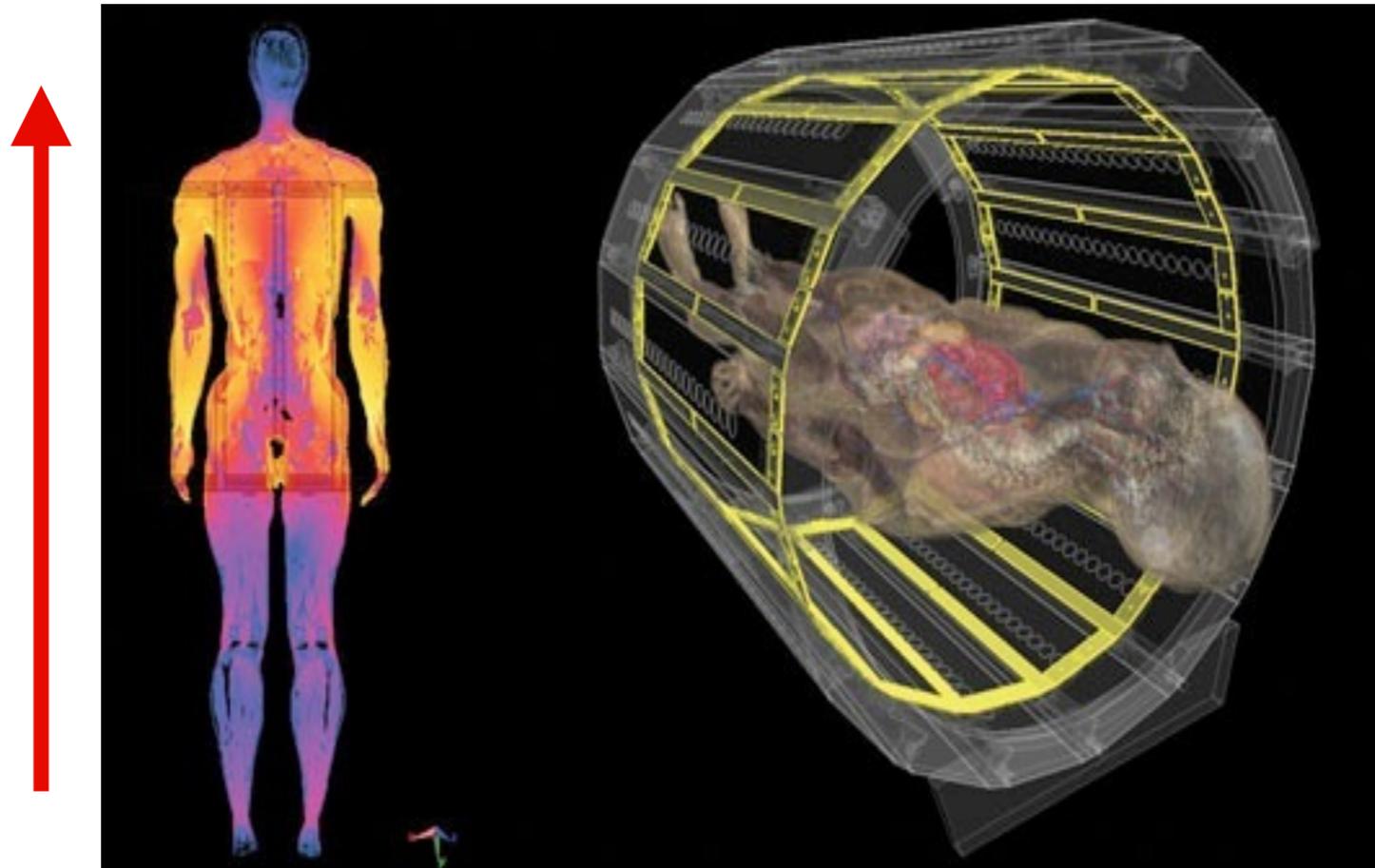
Zohaib Mahmood

Amit Hochman

Jorge Fernández Villena

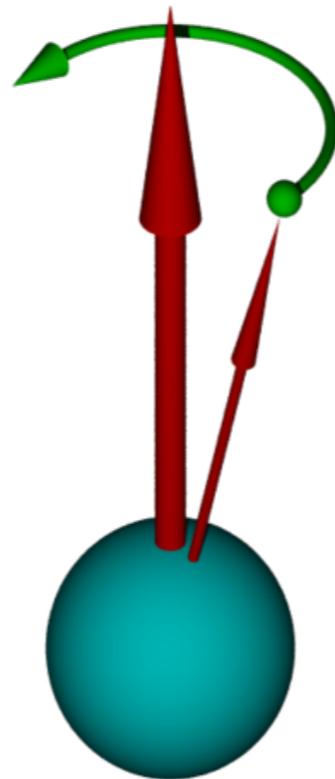
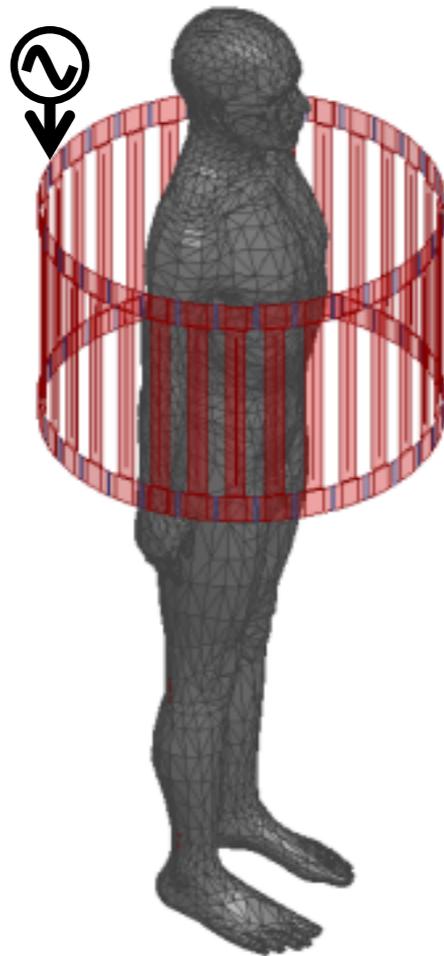
Magnetic Resonance Imaging

- ◆ **External large coils generate main uniform B field**
 - ◆ align protons in the direction of the scan
 - ◆ protons spinning at Larmor frequency
 - ◆ multiple of the main field strength



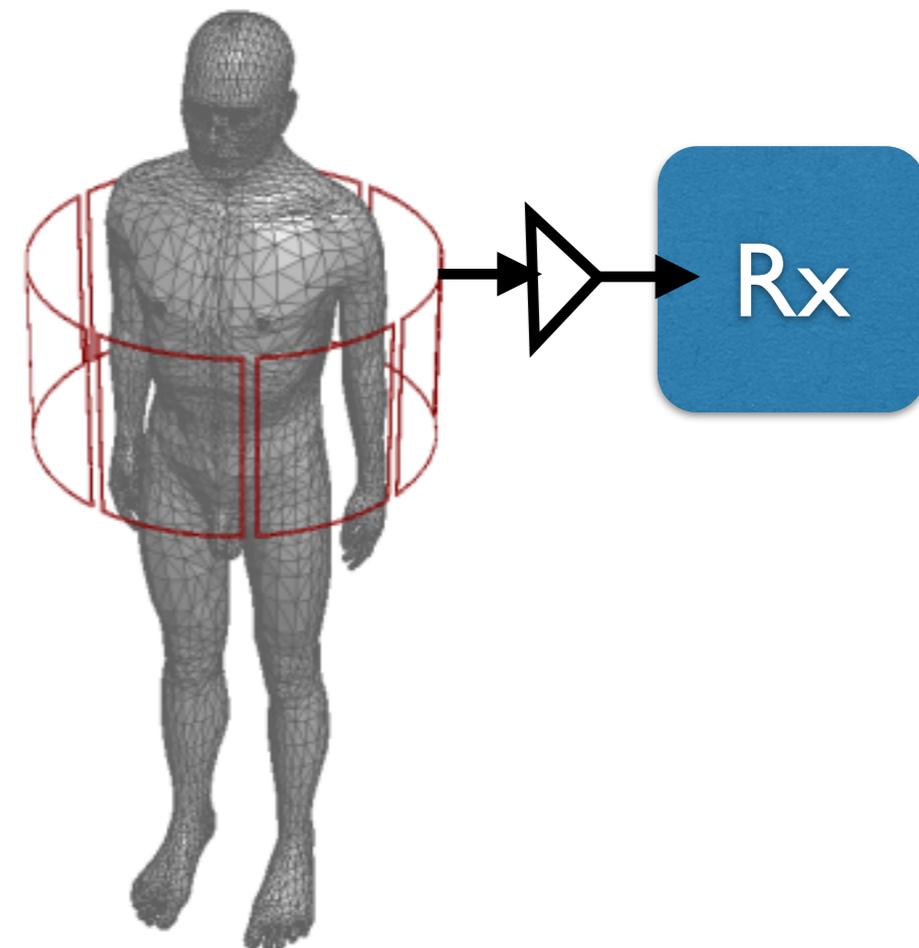
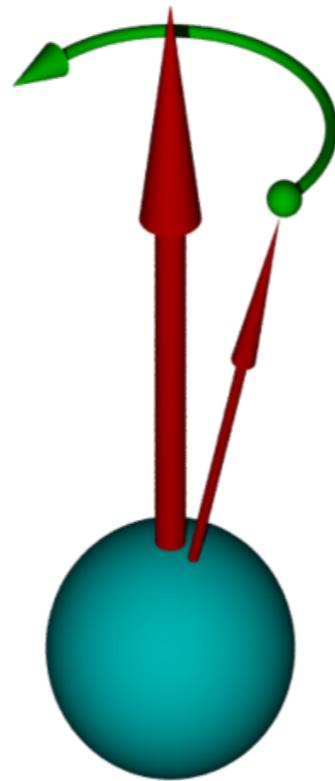
- ◆ **RF transmit (Tx) coil**

- ◆ applies a short RF signal at the Larmor frequency
- ◆ perturbs (tilts) the alignment of the spinning



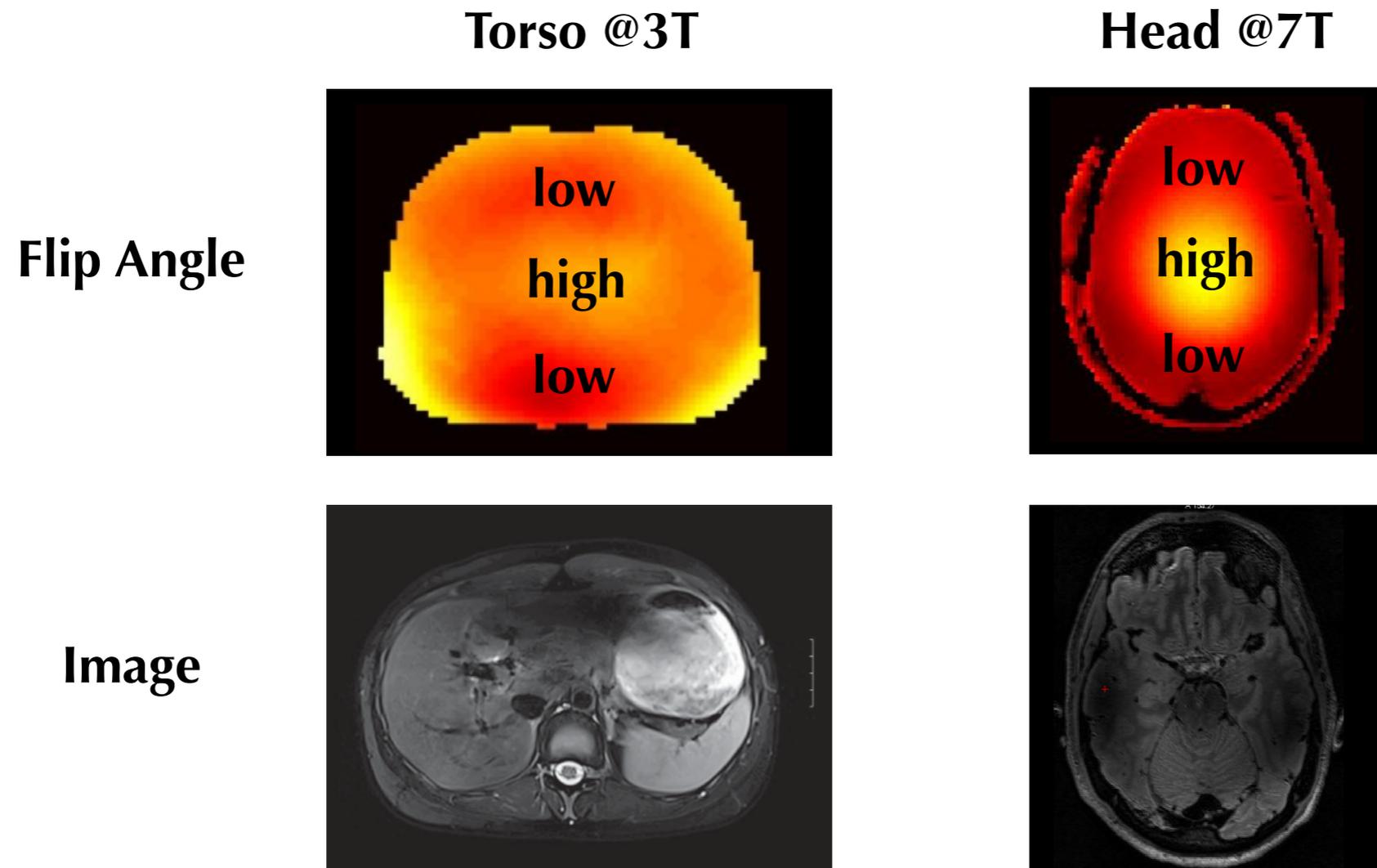
- ◆ **RF receiving (Rx) coils**

- ◆ protons return to original magnetization alignment
- ◆ generate small flux changes
 - ◆ voltage change in receiving (Rx) coils: signal to be processed
- ◆ time to return depends on time constants
 - ◆ related to tissue properties
 - ◆ contrast in the image



Parallel Transmission

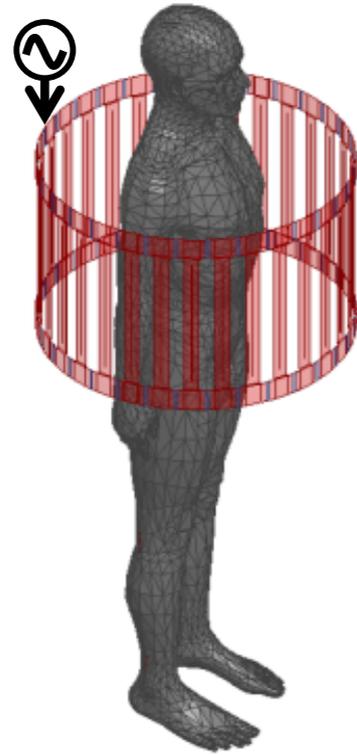
- ◆ As we move into high field (higher frequency) scanners



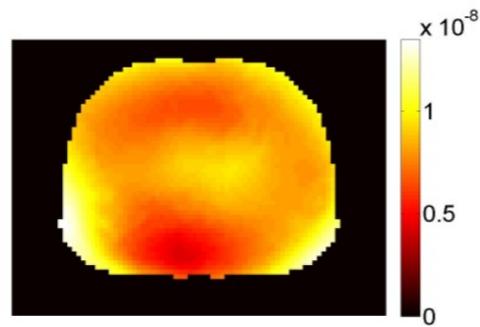
Inhomogeneities affect image quality

◆ Move from single channel

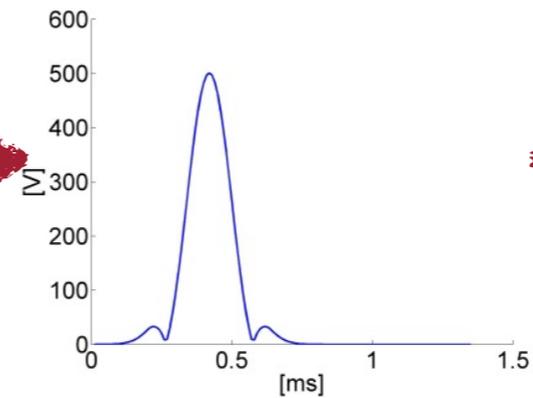
1 channel



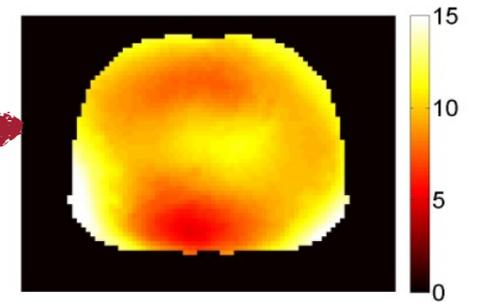
EM map / ch



pulse design

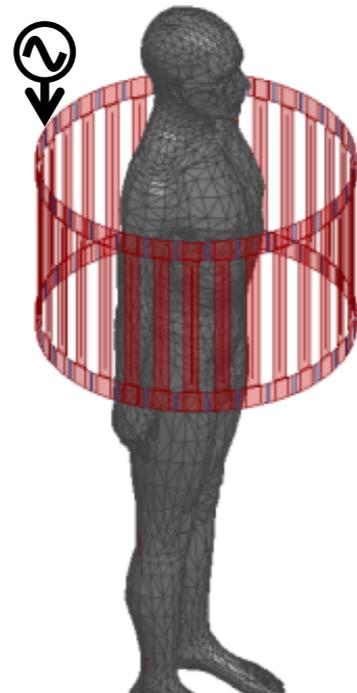


Flip-angle map

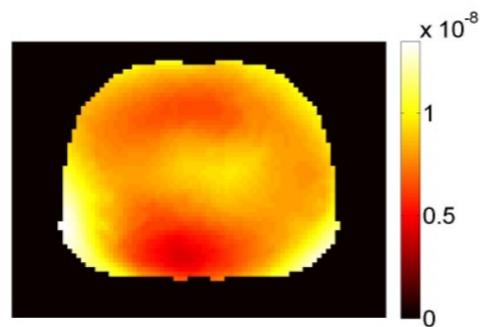


- ◆ Move from single channel to **multiple independent channels**

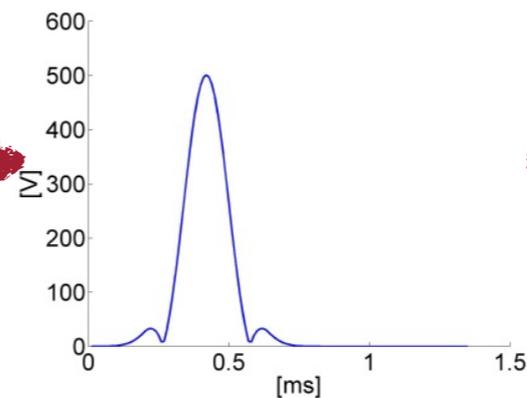
1 channel



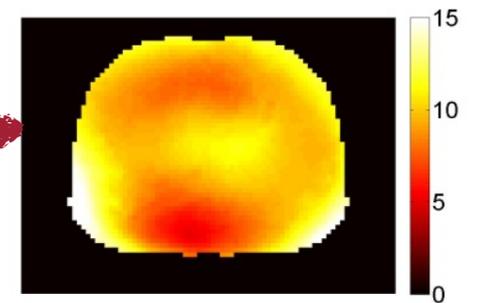
EM map / ch



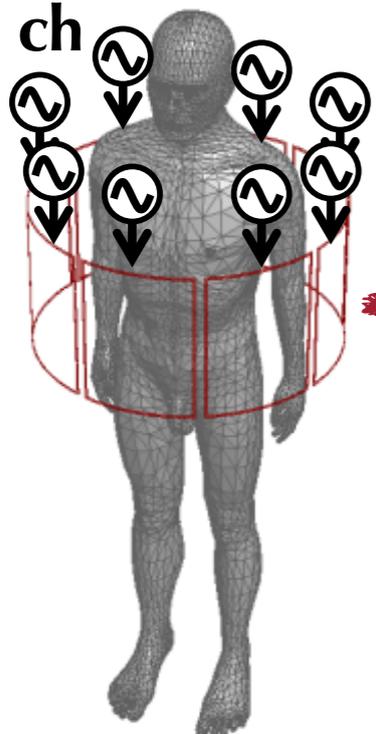
pulse design



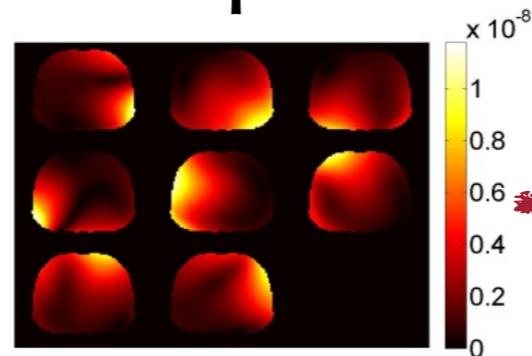
Flip-angle map



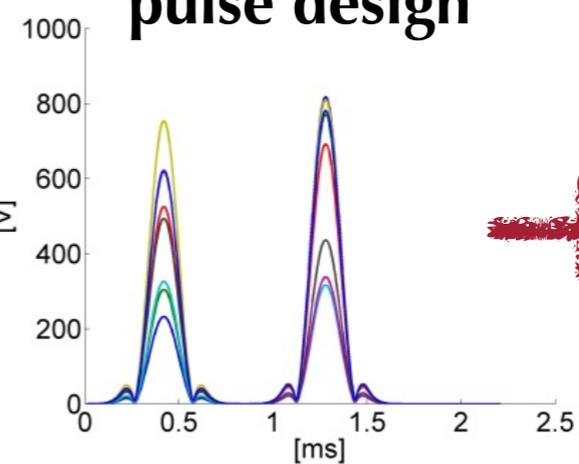
Multi ch



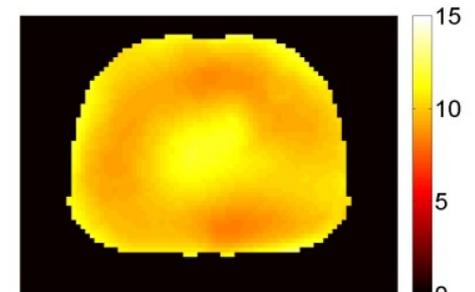
EM maps / ch



pulse design

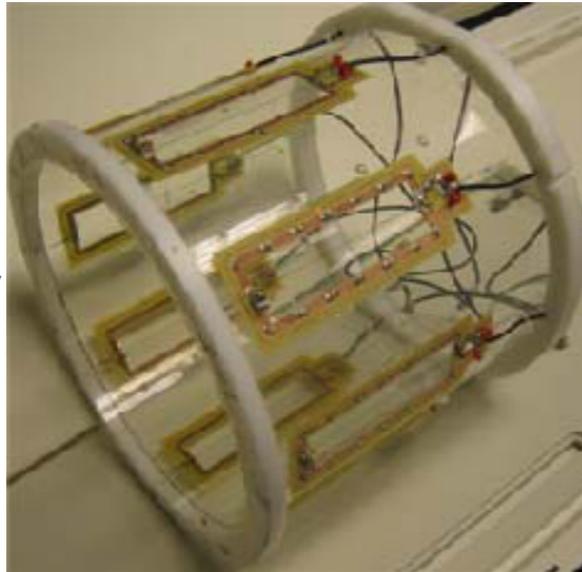


Flip-angle map

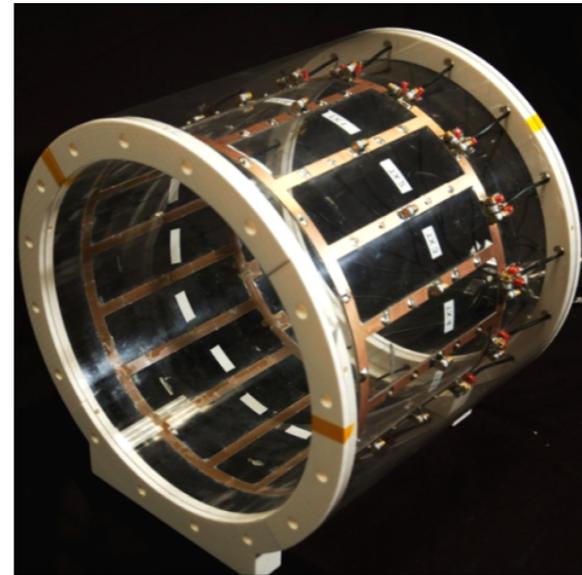


- ◆ **New MRI fashion** (images courtesy of Wei Zhao, MGH)

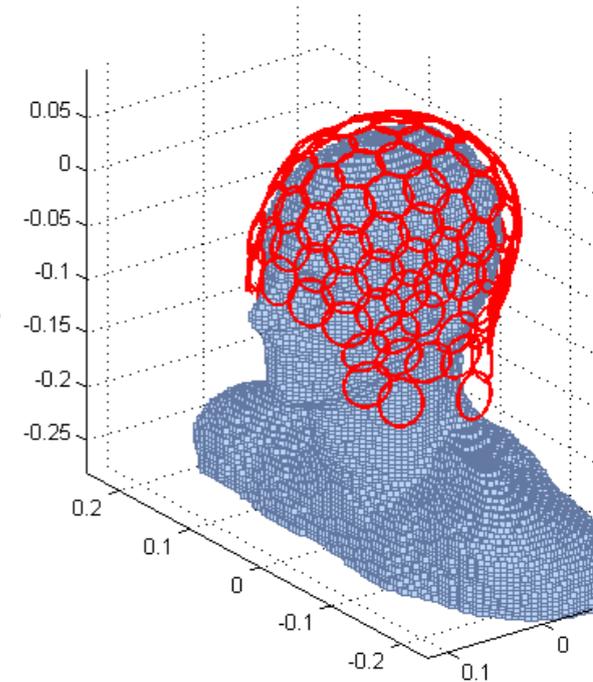
**Tx
8ch array**



**16ch
degenerate
birdcage**

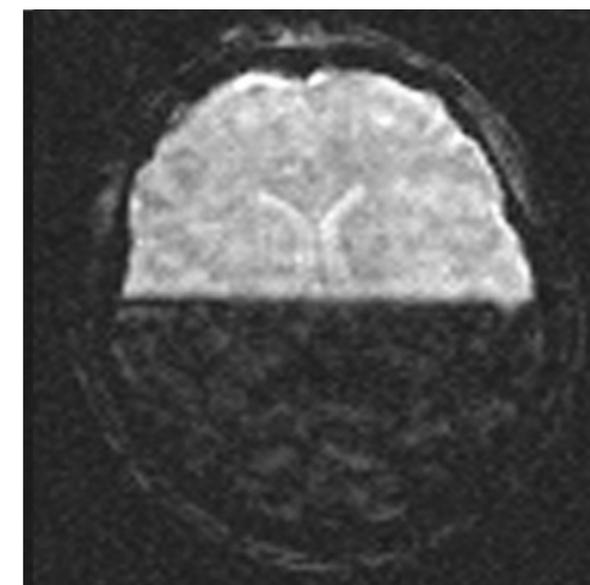
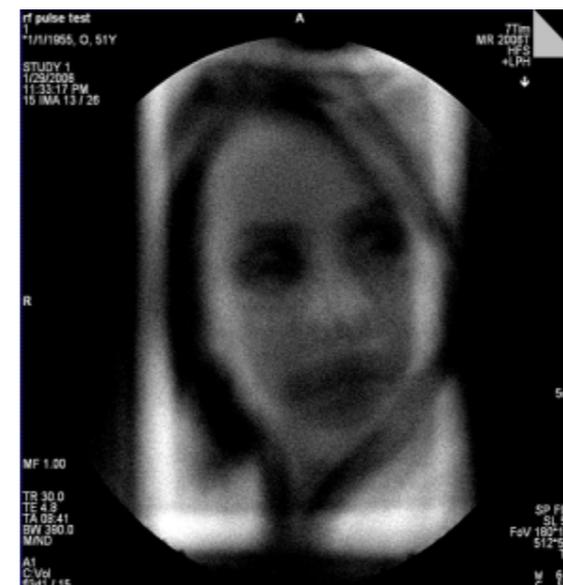
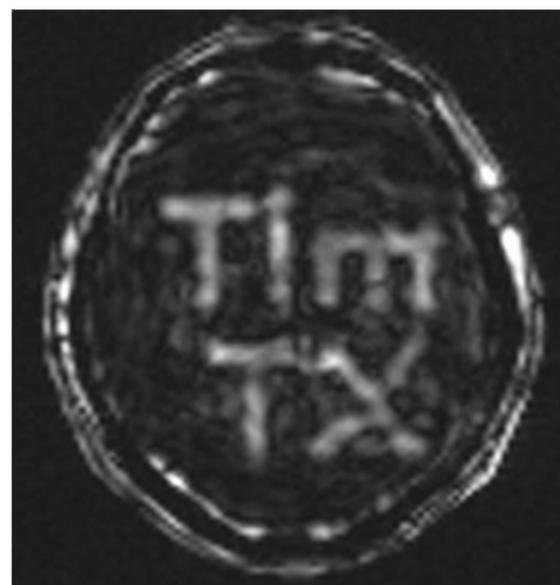


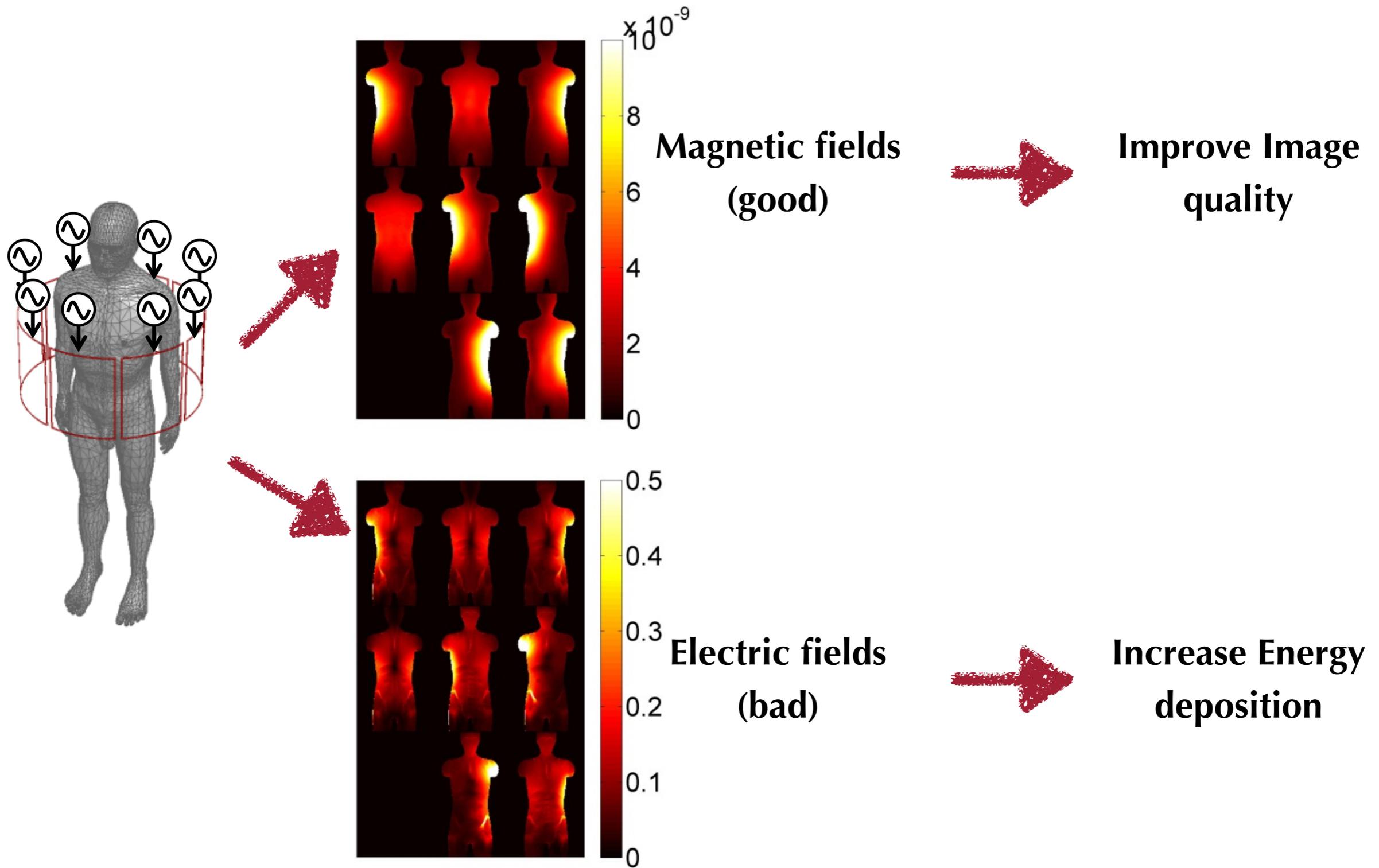
**Rx 128ch
prototype**



- ◆ **and artistic trends**

- ◆ 8ch pTx @7T, MLS (images courtesy of Kawin Setsompop, MGH)





- ◆ **Specific Absorption Rate (SAR)**

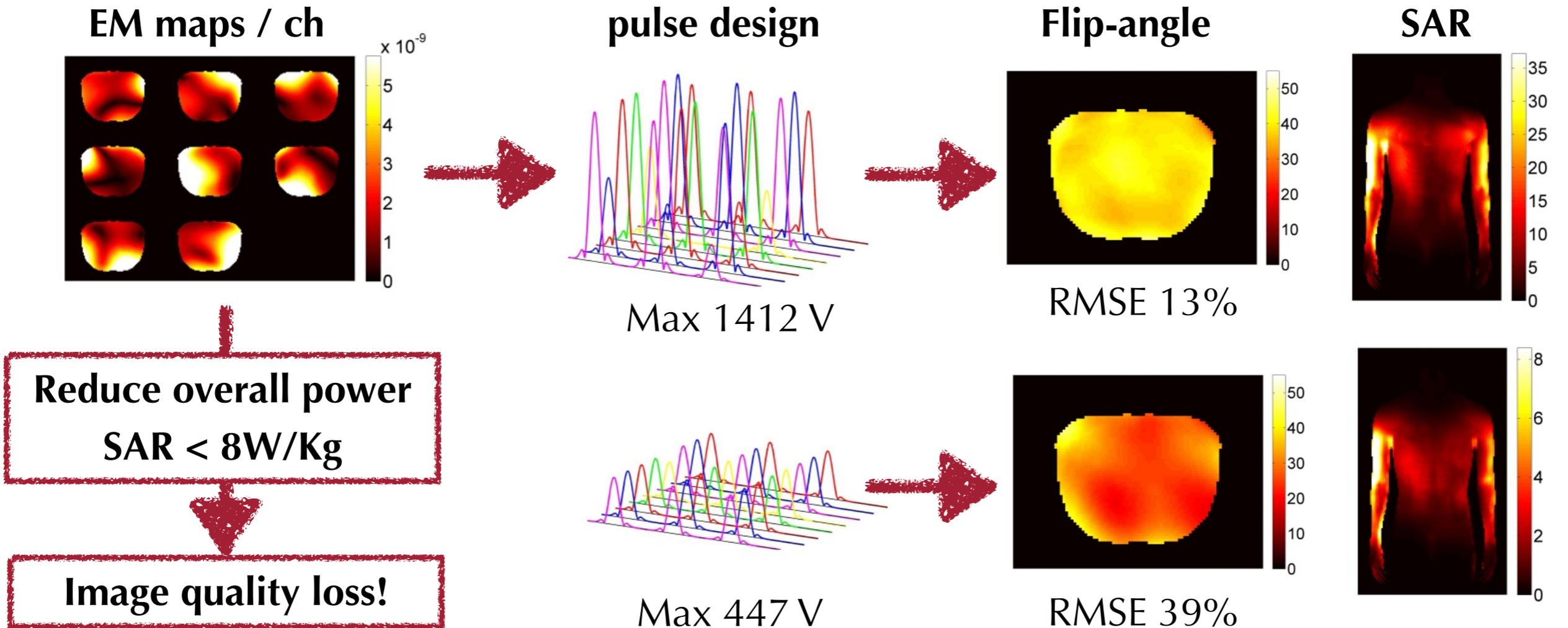
- ◆ time average energy deposited in patient

$$SAR(\mathbf{r}) = \frac{\sigma(\mathbf{r})}{2\rho(\mathbf{r})} \frac{1}{T} \int_0^T \|\mathbf{E}_{tot}(t)\|^2 dt$$

tissue properties

detailed E fields

◆ How to reduce SAR?



- ◆ How to reduce SAR?

$$SAR(\mathbf{r}) = \frac{\sigma(\mathbf{r})}{2\rho(\mathbf{r})} \frac{1}{T} \int_0^T \|\mathbf{E}_{tot}(t)\|^2 dt$$

$$\mathbf{E}_{tot}(\mathbf{r}, t) = \sum_{c=1}^C \mathbf{b}_c(t) \mathbf{E}_c(\mathbf{r})$$

channels

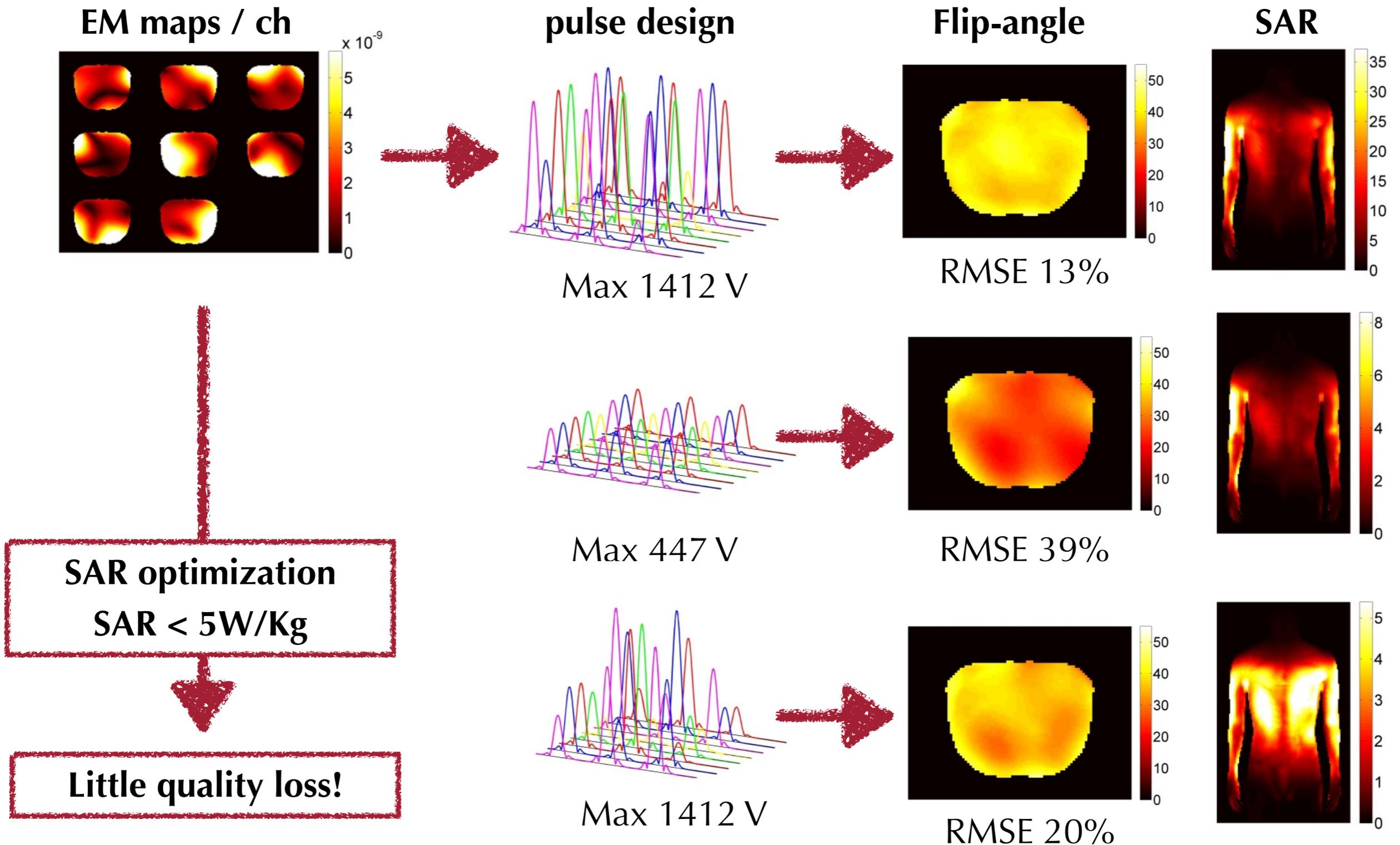
RF pulse at channel c at time t

E map of channel c

Play with RF pulses
to reduce SAR!

$$SAR(\mathbf{r}) = \frac{1}{N} \sum_{t=1}^N \mathbf{b}^H(t) \mathbf{Q}(\mathbf{r}) \mathbf{b}(t)$$

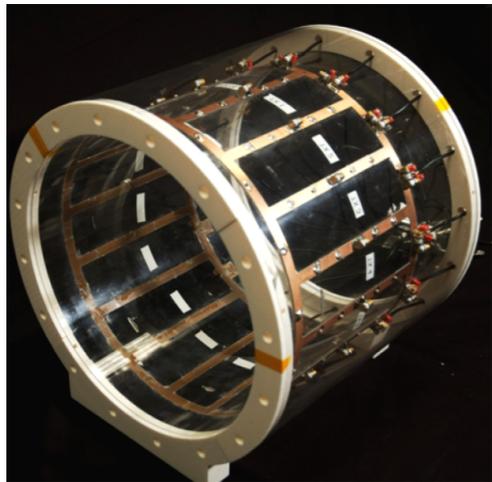
◆ How to reduce SAR?



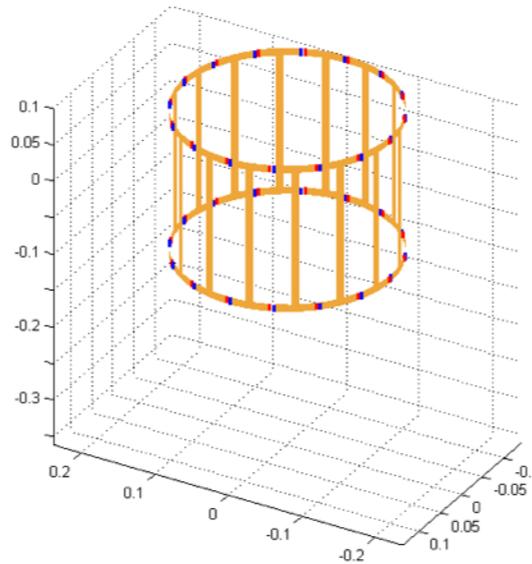
We need the EM field maps per channel



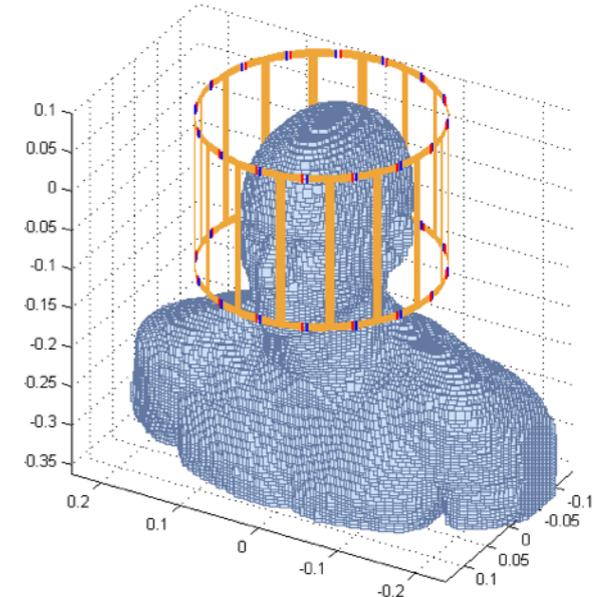
- ◆ Need EM distribution in **realistic human body models**



load model
flag ports



body model

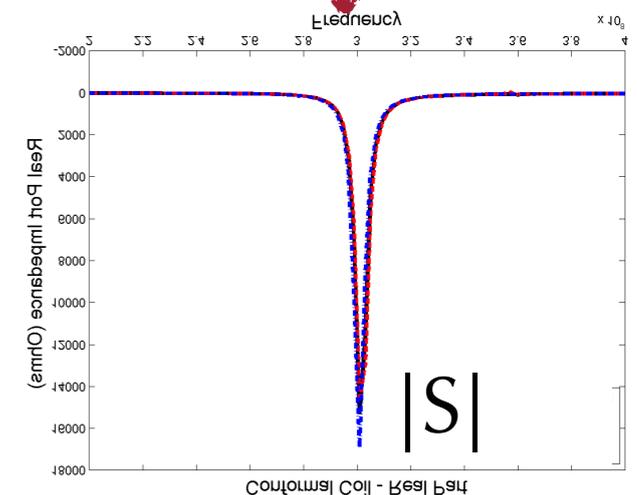
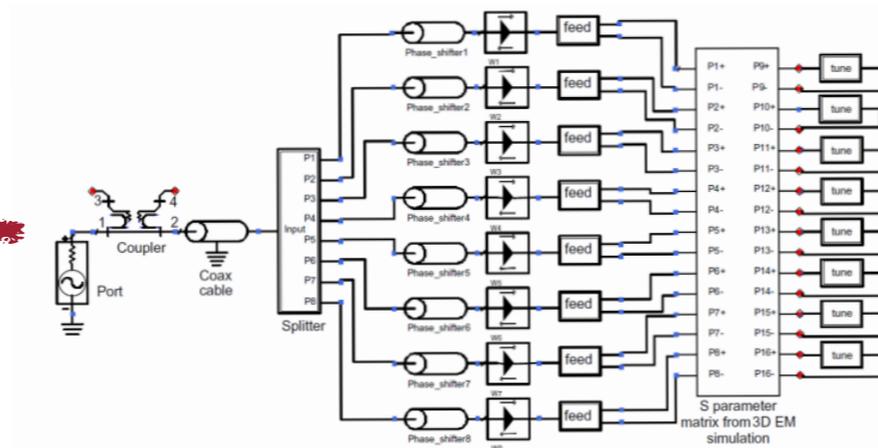


Full-wave EM simulation



circuit co-simulation [1]

Tuning
Matching
Decoupling
Circuitry

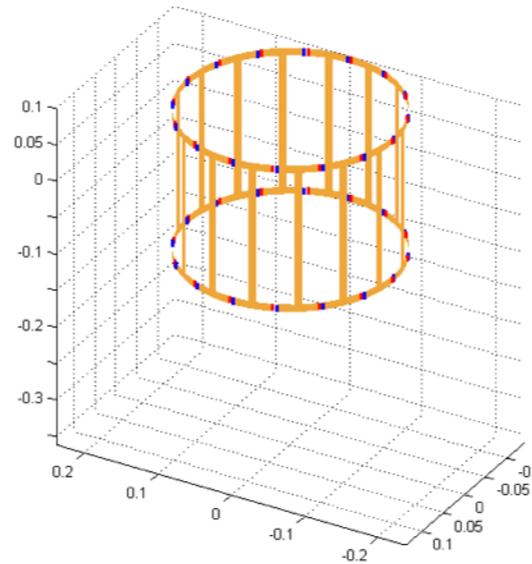


[1] M. Kozlov et al., "Fast MRI coil analysis based on 3-D electromagnetic and RF circuit co-simulation", *JMR* 2009.

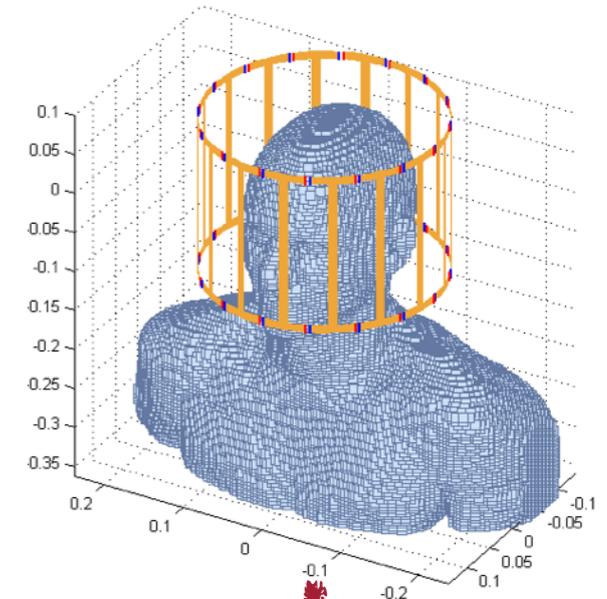
- ◆ Need EM distribution in **realistic human body models**

Tuning
Matching
Decoupling
Circuitry

connect to
coil array



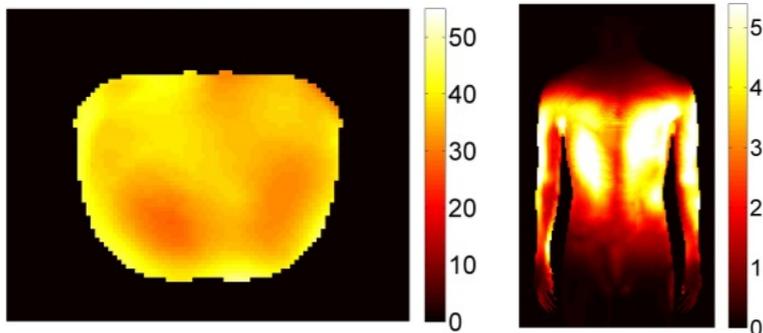
body model



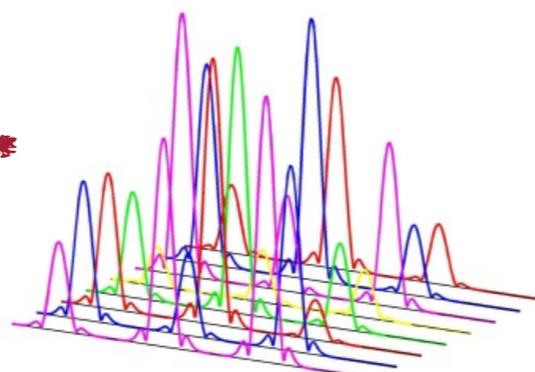
Full-wave EM simulation



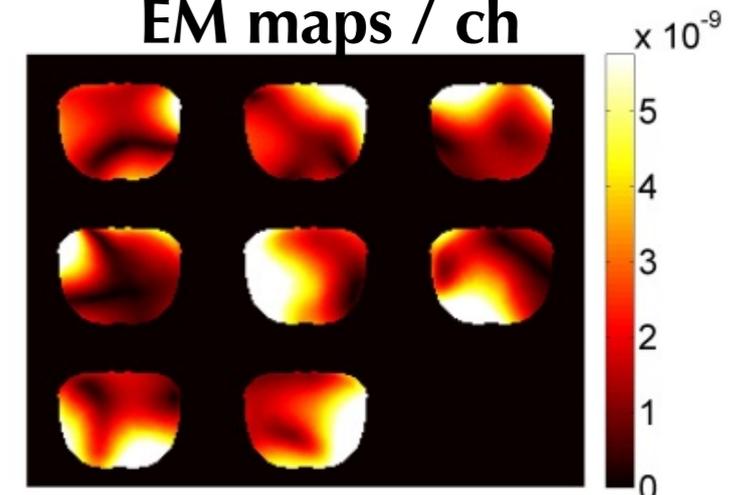
SAR compliant pulse



pulse design [2]

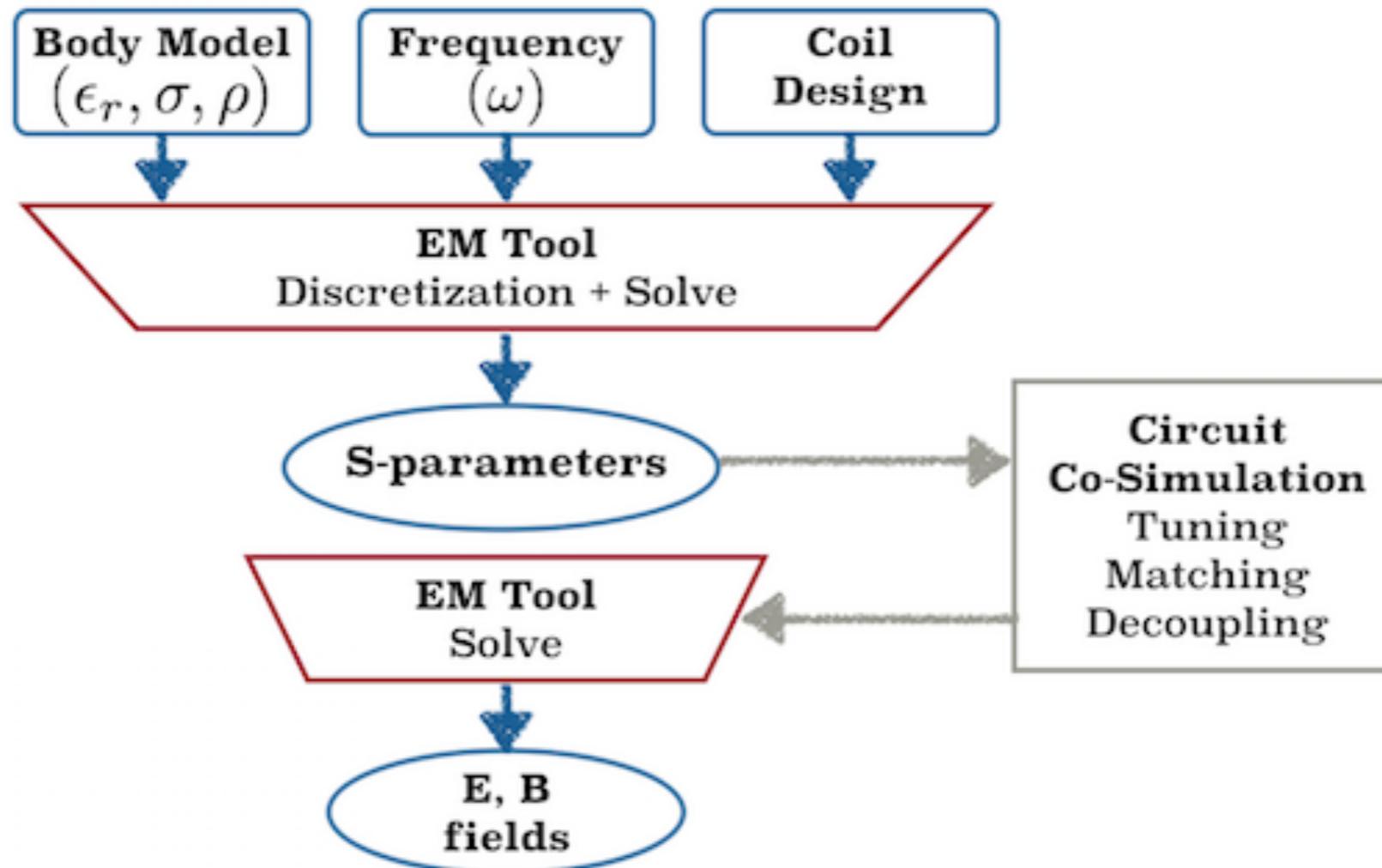


EM maps / ch



[2] B. Guerin et al., "Local SAR, global SAR, transmitter power, and excitation accuracy trade-offs in low flip-angle parallel transmit pulse design", **MRM 2013**.

- ◆ **Traditional EM analysis tools**



simply too slow and not flexible!

- ◆ **EM analysis tools: Surface integral equation methods**
 - ◆ Approximate: body model by homogeneous phantom
 - ◆ Discretize: only body and conductors surface
 - ◆ model conformal surfaces
 - ◆ no air discretization
 - ◆ smaller systems
 - ◆ fast (10min/simulation)
 - ◆ OK for coil S-parameters
 - ◆ approximate EM fields
 - ◆ useless for SAR calculations

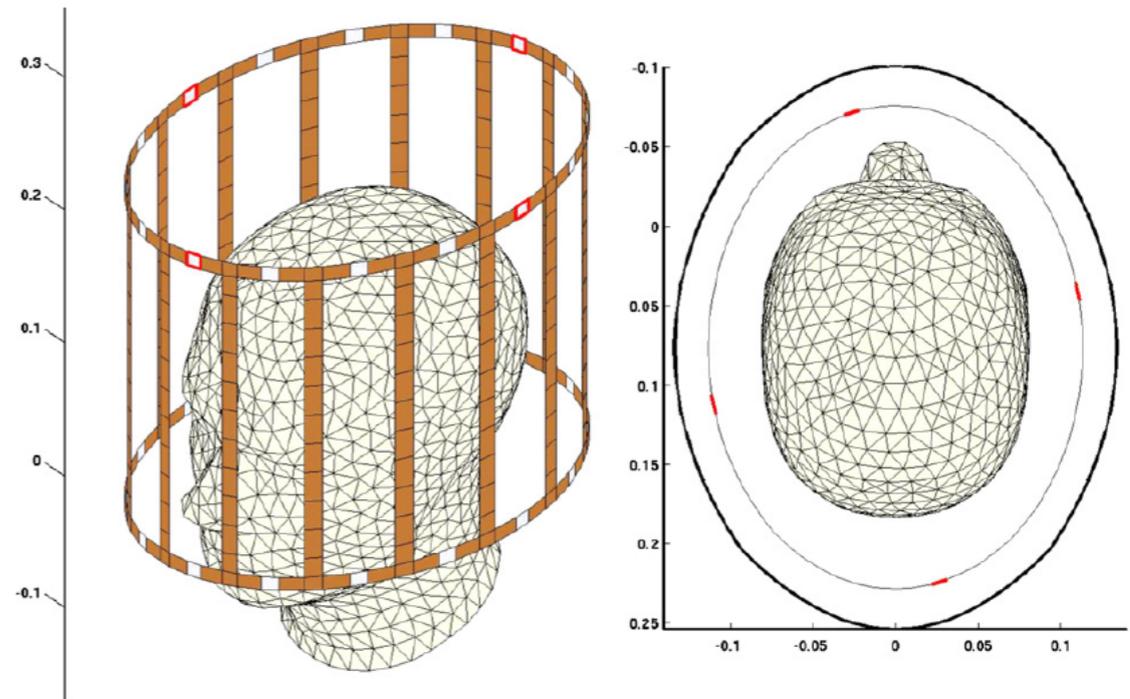


image courtesy of S. Wang, PMB 2008

- ◆ **EM analysis tools: Finite Difference Time Domain / Finite Element**
 - ◆ Volume discretization: inhomogeneous models
 - ◆ Discretize: whole domain, plus boundary conditions
 - ◆ refinement for conformal surfaces
 - ◆ air discretization
 - ◆ large (sparse) systems
 - ◆ convergence issues
 - ◆ Slow (hours/simulation)
 - ◆ bad coil S-parameters approx. (FDTD)
 - ◆ good for SAR calculations

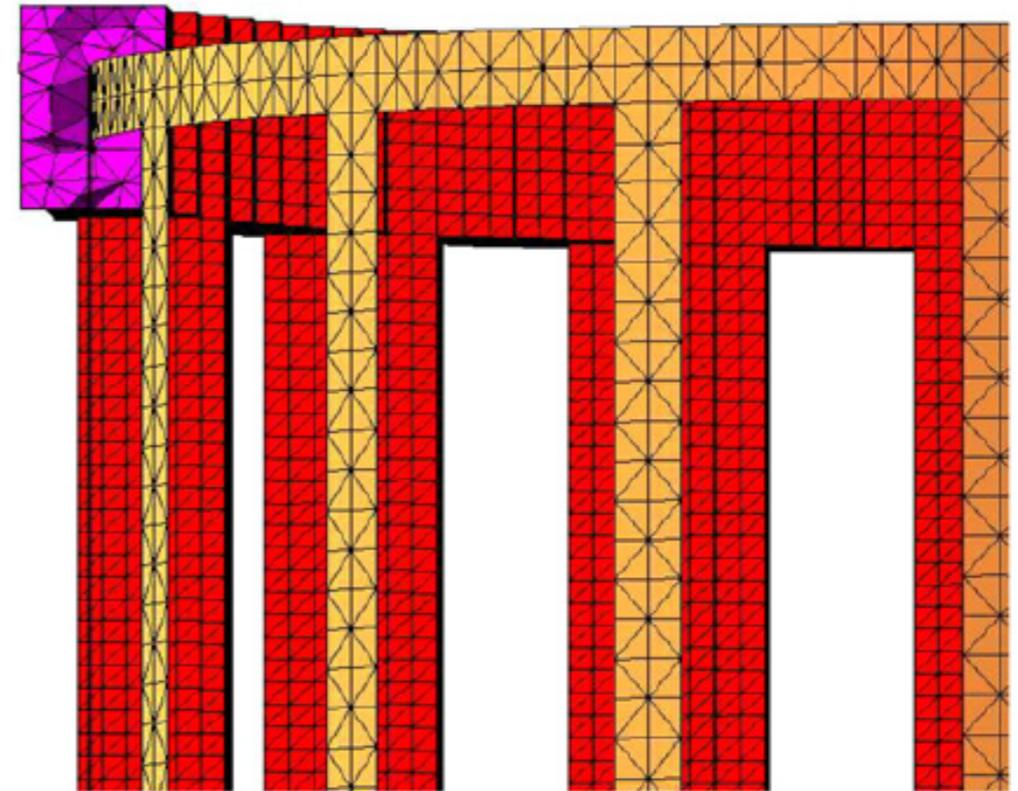


image courtesy of S. Wang, PMB 2008

- ◆ **Traditional EM analysis tools: acceleration? sure!**

...for \$97 million

Flagship accelerated computing system | 200-cabinet Cray XK7 supercomputer |
18,688 nodes (AMD 16-core Opteron + NVIDIA Tesla K20 GPU) |
CPUs/GPUs working together – GPU accelerates | 20+ Petaflops

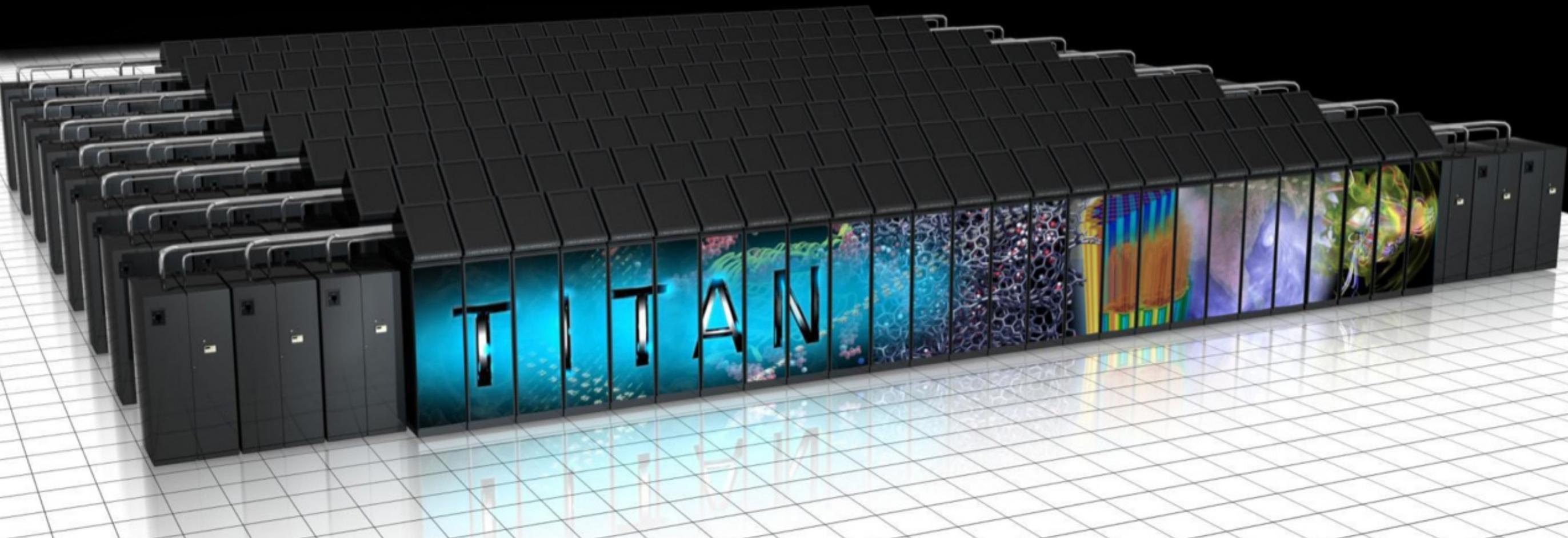
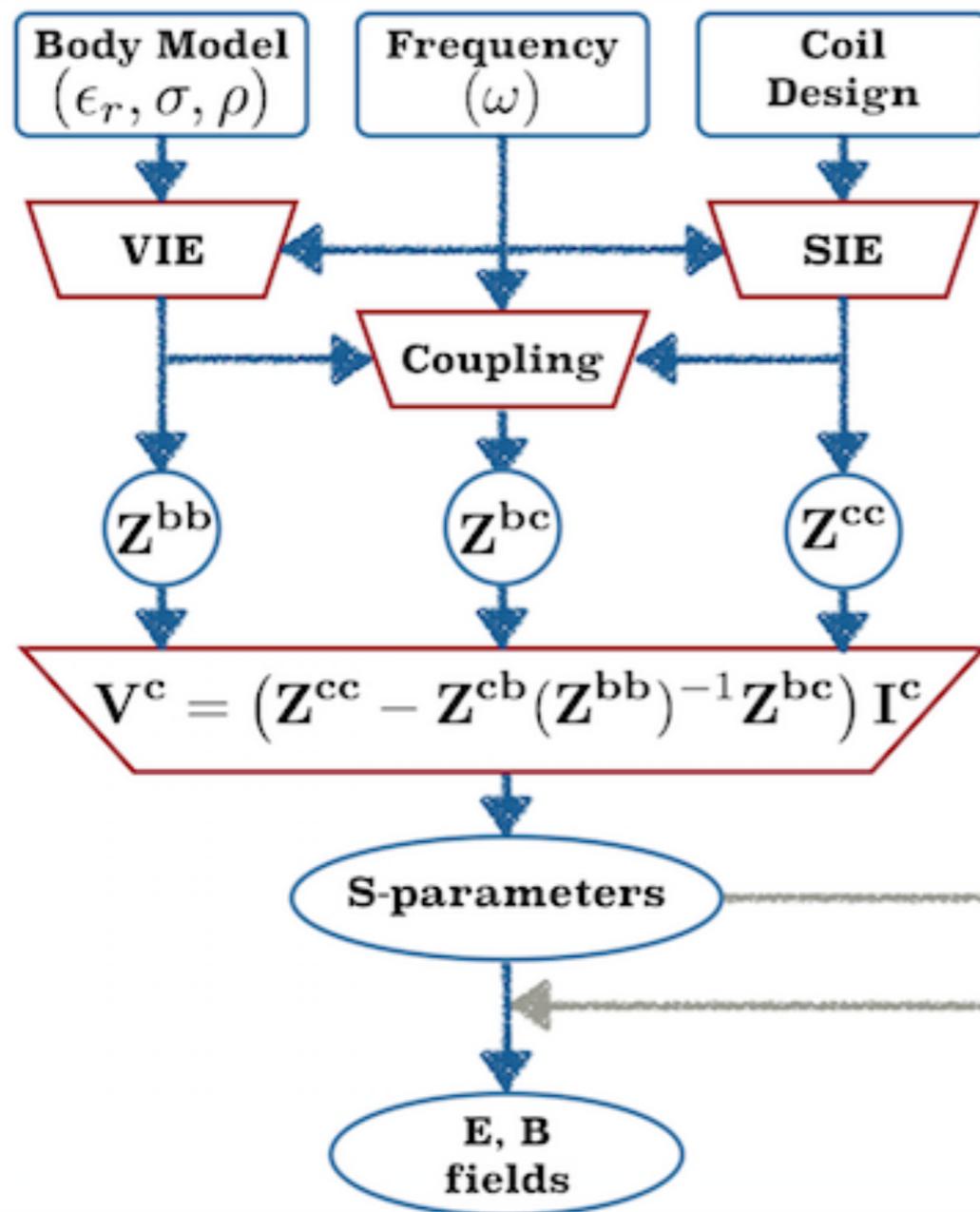


Image: Cray Titan supercomputer at Oak Ridge National Laboratory

- ♦ **Goal: accelerate the EM analysis flow**

- ♦ Integral equation methods & sophisticated numerical methods
- ♦ Leverage problem knowledge



complete analysis in minutes!

- ◆ **1 desktop server**

- ◆ MATLAB 2013 running on Windows R2008
- ◆ two Xeon E2685W (16 cores total) @3.1GHz
- ◆ a K20X GPU Nvidia (6GB mem.)



MRI coil
design

Patient
Specific MRI

?

Robust
Optimisation

Ultimate
SNR/SAR

MRI coil
design

Patient
Specific MRI

 Marie
magnetic resonance integral equation

Ultimate
SNR/SAR

Robust
Optimisation

- ◆ **Open source MATLAB code**
 - ◆ beta-version coming soon

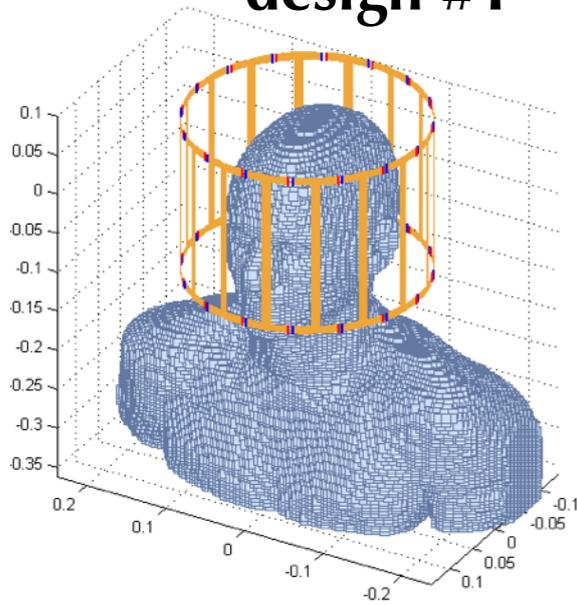


- ◆ **Prototype tools with focus on**
 - ◆ Fast solvers for complex inhomogeneous media
 - ◆ Combination with surface-based coil models
 - ◆ Domain oriented iterative methods
 - ◆ Acceleration: pre-computation of fixed parts

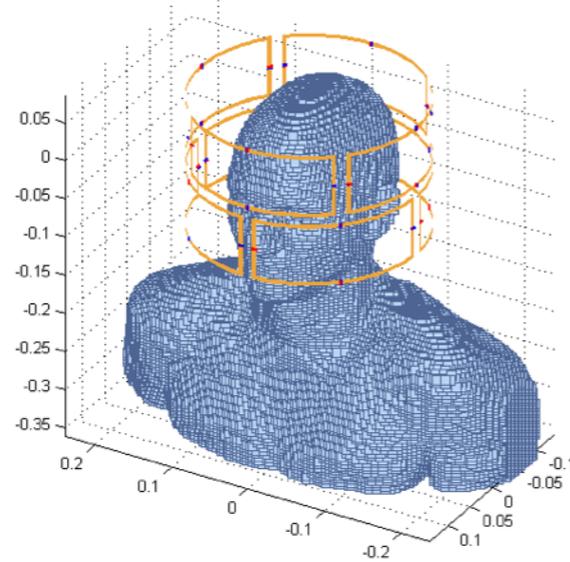
MRI coil
design

◆ Best out of 500 coil designs?

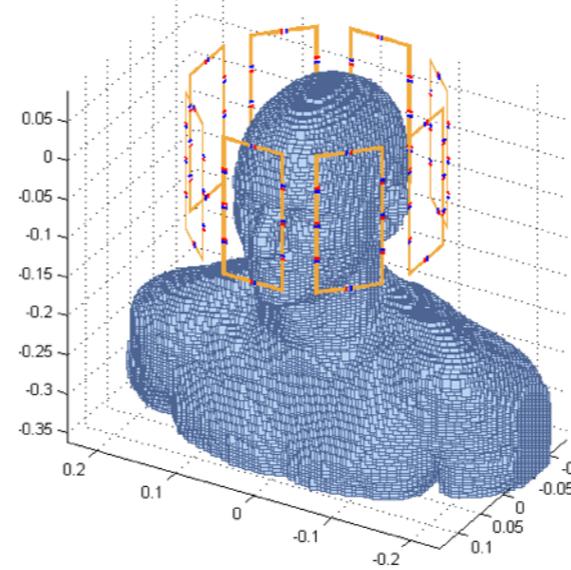
design #1



design #2

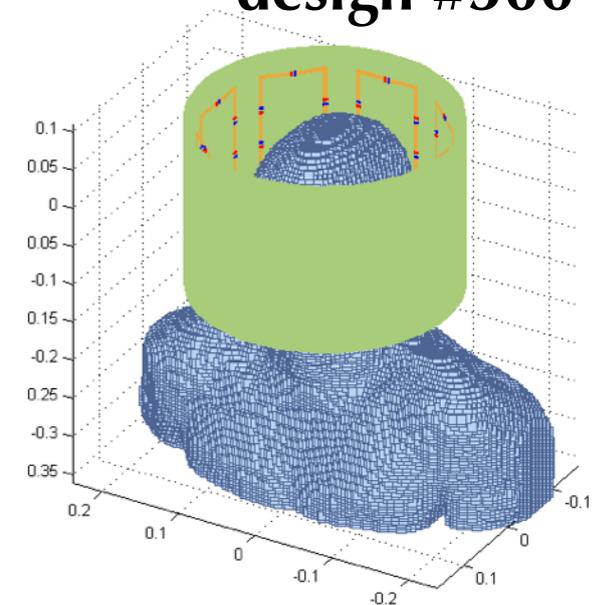


design #3



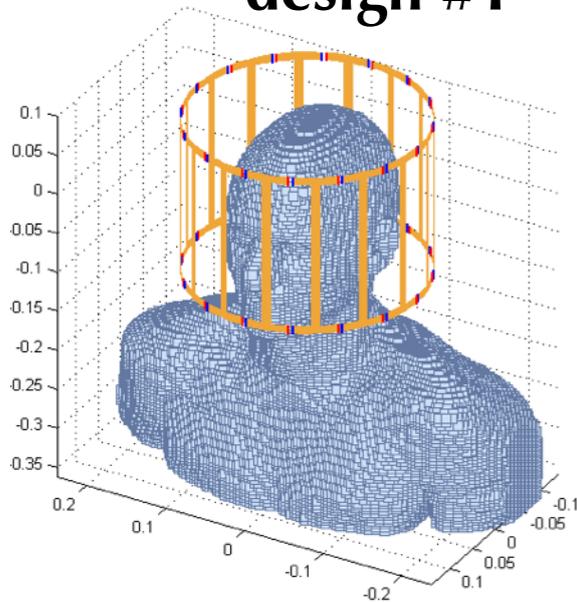
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design #500

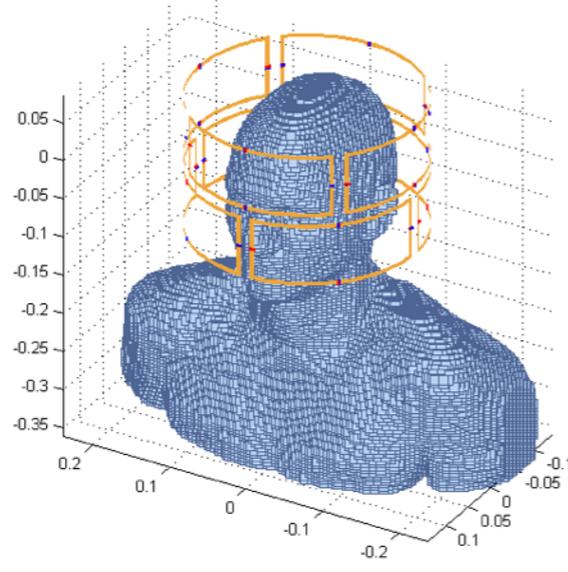


◆ Best out of 500 coil designs?

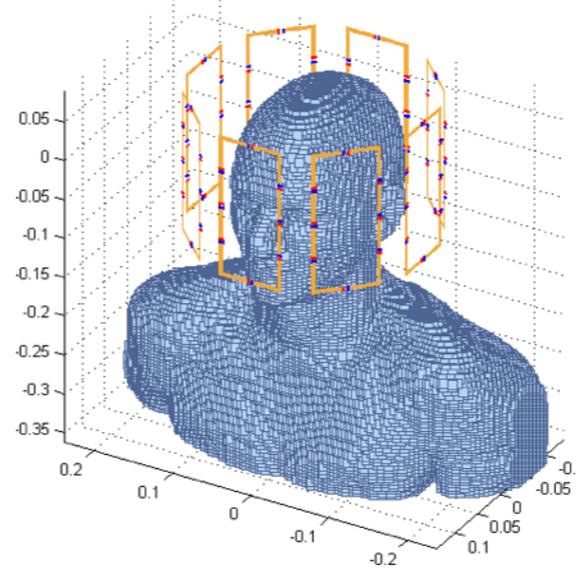
design #1



design #2

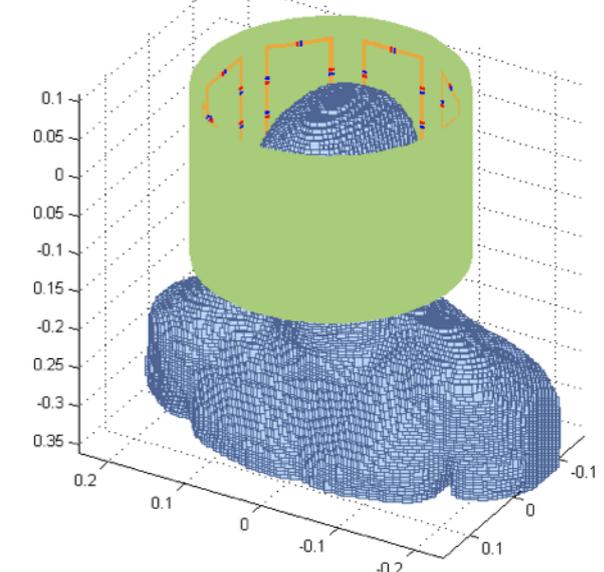


design #3

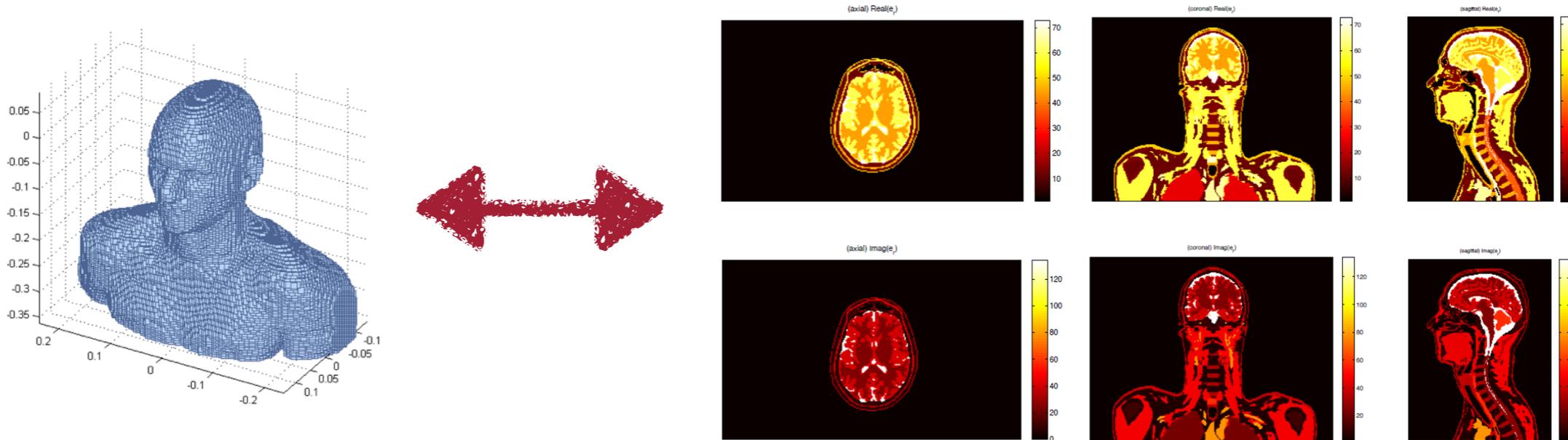


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design #500



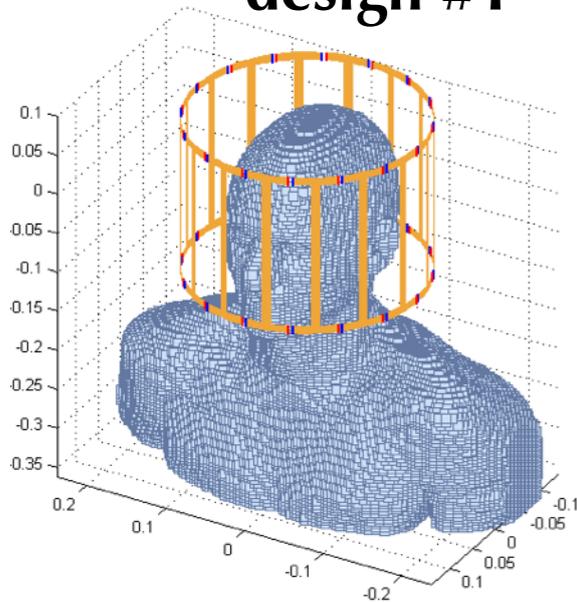
for inhomogeneous realistic human body models [1]



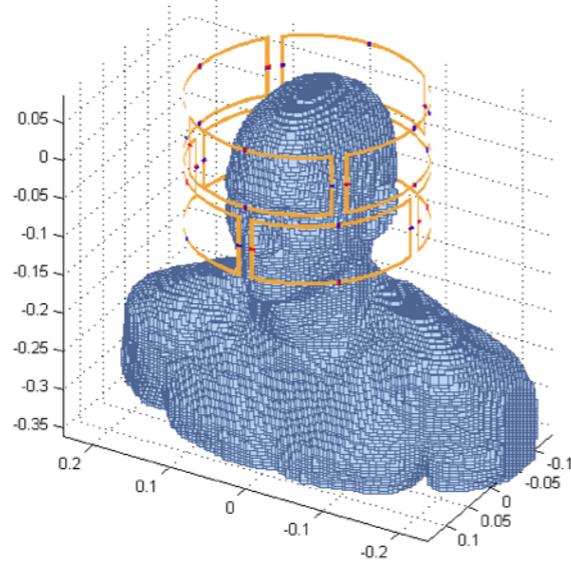
[1] A. Christ et al., "The Virtual Family - development of anatomical CAD models of two adults and two children for dosimetric simulations," *PMB* 2010.

- ◆ Best out of 500 coil designs? **Need full EM analysis of each design**

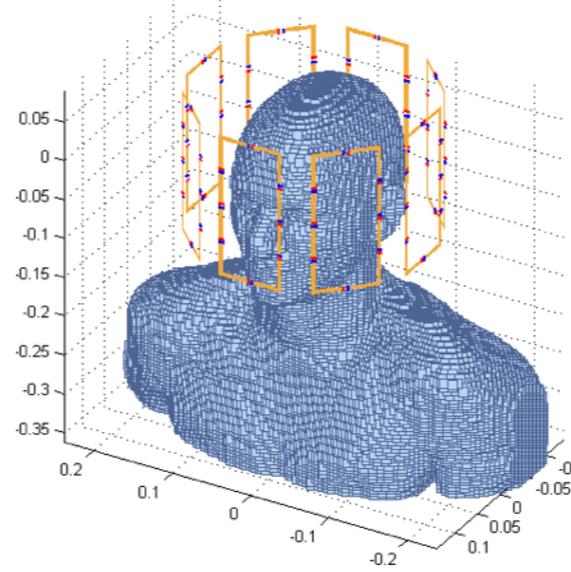
design #1



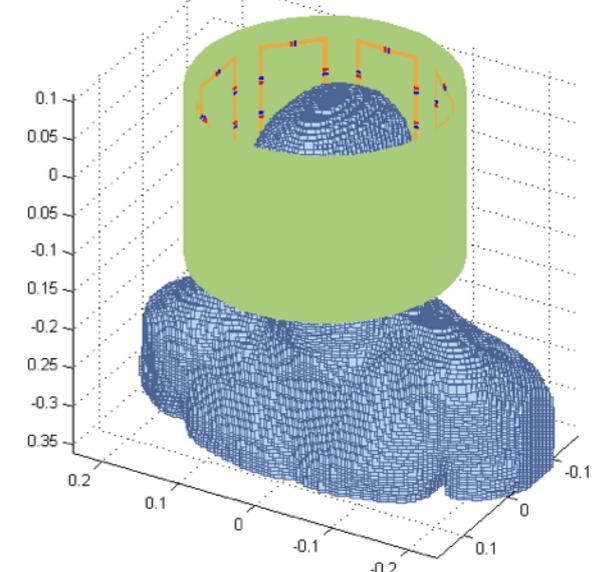
design #2



design #3

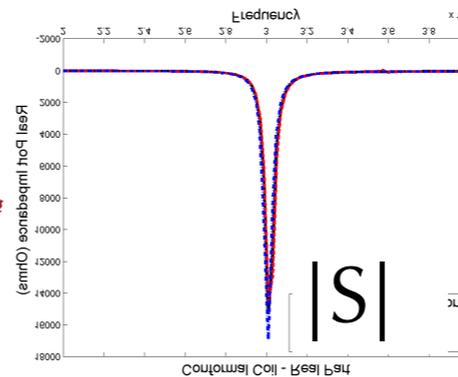


design #500

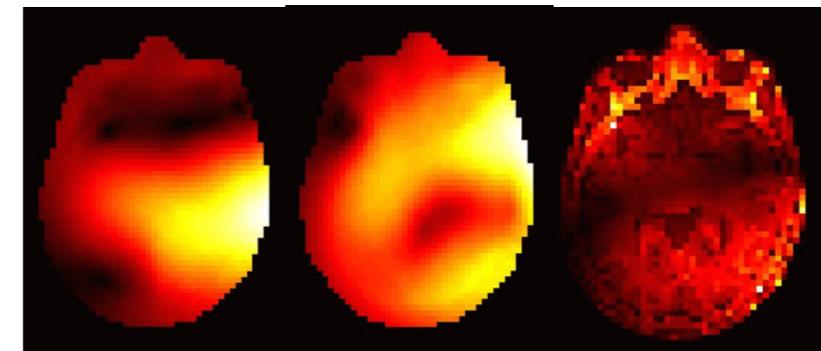


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Full EM analysis

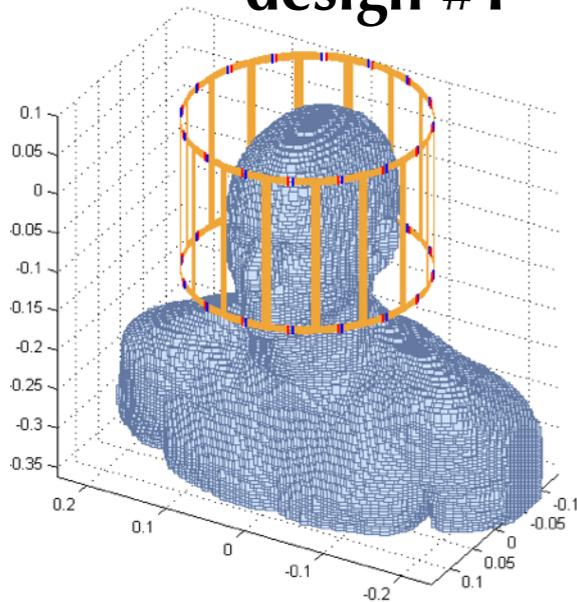


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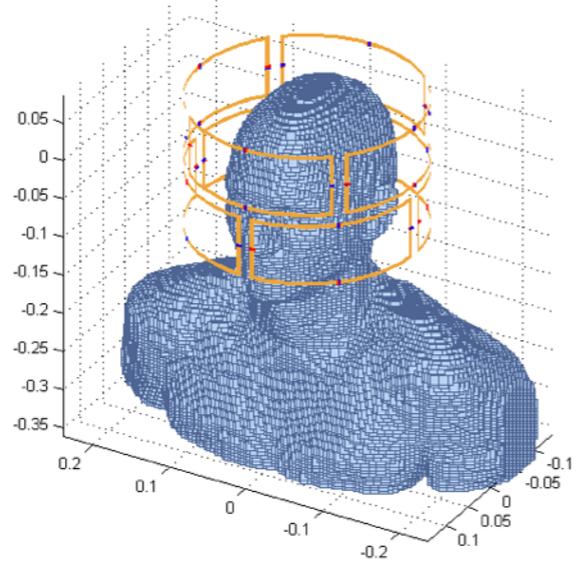


- ◆ Best out of 500 coil designs? **Need full EM analysis of each design**

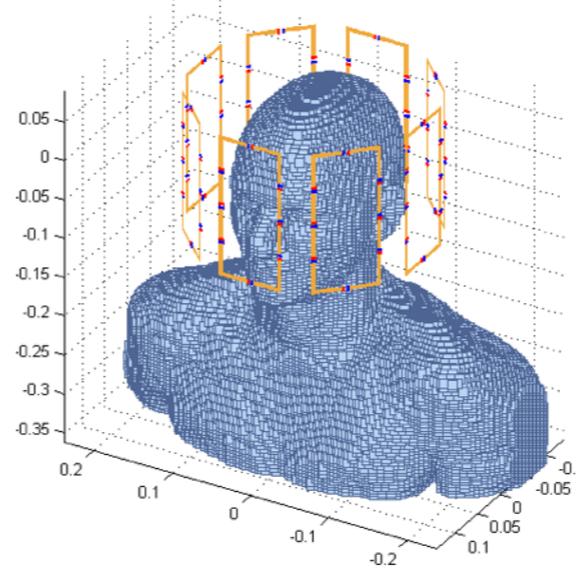
design #1



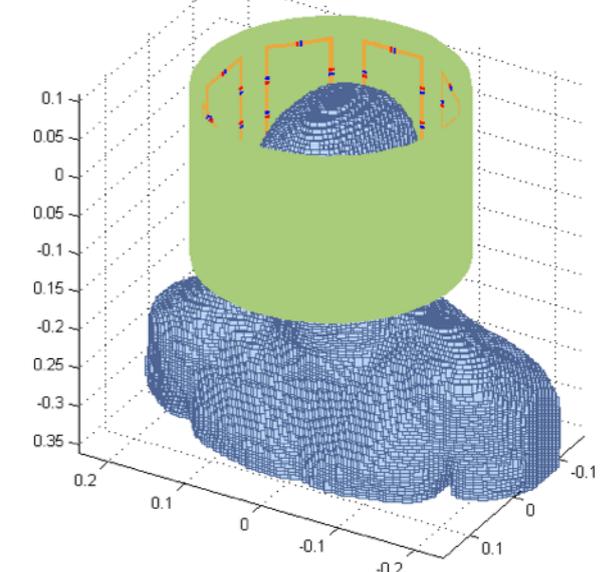
design #2



design #3

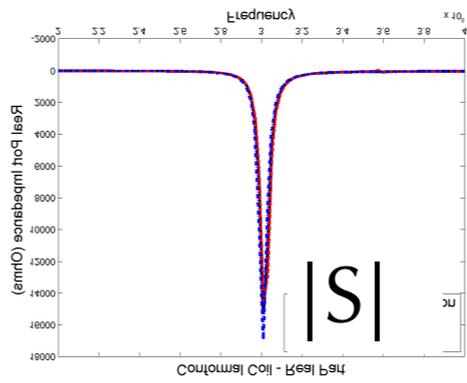


design #500

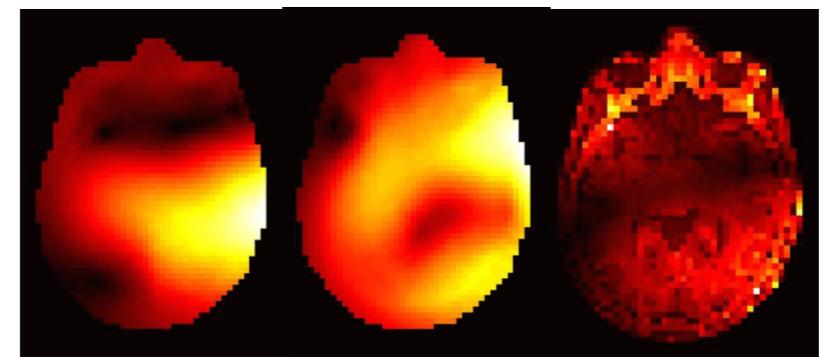


**Existing tools:
> 1 month
(hours / design)**

Full EM analysis

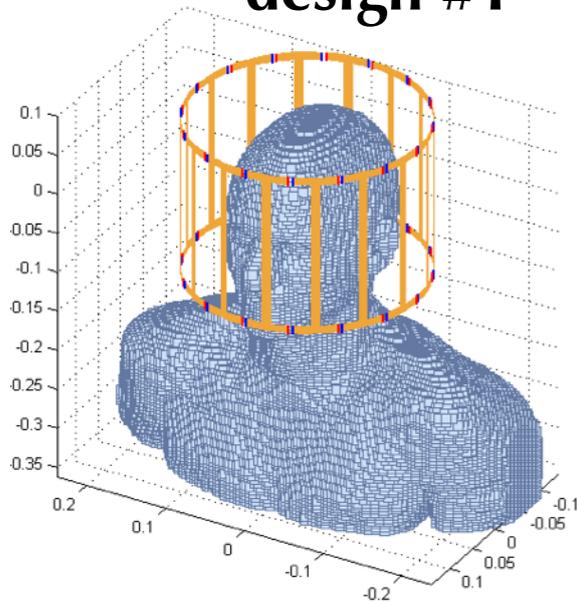


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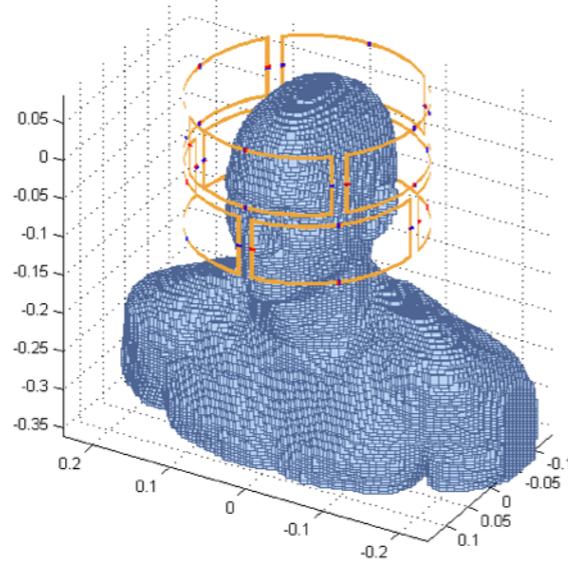


- ◆ Best out of 500 coil designs? **Need full EM analysis of each design**

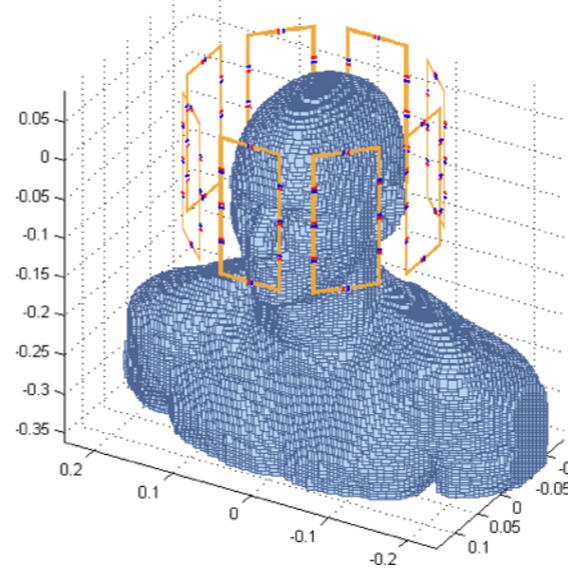
design #1



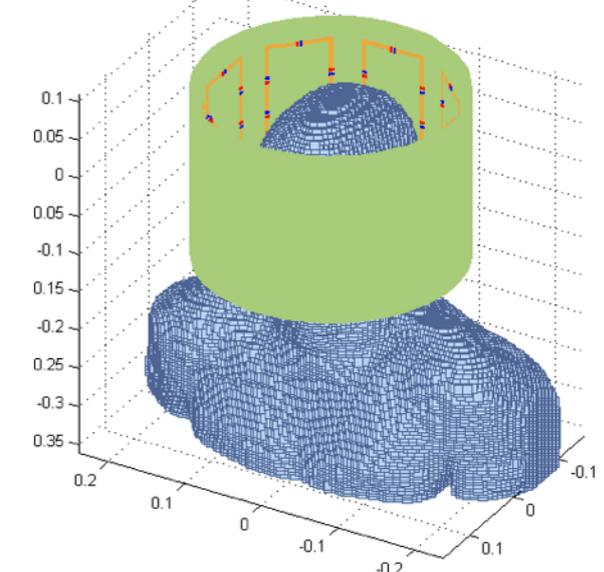
design #2



design #3



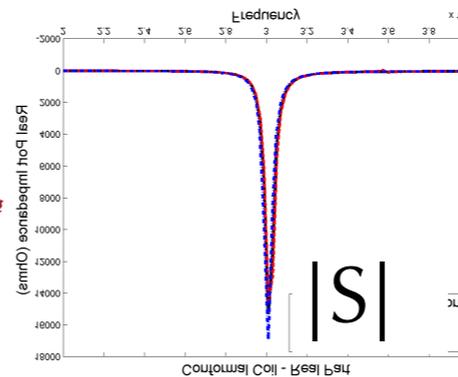
design #500



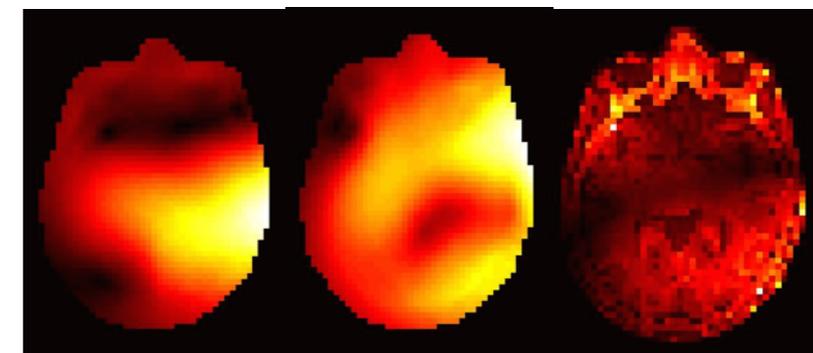
~~Existing tools:
> 1 month
(hours / design)~~

Proposed tool:
over the weekend
(~4min / design)

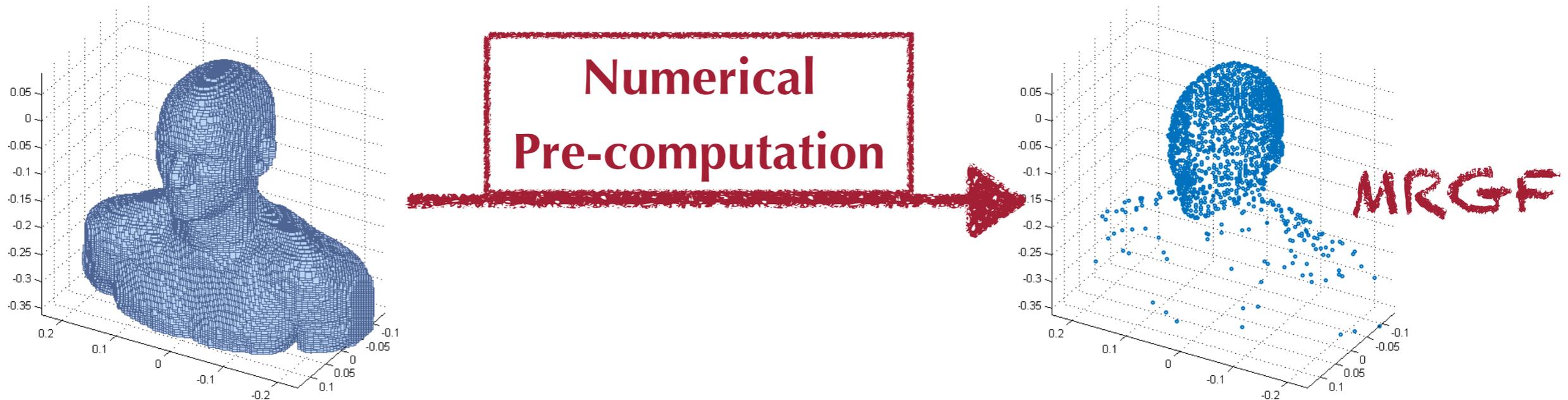
Full EM analysis



&



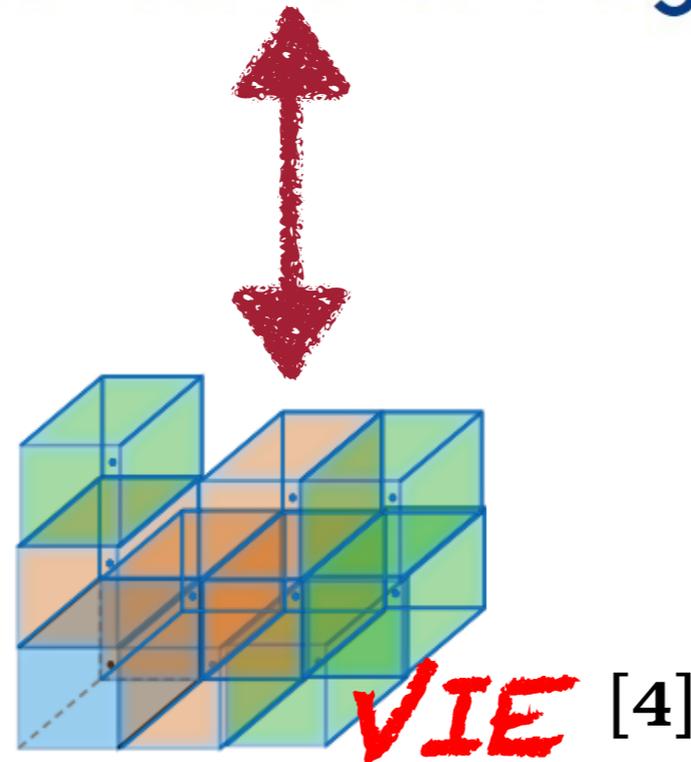
- ◆ **MRI customized simulation tools**
 - ◆ based on **Integral Equation** methods
 - ◆ and **pre-computed Magnetic Resonance Green functions**



Magnetic Resonance specific Integral Equation suite

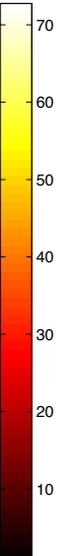
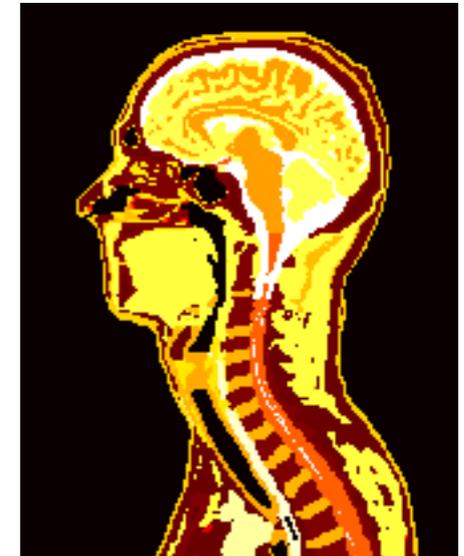
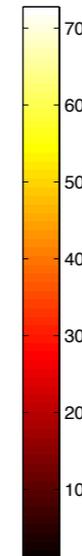
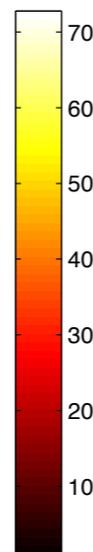
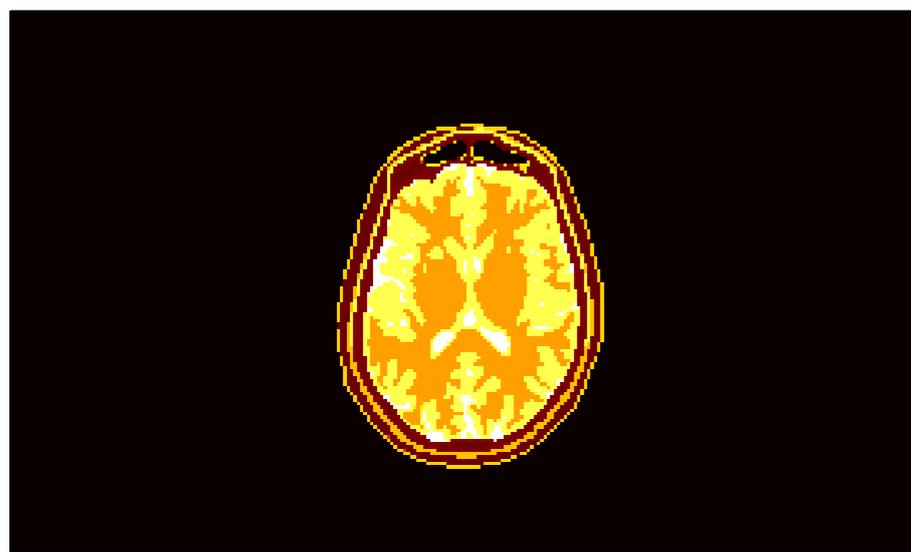
- ♦ Fast MR-specific Volume Integral Equation (VIE) solver

 **Marie**
magnetic resonance integral equation

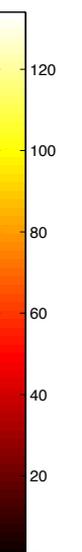
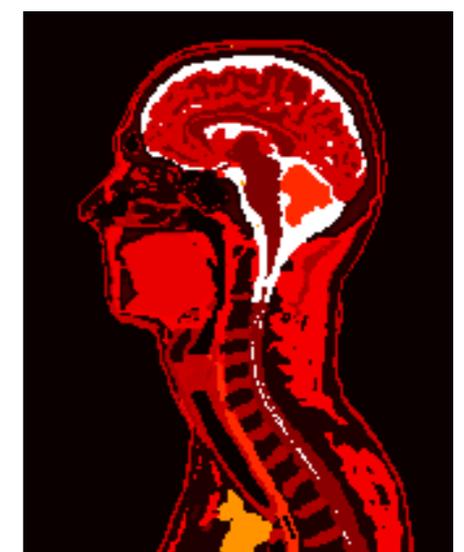
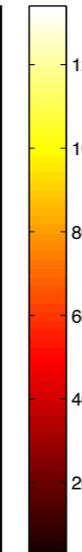
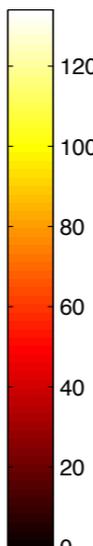
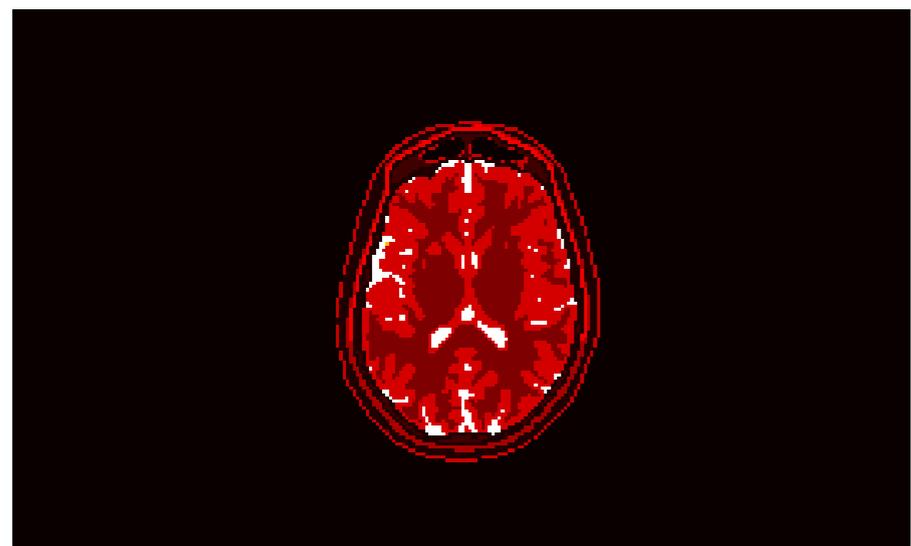


- ◆ Electric properties at 7T (298MHz)

$$\text{Re}\{\epsilon_r\}$$

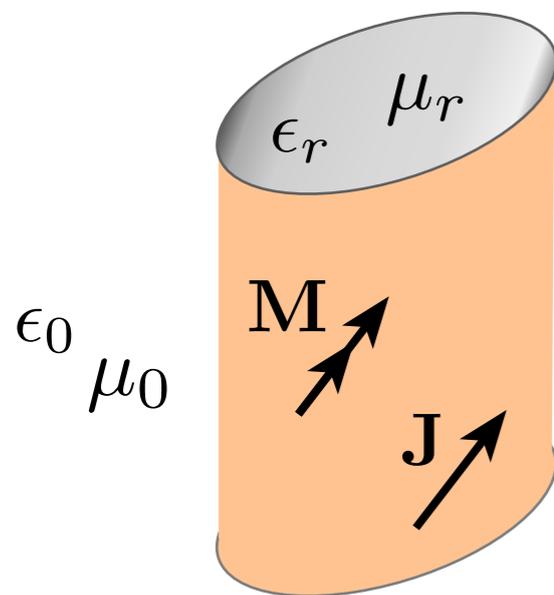


$$\text{Im}\{\epsilon_r\}$$



- ◆ **IE-based**
 - ◆ frequency domain (MRI is single frequency analysis)
 - ◆ reduces dimensionality and satisfy radiation conditions
 - ◆ easy to “couple” with other solvers
- ◆ **New current-based formulation (JVIE)**
 - ◆ natural formulation for MRI applications
- ◆ **Machine precision integration**
 - ◆ DEMCEM and DIRECTFN packages (http://web.mit.edu/thanos_p/www/)
- ◆ **FFT-based fast solver**
 - ◆ exploit voxel based data from MRI
- ◆ **Well conditioned system - fast convergence**
 - ◆ even for high contrast

◆ Formulas for total fields



$$\mathbf{e} = \mathbf{e}^{\text{inc}} + \mathbf{e}^{\text{sca}} = \mathbf{e}^{\text{inc}} + \frac{1}{c_\epsilon} \mathcal{L} \mathbf{j} - \mathcal{K} \mathbf{m}$$

$$\mathbf{h} = \mathbf{h}^{\text{inc}} + \mathbf{h}^{\text{sca}} = \mathbf{h}^{\text{inc}} + \frac{1}{c_\mu} \mathcal{L} \mathbf{m} + \mathcal{K} \mathbf{j}$$

$$\mathbf{j}(\mathbf{r}) \triangleq c_\epsilon \chi_\epsilon(\mathbf{r}) \mathbf{e}(\mathbf{r})$$

$$c_\epsilon = j\omega\epsilon_0$$

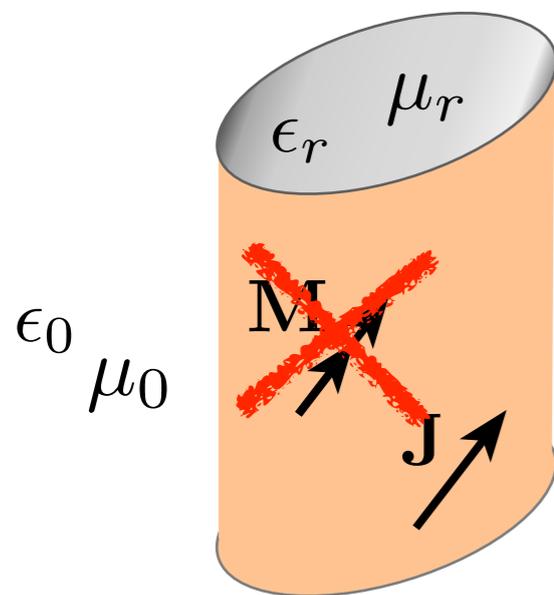
$$\chi_\epsilon = \epsilon_r(\mathbf{r}) - 1$$

$$\mathcal{L} \mathbf{u} \triangleq (k_0^2 + \nabla \nabla \cdot) \mathcal{S}(\mathbf{u}; \Omega)(\mathbf{r})$$

$$\mathcal{K} \mathbf{u} \triangleq \nabla \times \mathcal{S}(\mathbf{u}; \Omega)(\mathbf{r})$$

$$\mathcal{S}(\mathbf{u}; \Omega)(\mathbf{r}) \triangleq \int_{\Omega} G(\mathbf{R}) \mathbf{u}(\mathbf{r}') d\mathbf{r}'$$

- ◆ Formulas for total fields
 - ◆ non-magnetic material



$$\mathbf{e} = \mathbf{e}^{\text{inc}} + \mathbf{e}^{\text{sca}} = \mathbf{e}^{\text{inc}} + \frac{1}{c_\epsilon} \mathcal{L} \mathbf{j} - \mathcal{K} \mathbf{m}$$

$$\mathbf{h} = \mathbf{h}^{\text{inc}} + \mathbf{h}^{\text{sca}} = \mathbf{h}^{\text{inc}} + \frac{1}{c_\mu} \mathcal{K} \mathbf{m} + \mathcal{L} \mathbf{j}$$

$$\mathbf{j}(\mathbf{r}) \triangleq c_\epsilon \chi_\epsilon(\mathbf{r}) \mathbf{e}(\mathbf{r})$$

$$c_\epsilon = j\omega\epsilon_0$$

$$\chi_\epsilon = \epsilon_r(\mathbf{r}) - 1$$

$$\mathcal{L} \mathbf{u} \triangleq (k_0^2 + \nabla \nabla \cdot) \mathcal{S}(\mathbf{u}; \Omega)(\mathbf{r})$$

$$\mathcal{K} \mathbf{u} \triangleq \nabla \times \mathcal{S}(\mathbf{u}; \Omega)(\mathbf{r})$$

$$\mathcal{S}(\mathbf{u}; \Omega)(\mathbf{r}) \triangleq \int_{\Omega} G(\mathbf{R}) \mathbf{u}(\mathbf{r}') d\mathbf{r}'$$

- ◆ **Select a current based formulation**

- ◆ behaves well for high contrast

$$\lim_{\epsilon_r \rightarrow \infty} \text{JVIE} :$$

$$(\mathcal{I} - \mathcal{N})\mathbf{j} = c_\epsilon \mathbf{e}^{\text{inc}}$$

- ◆ Two possible formulations

- ◆ Second one is naturally pre-conditioned

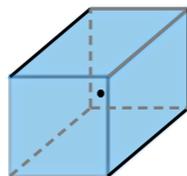
$$\text{JVIE}_{\text{I}} : \quad (\mathcal{M}_{\epsilon_r} - \mathcal{M}_{\chi_\epsilon} \mathcal{N}) \mathbf{j} = c_\epsilon \mathcal{M}_{\chi_\epsilon} \mathbf{e}^{\text{inc}}$$

$$\text{JVIE}_{\text{II}} : \quad (\mathcal{I} - \mathcal{M}_{\tau_\epsilon} \mathcal{N}) \mathbf{j} = c_\epsilon \mathcal{M}_{\tau_\epsilon} \mathbf{e}^{\text{inc}}$$

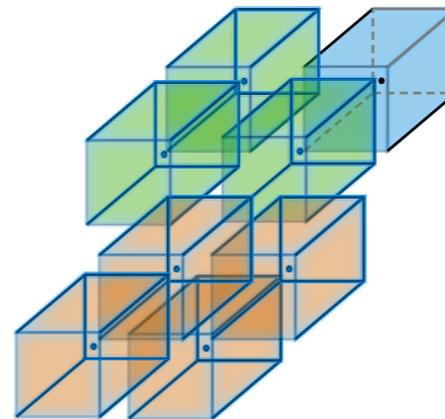
$$\tau_\epsilon = \chi_\epsilon / \epsilon_r$$

- ◆ **Voxel as support**
 - ◆ natural discretization of MRI applications
 - ◆ transform volume integrals into surface
 - ◆ allows to apply FFT based approaches

Toeplitz



Circulant



$$Ax = b$$



*Iterative
Solver*



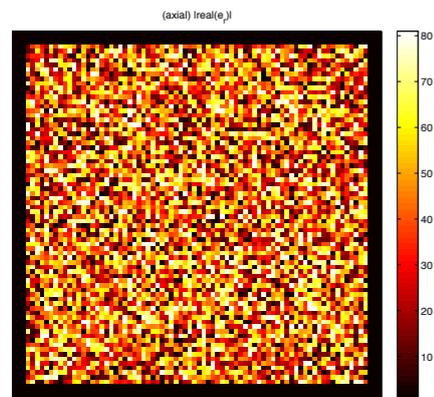
*M-v
product*



*FFT
 $N \log(N)$*

◆ Extremely challenging case

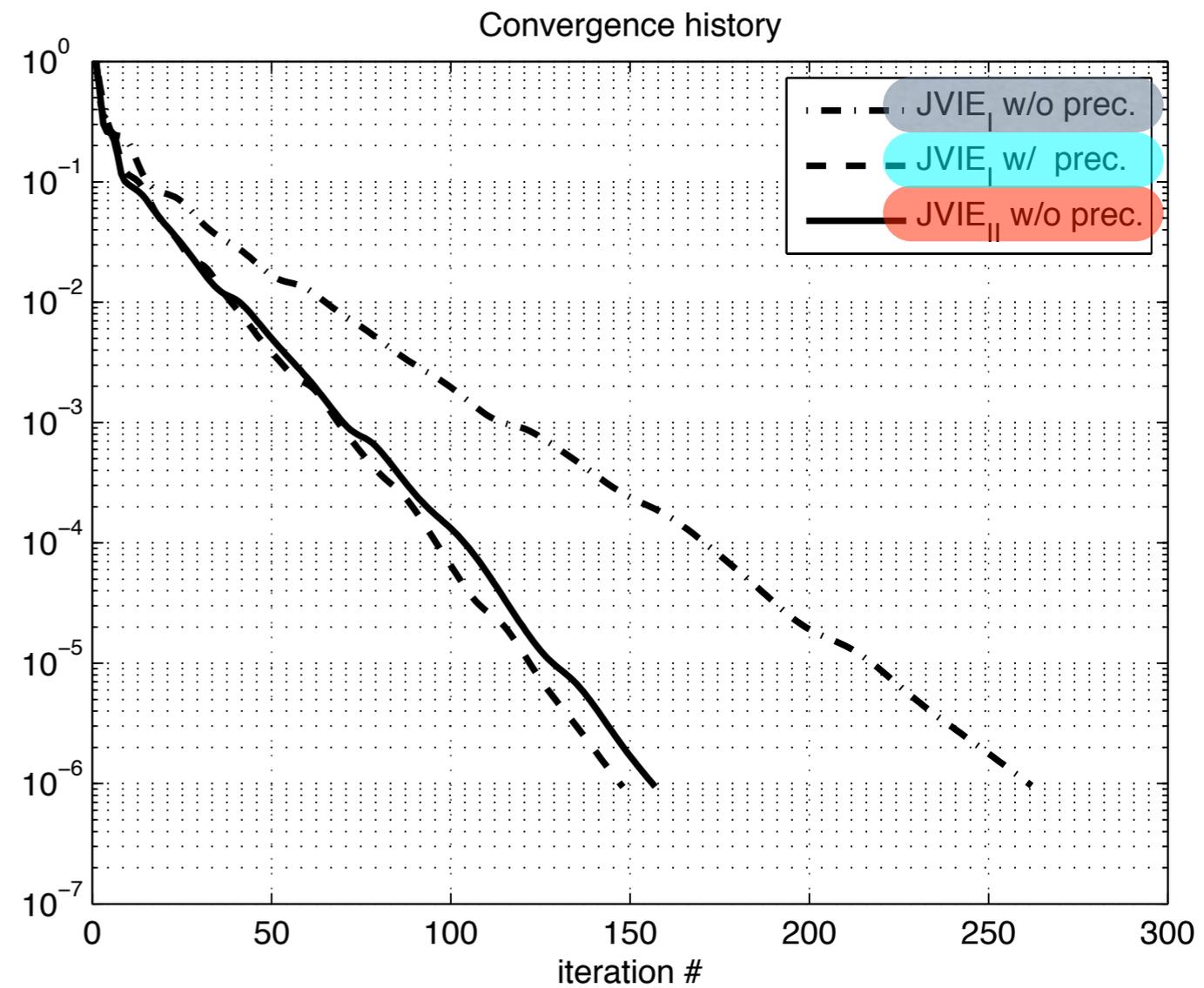
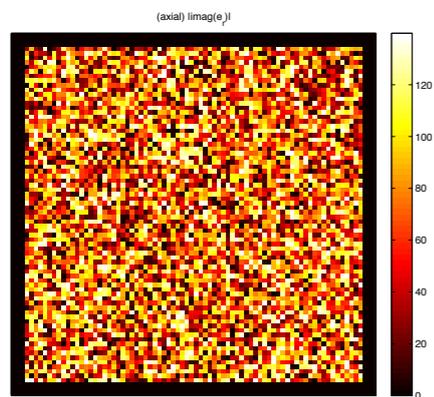
$$1 \leq \text{Re}\{\epsilon_r\} \leq 80$$



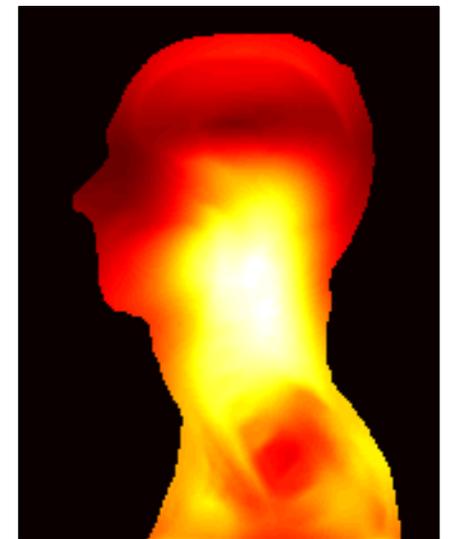
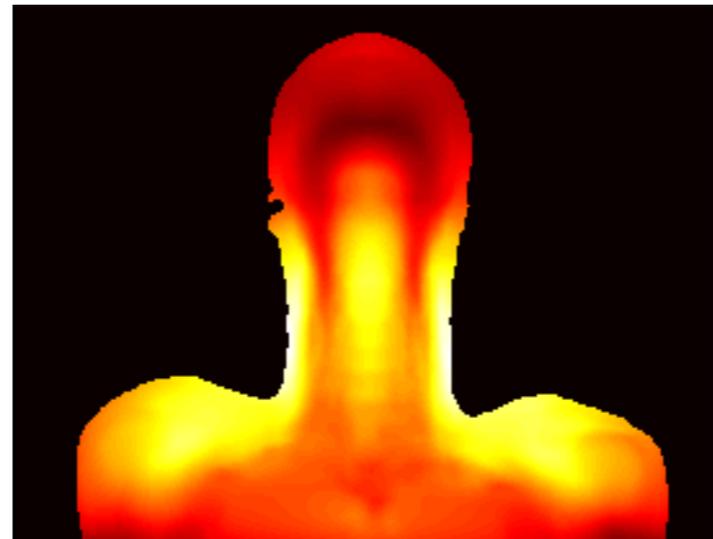
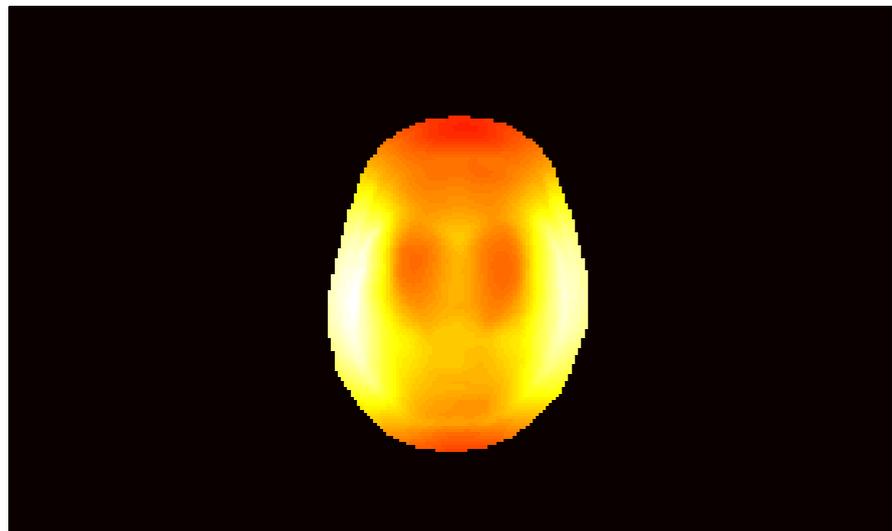
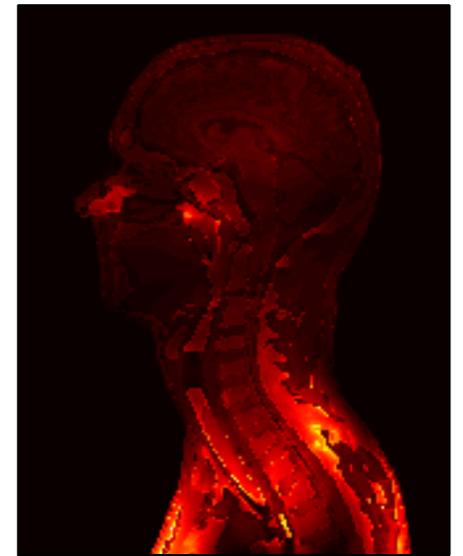
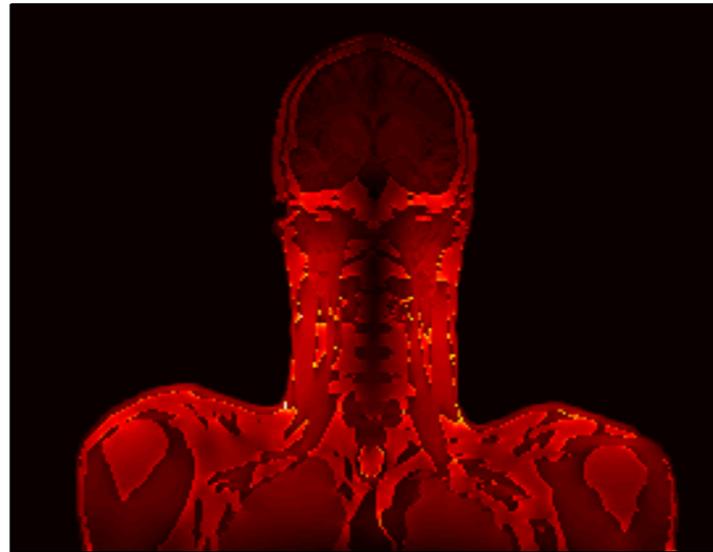
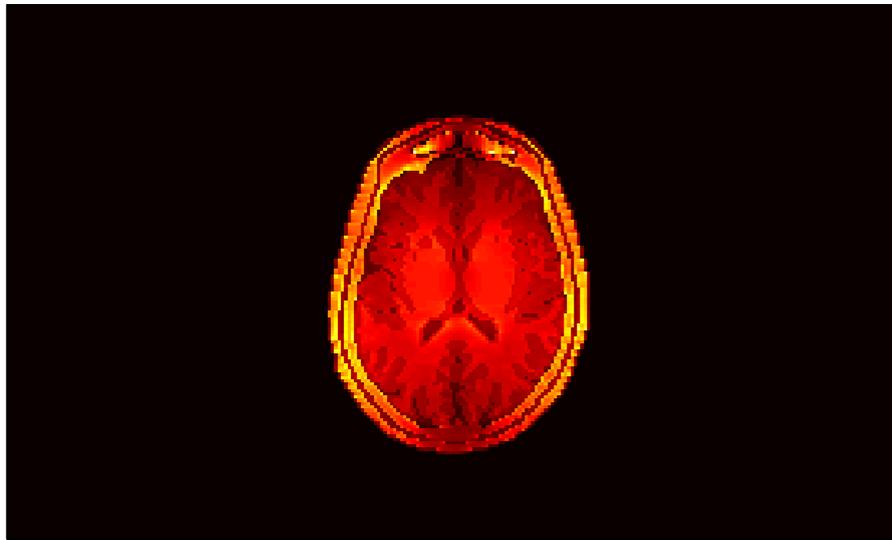
Cube
 $kL = 1$

GMRES

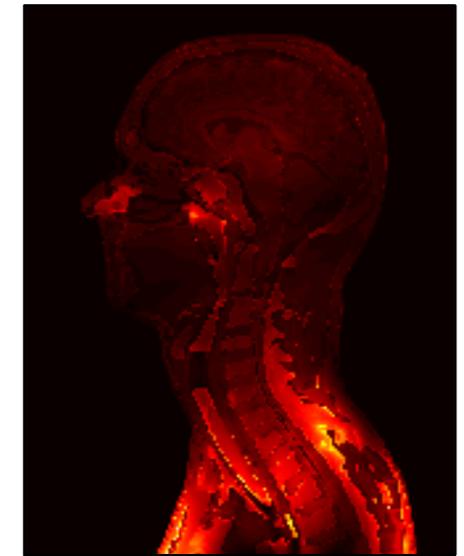
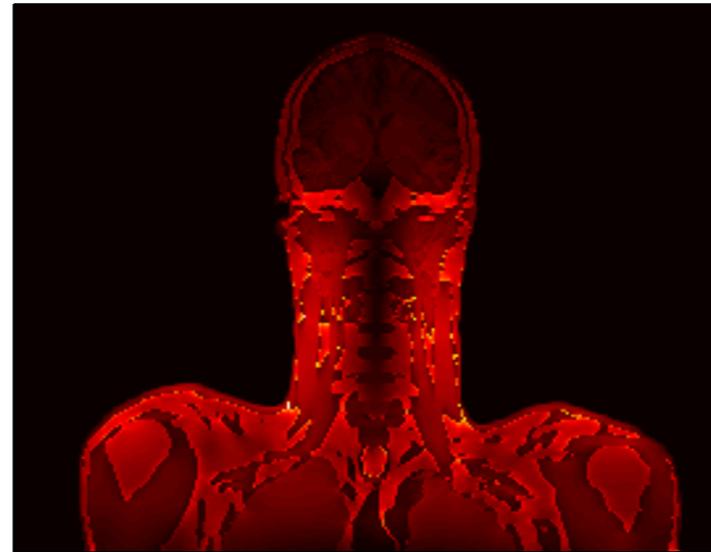
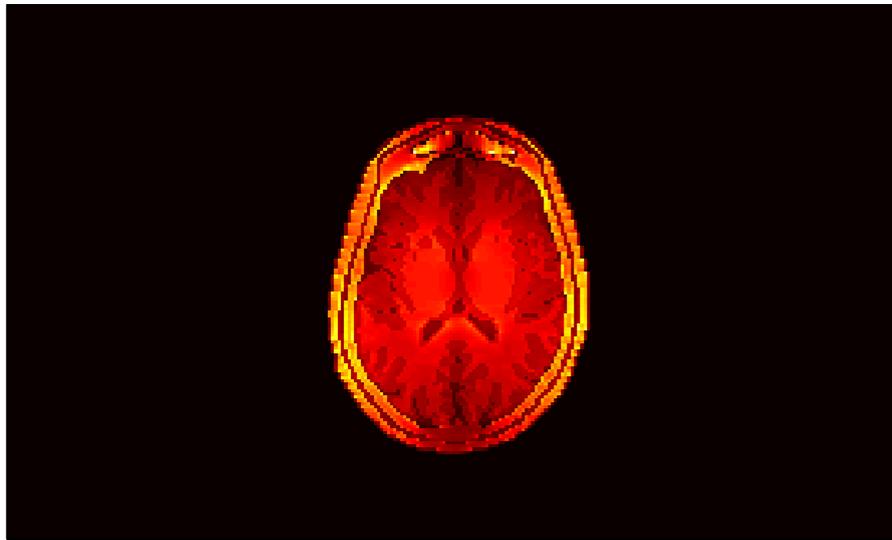
$$0 \leq |\text{Im}\{\epsilon_r\}| \leq 140$$



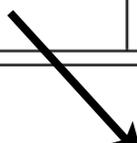
- ◆ Realistic human body model at 7T



◆ Realistic human body model at 7T



		OFFLINE	GMRES	GMRES (40)	GMRES (40,5)	BICG	BICGSTAB	QMR	TFQMR
5mm	Serial	20 s	15 s	15 s	13 s	28 s	16 s	23 s	17s
	Parallel	5 s	7 s	5 s (3 s)	5 s	4 s	3 s	4 s	3 s
	Speed-Up	4×	2.1×	3.0× (5×)	2.6×	7.0×	5.3×	5.7×	5.6×
2.5mm	Serial	146 s	146 s	142 s	125 s	276 s	162 s	266 s	174 s
	Parallel	27 s	65 s	48 s (23 s)	42 s	40 s	25 s	40 s	32 s
	Speed-Up	5.4×	2.2×	2.9× (6.1×)	2.9×	6.9×	6.4×	6.6×	5.4×

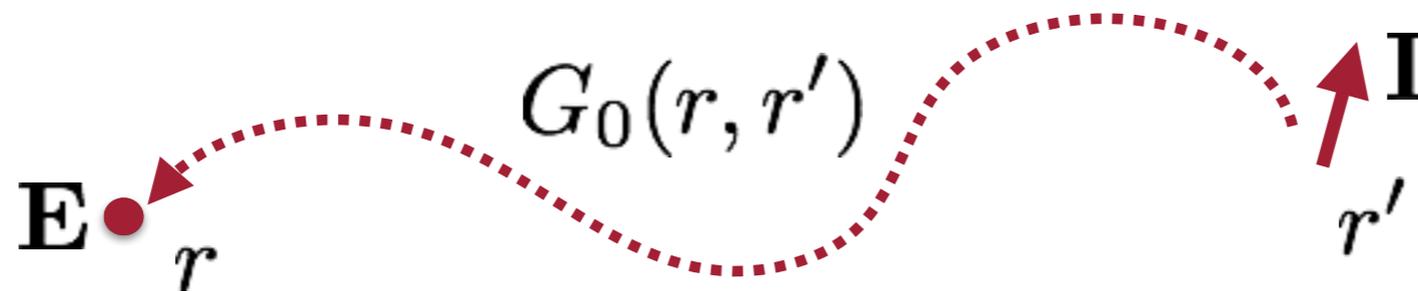


3,000,000 unknowns!

Integral Equation solvers for MRI coil analysis

- ♦ **Green function [2]**

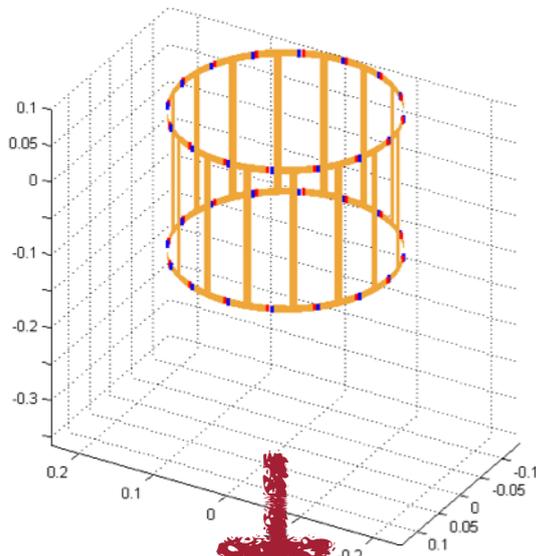
- ♦ gives fundamental solution of the problem at any point
- ♦ satisfies (by definition) radiation conditions (no ABC or PML)



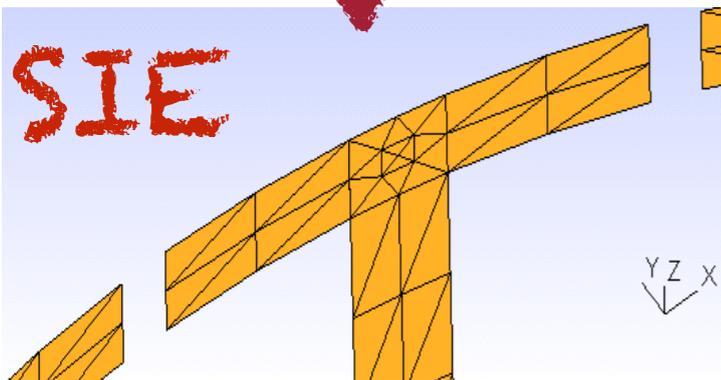
- ◆ **Green function**

- ◆ gives fundamental solution of the problem at any point
- ◆ satisfies (by definition) radiation conditions (no ABC or PML)

- ◆ **At the core of Integral Equation methods**

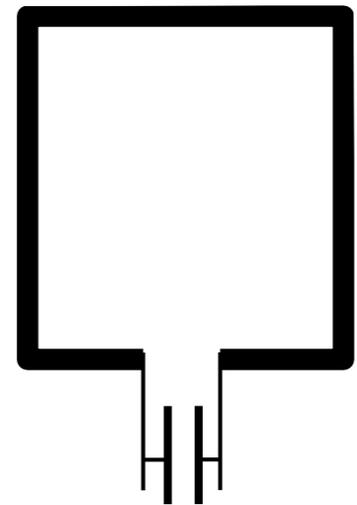
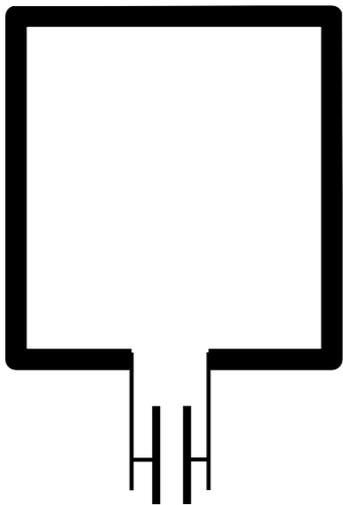


[3]

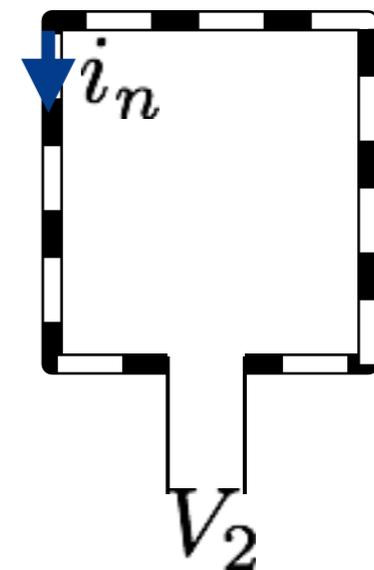
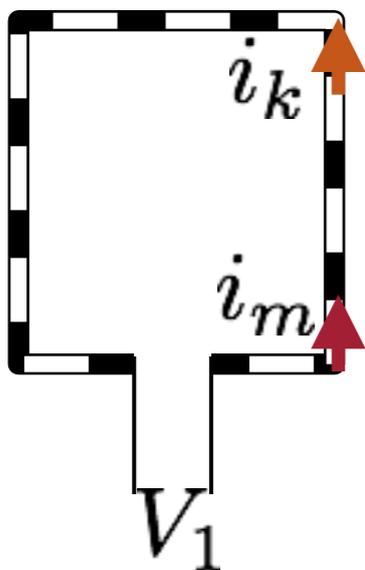


[3] Rao et al., "Electromagnetic scattering by surfaces of arbitrary shape", TAP 1982

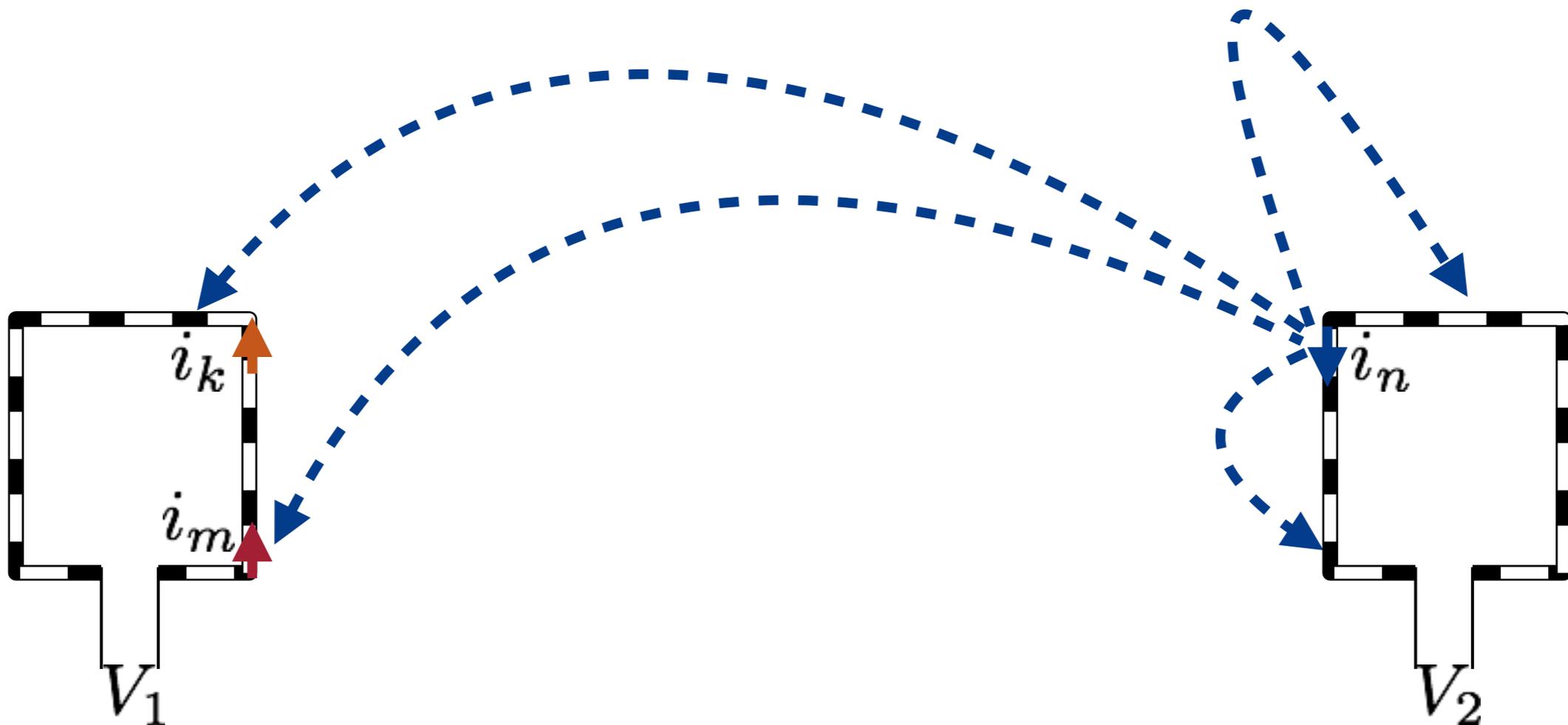
- ◆ **Two homogeneous coils**
 - ◆ free space



- ◆ **Discretize the conductors (not the air)**
 - ◆ connection segments define a port
 - ◆ constant current at each element

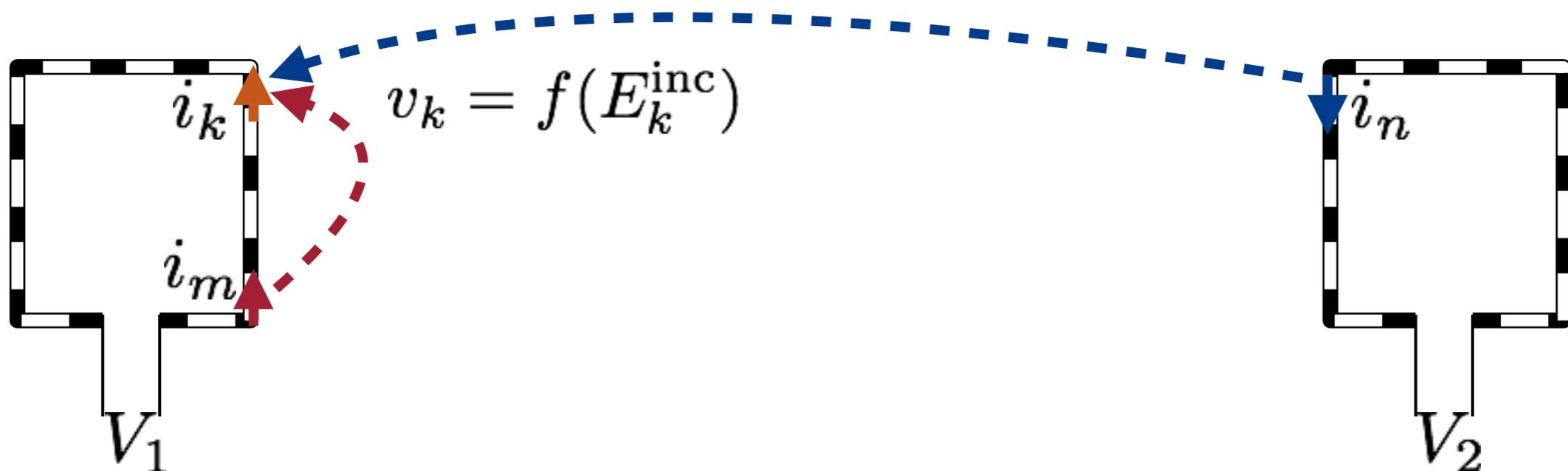


- ◆ **Discretize the conductors (not the air)**
 - ◆ connection segments define a port
 - ◆ constant current at each element
 - ◆ each current radiates a field



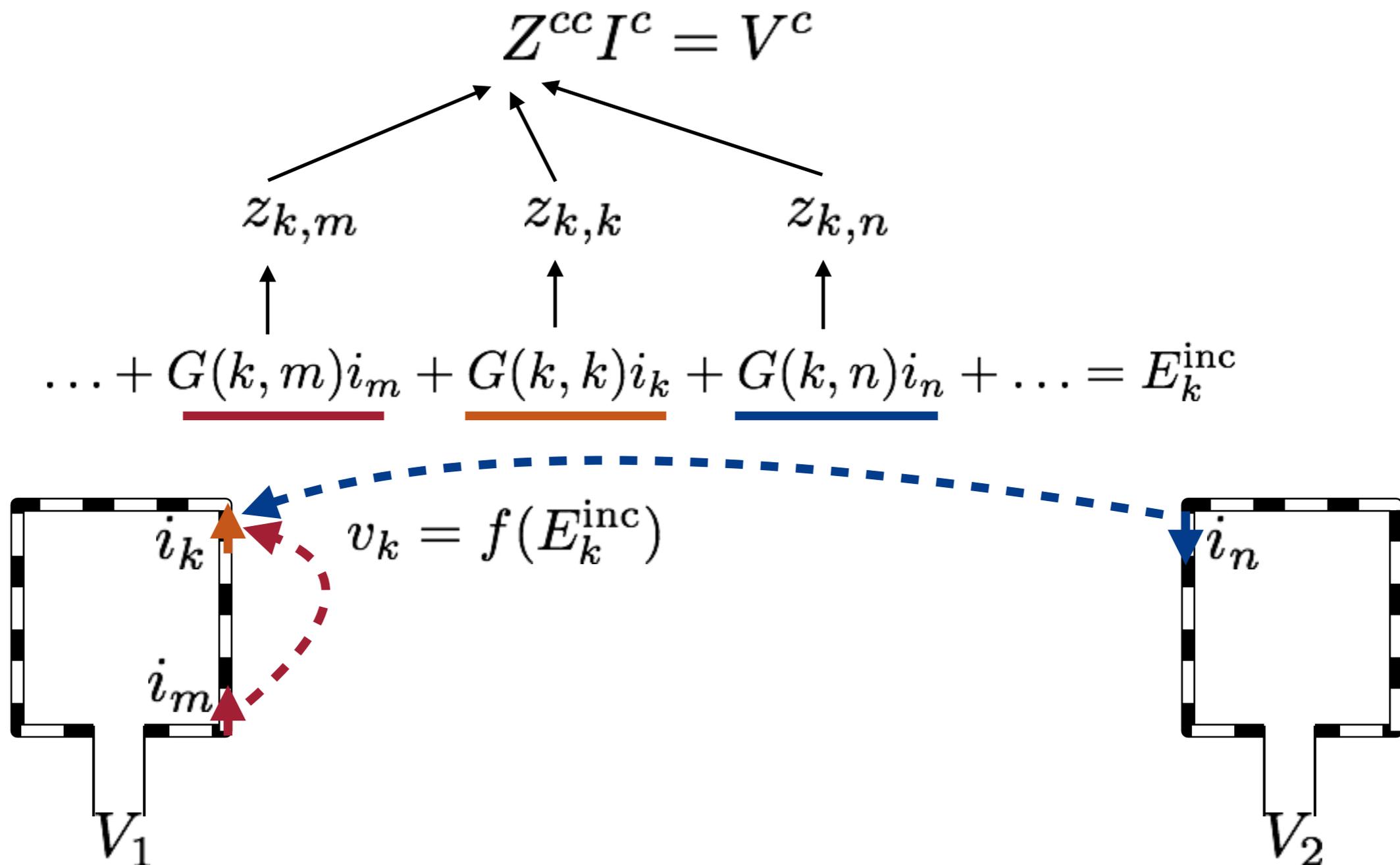
- ◆ **Discretize the conductors (not the air)**
 - ◆ connection segments define a port
 - ◆ constant current at each element
 - ◆ each current radiates a field
 - ◆ field at each element:
 - ◆ contribution from all currents

$$\dots + \underline{G(k, m)}i_m + \underline{G(k, k)}i_k + \underline{G(k, n)}i_n + \dots = E_k^{\text{inc}}$$



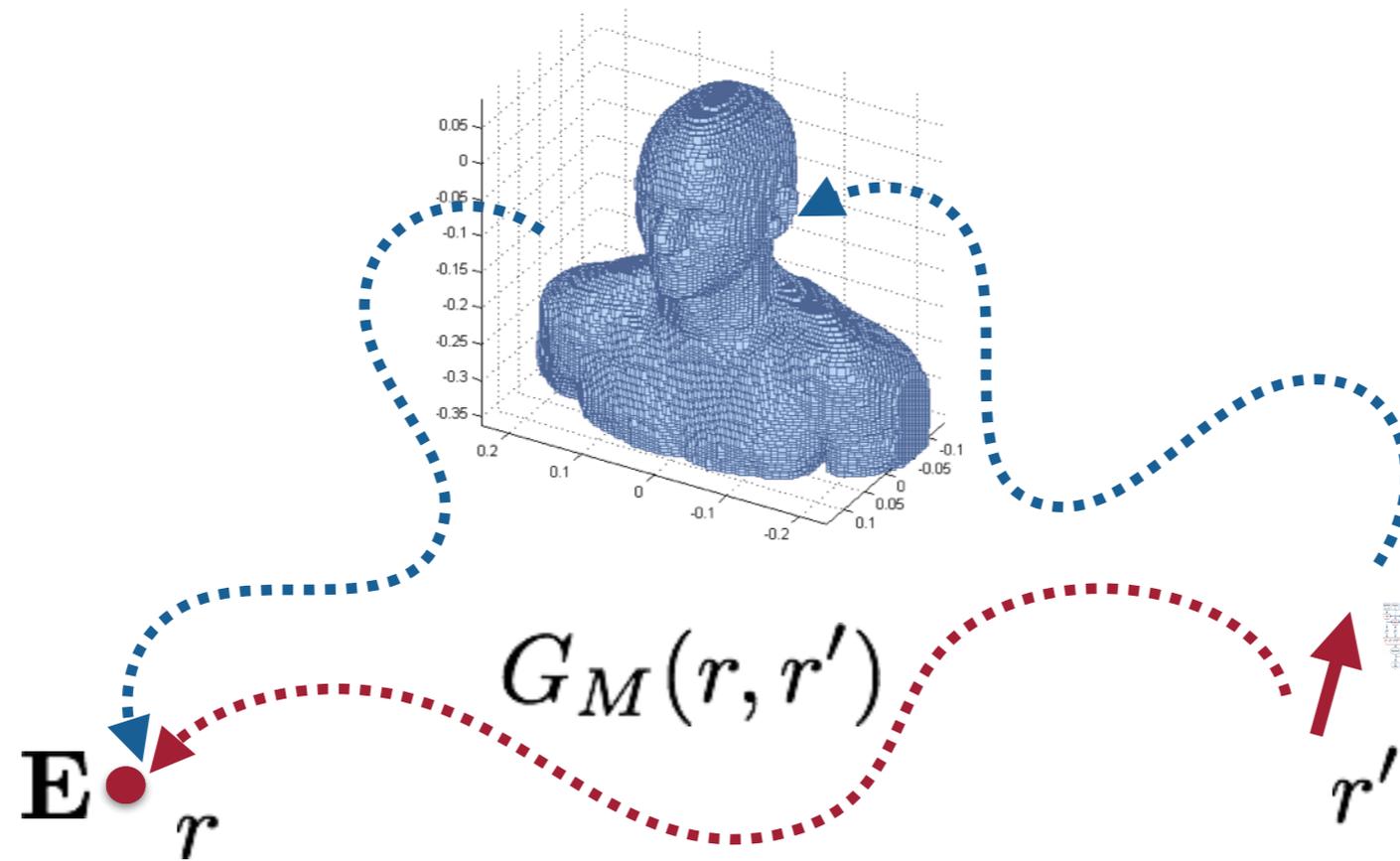
- ◆ **Construct system of equations**

- ◆ relates the variables (currents)
- ◆ external excitations (port voltage)



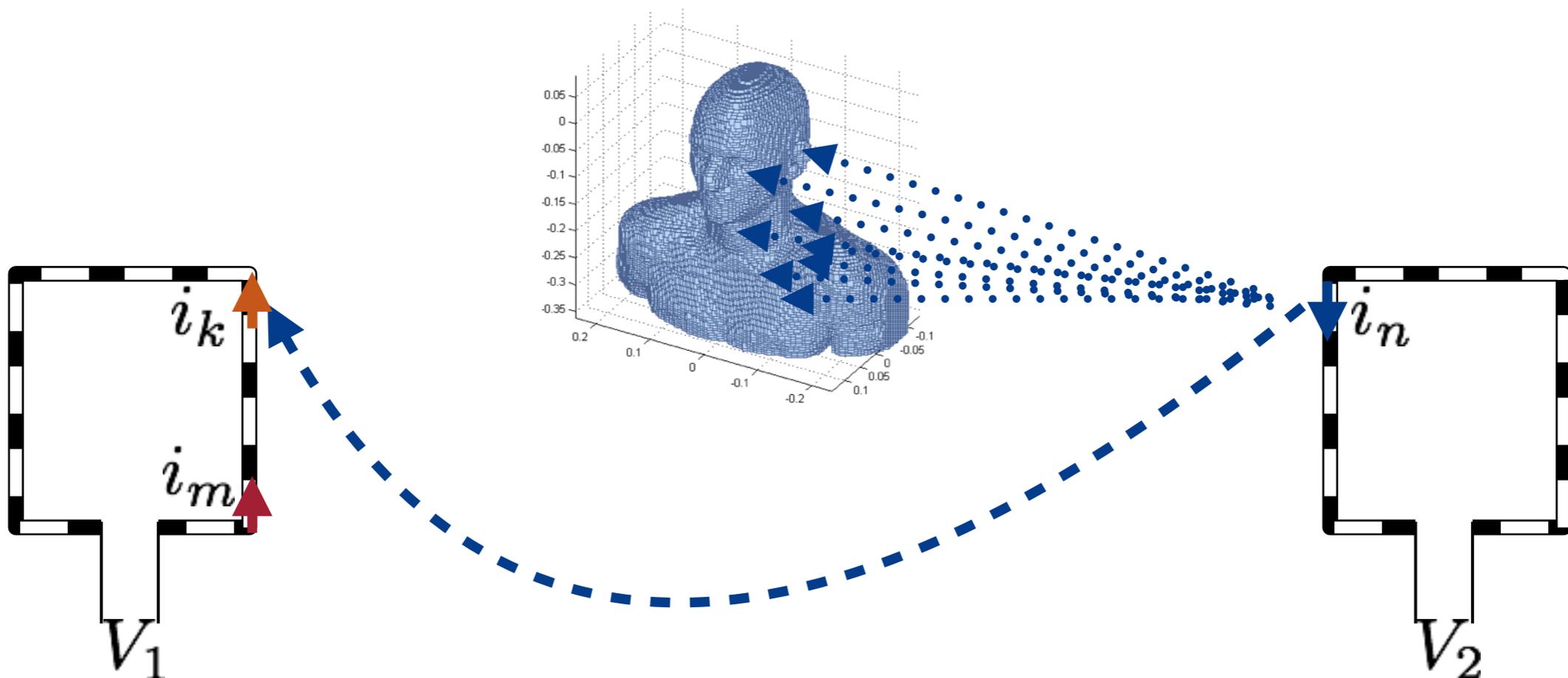
Now...if there is a scatterer?

- ◆ There is a perturbation induced by the body

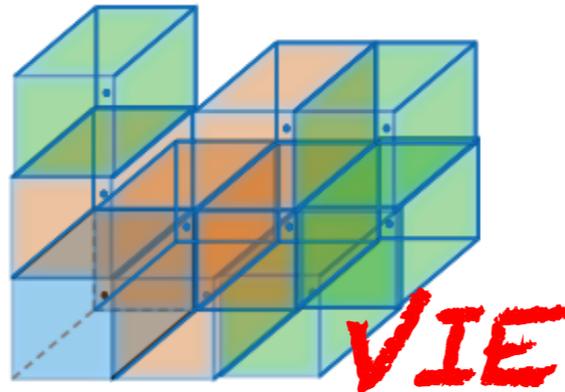


- ◆ There is a perturbation induced by the body

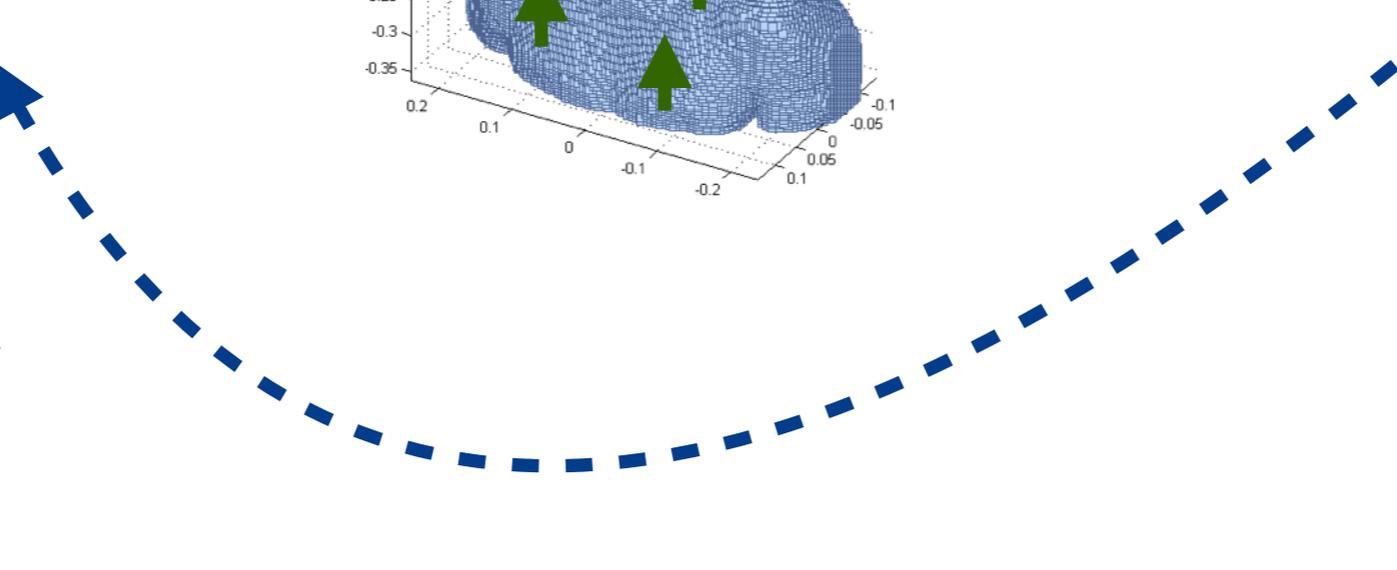
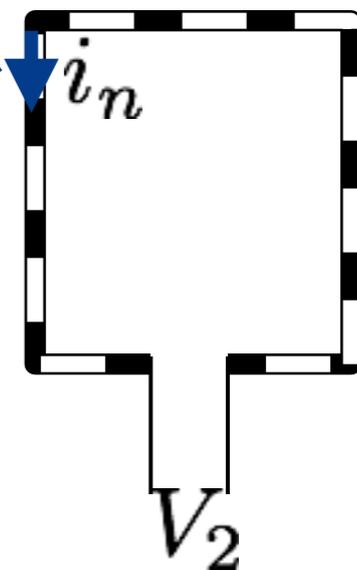
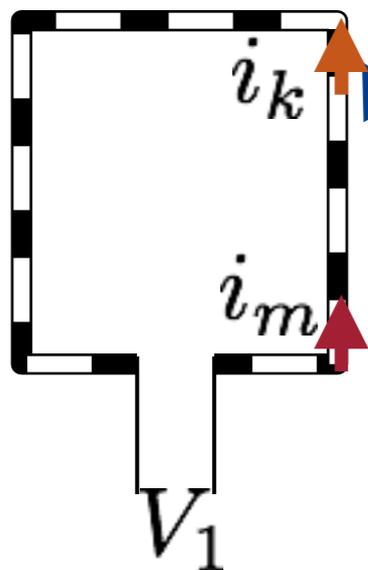
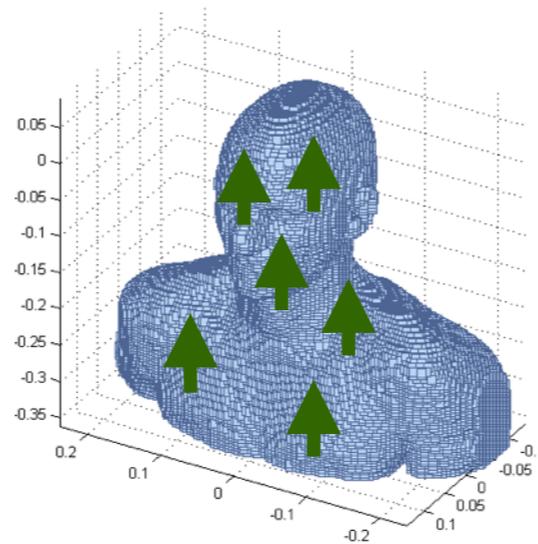
$$E^{\text{inc}} = G(r', r_n) i_n$$



- ◆ There is a perturbation induced by the body

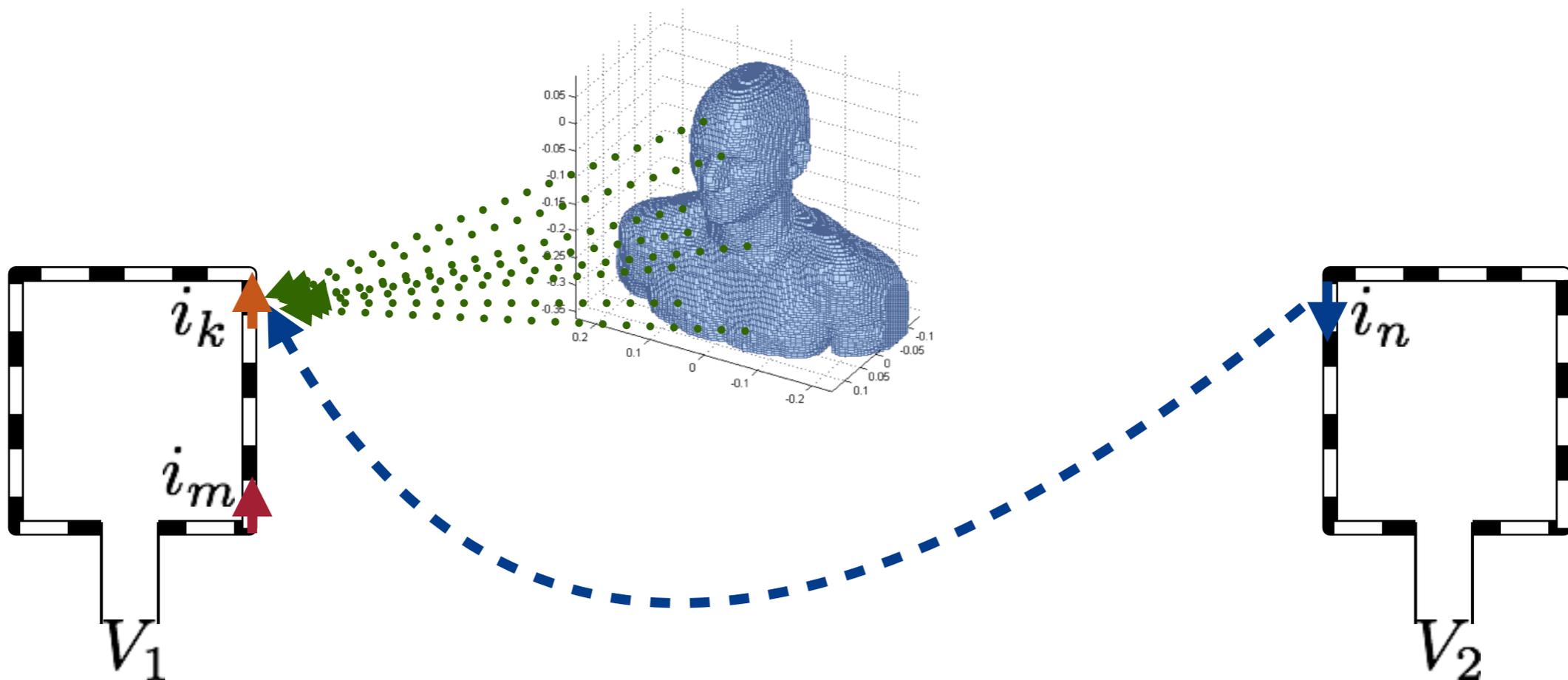


$$J^b = (Z^{bb})^{-1} E^{\text{inc}}$$



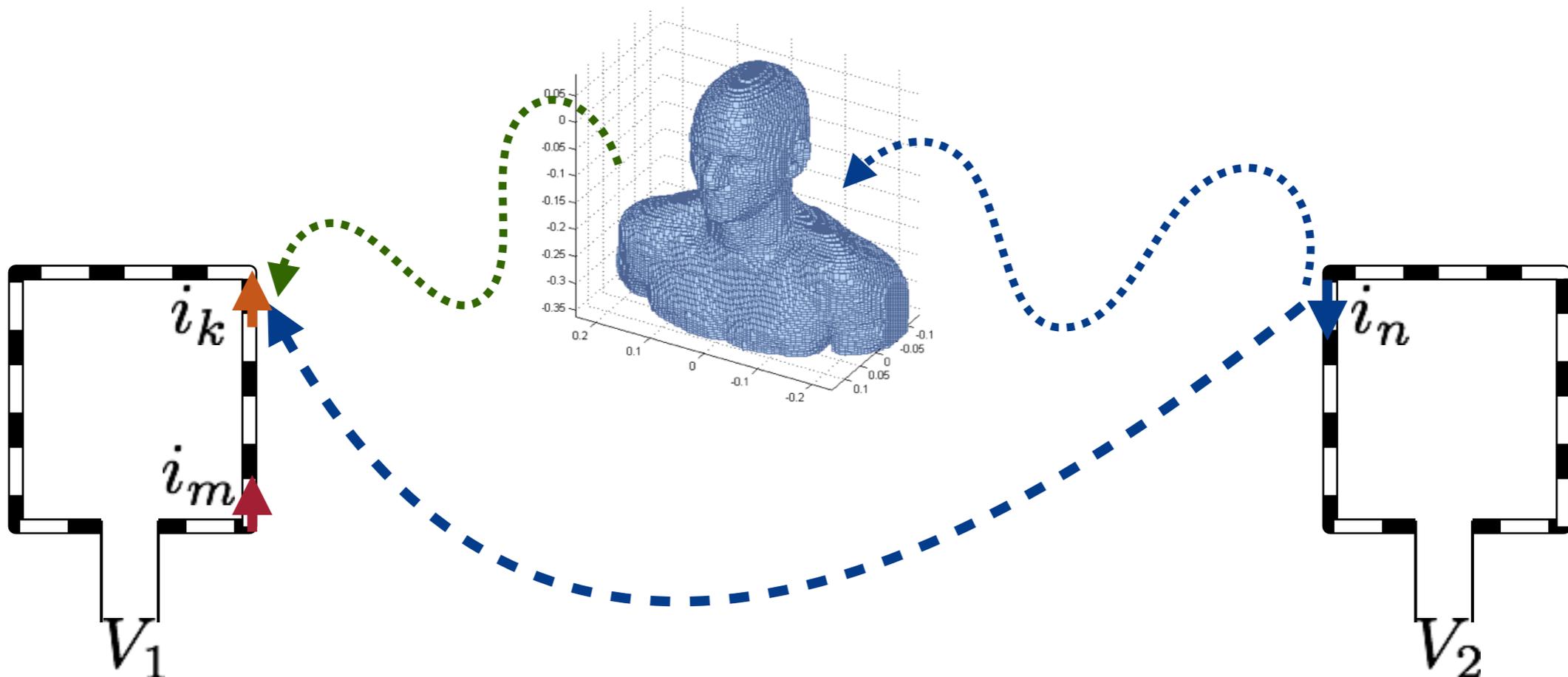
- ◆ There is a perturbation induced by the body

$$E^{\text{inc}} = G(r_k, r') J^b$$



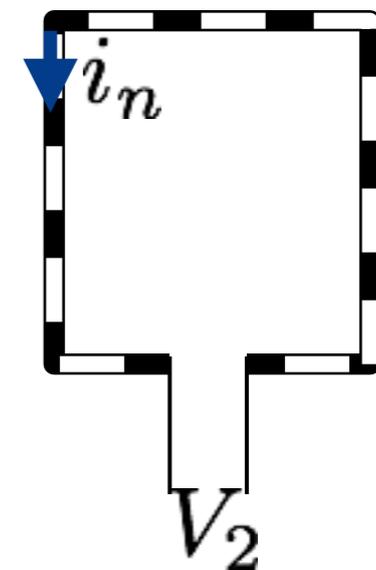
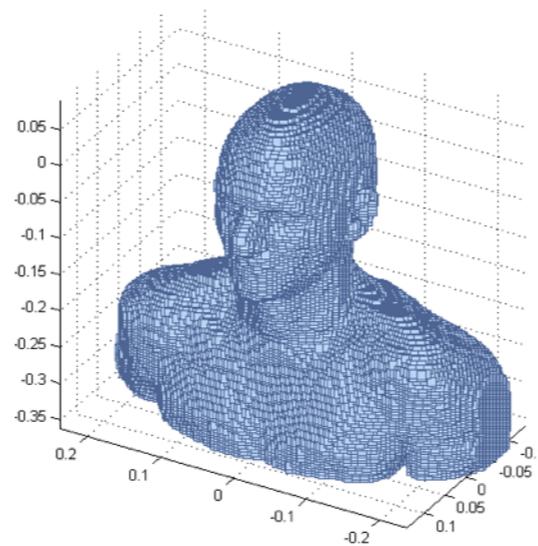
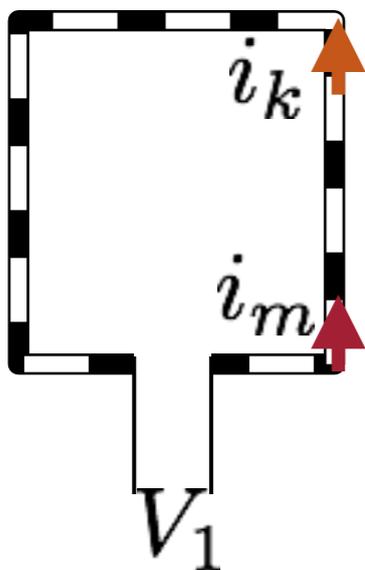
- ◆ **There is a perturbation induced by the body**
 - ◆ total contribution of elements is direct+scattered

$$E_k^{\text{inc}} = G(k, n)i_n + G(k, r')(Z^{bb})^{-1}G(r', n)i_n$$

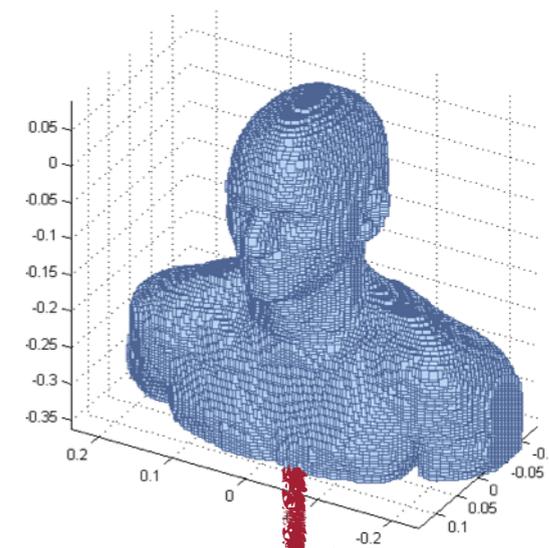
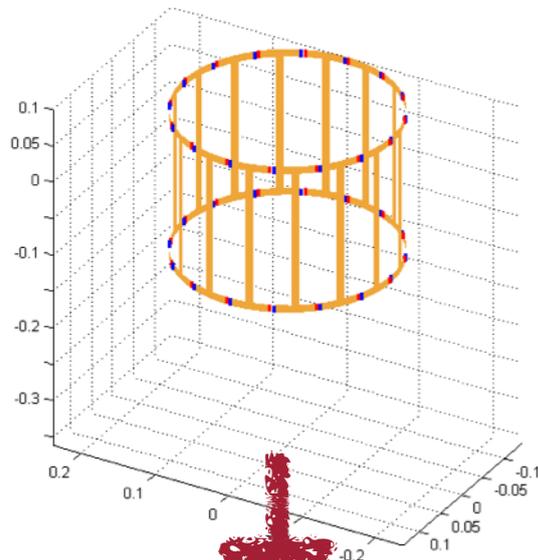


- ◆ **There is a perturbation induced by the body**
 - ◆ total contribution of elements is direct+scattered
 - ◆ assemble total system

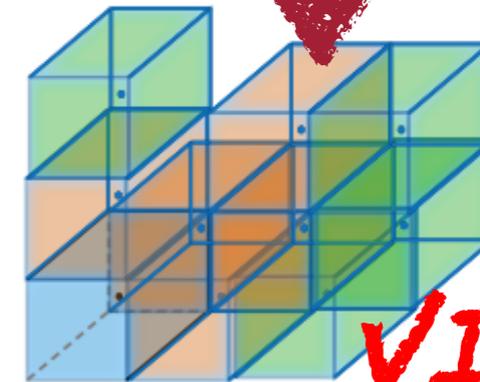
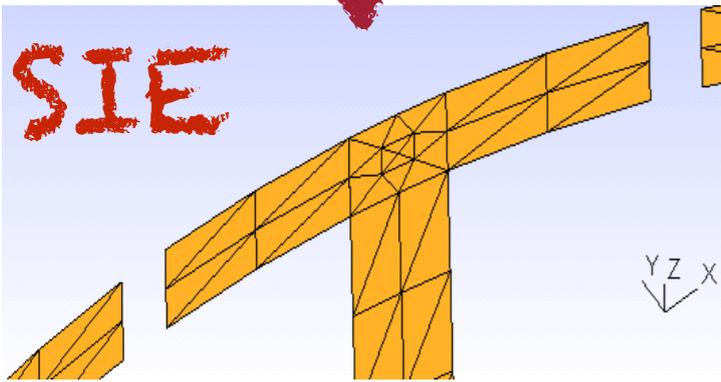
$$\left(Z^{cc} - Z^{cb} (Z^{bb})^{-1} Z^{cb} \right) I^c = V^c$$



- ◆ **SIE for coils and VIE for body model**



[3]

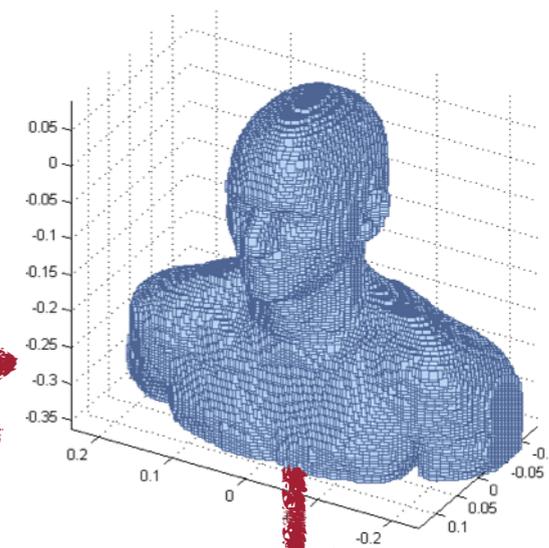
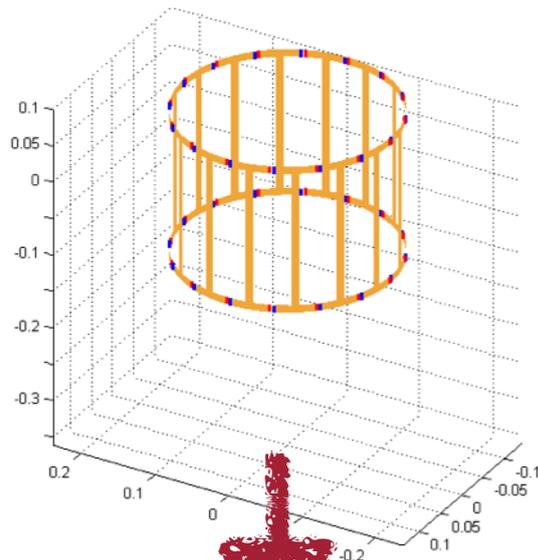


[4]

[3] Rao et al., "Electromagnetic scattering by surfaces of arbitrary shape", **TAP 1982**

[4] Polimeridis et al., "Stable FFT-JVIE solvers for fast analysis of highly inhomogeneous dielectric objects", **JCP 2014**

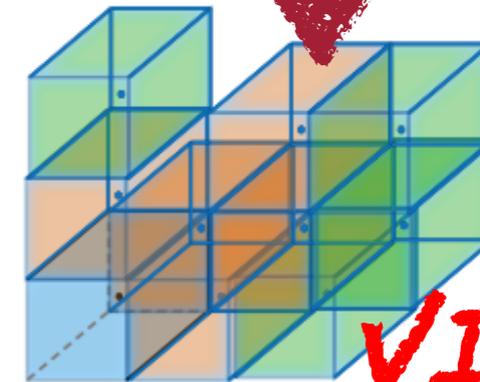
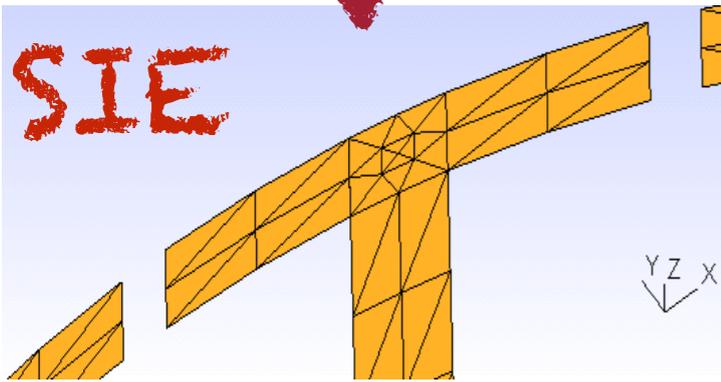
- ◆ **SIE for coils and VIE for body model**
 - ◆ Coupling is done via free-space Green function
 - ◆ Superposition + linearity: seamlessly combination



Coupling



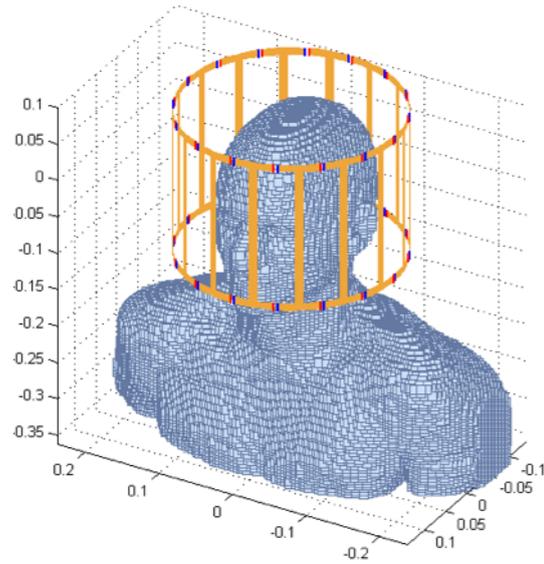
[3]



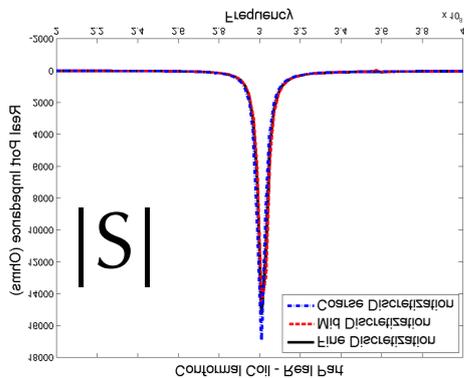
VIE [4]

[3] Rao et al., "Electromagnetic scattering by surfaces of arbitrary shape", **TAP 1982**

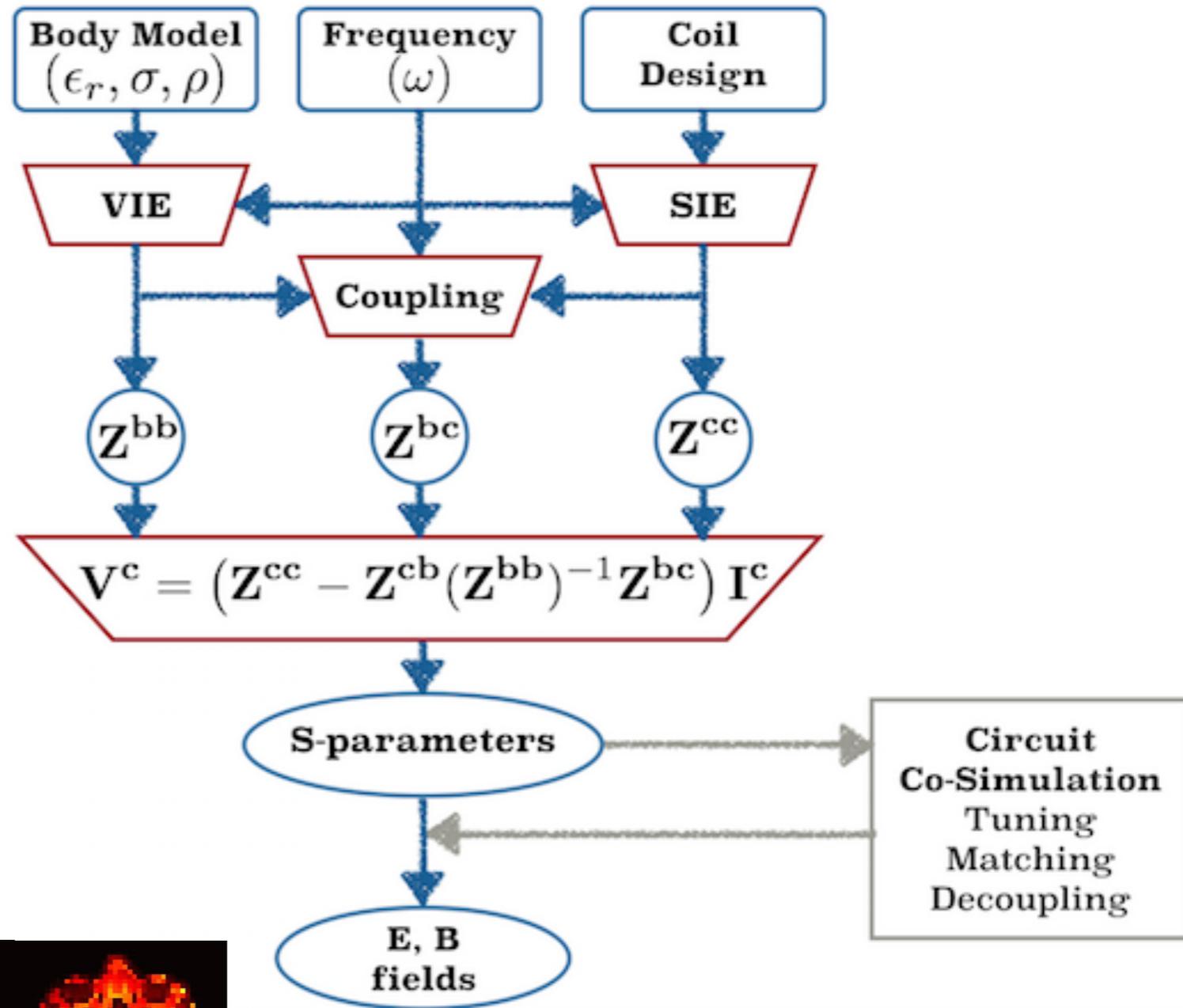
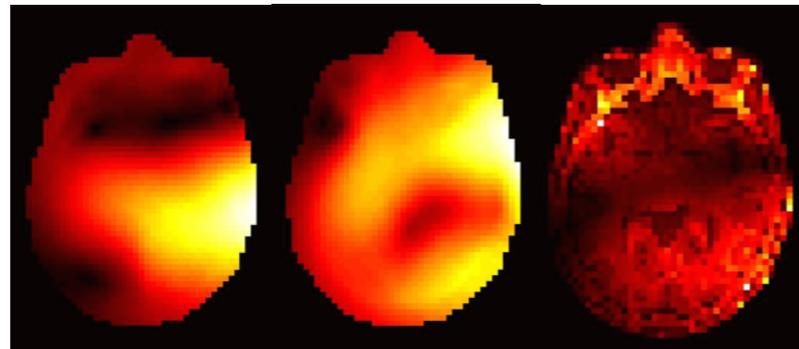
[4] Polimeridis et al., "Stable FFT-JVIE solvers for fast analysis of highly inhomogeneous dielectric objects", **JCP 2014**



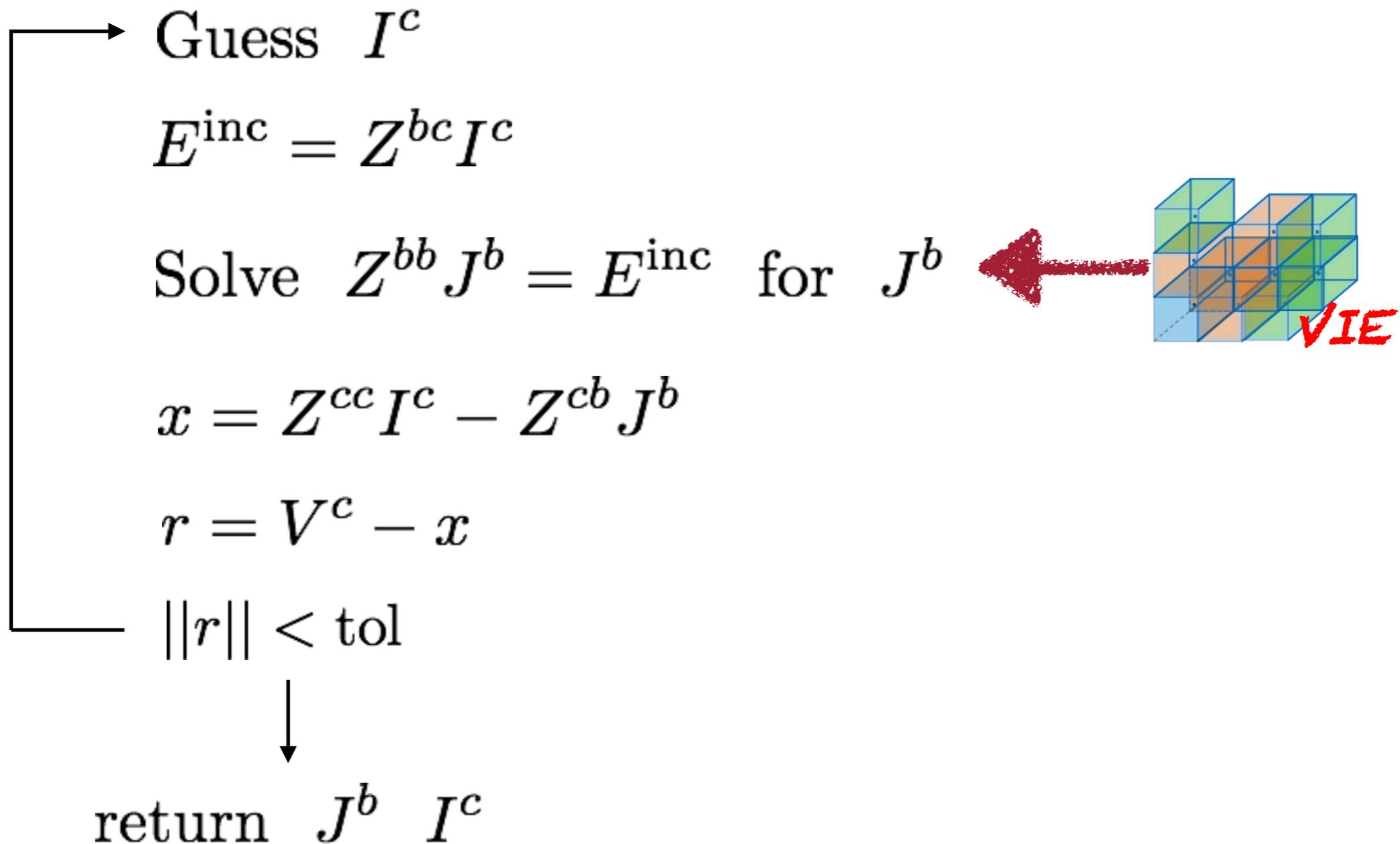
**Full-wave EM
Integral Equation Solver**



&

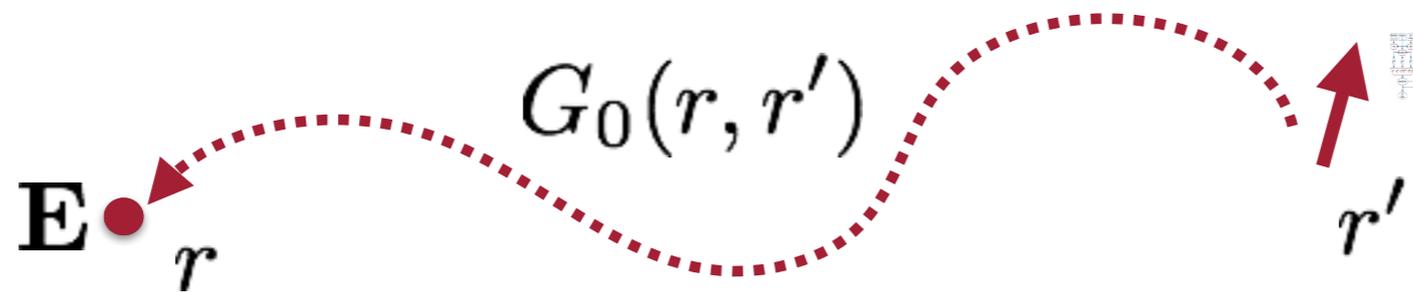


- ♦ Two level iterative solver $(Z^{cc} - Z^{cb}(Z^{bb})^{-1}Z^{cb})I^c = V^c$

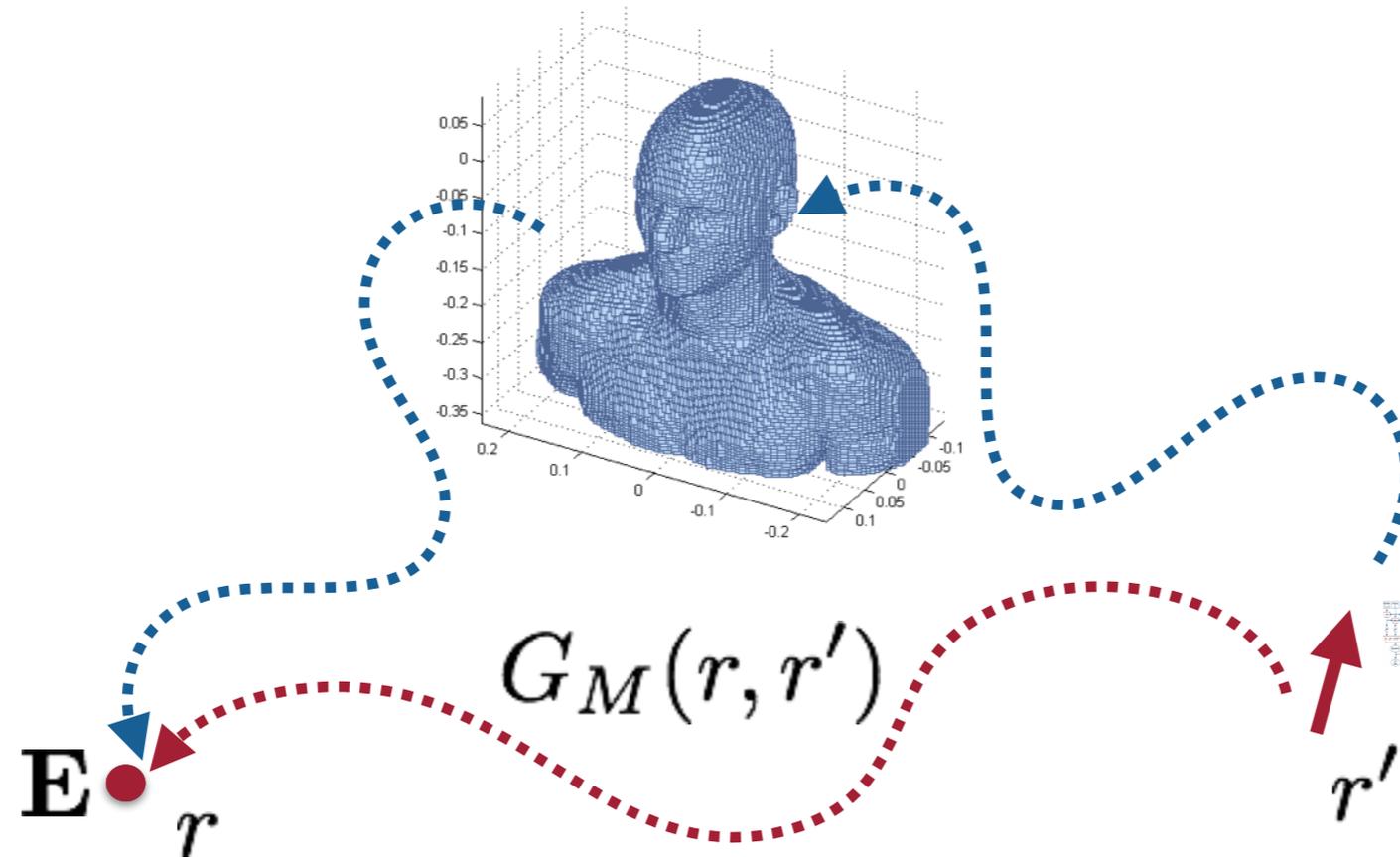


Basis for the EM fields in realistic body models

- ◆ **Free space Green function**
 - ◆ fundamental solution of the problem at any point

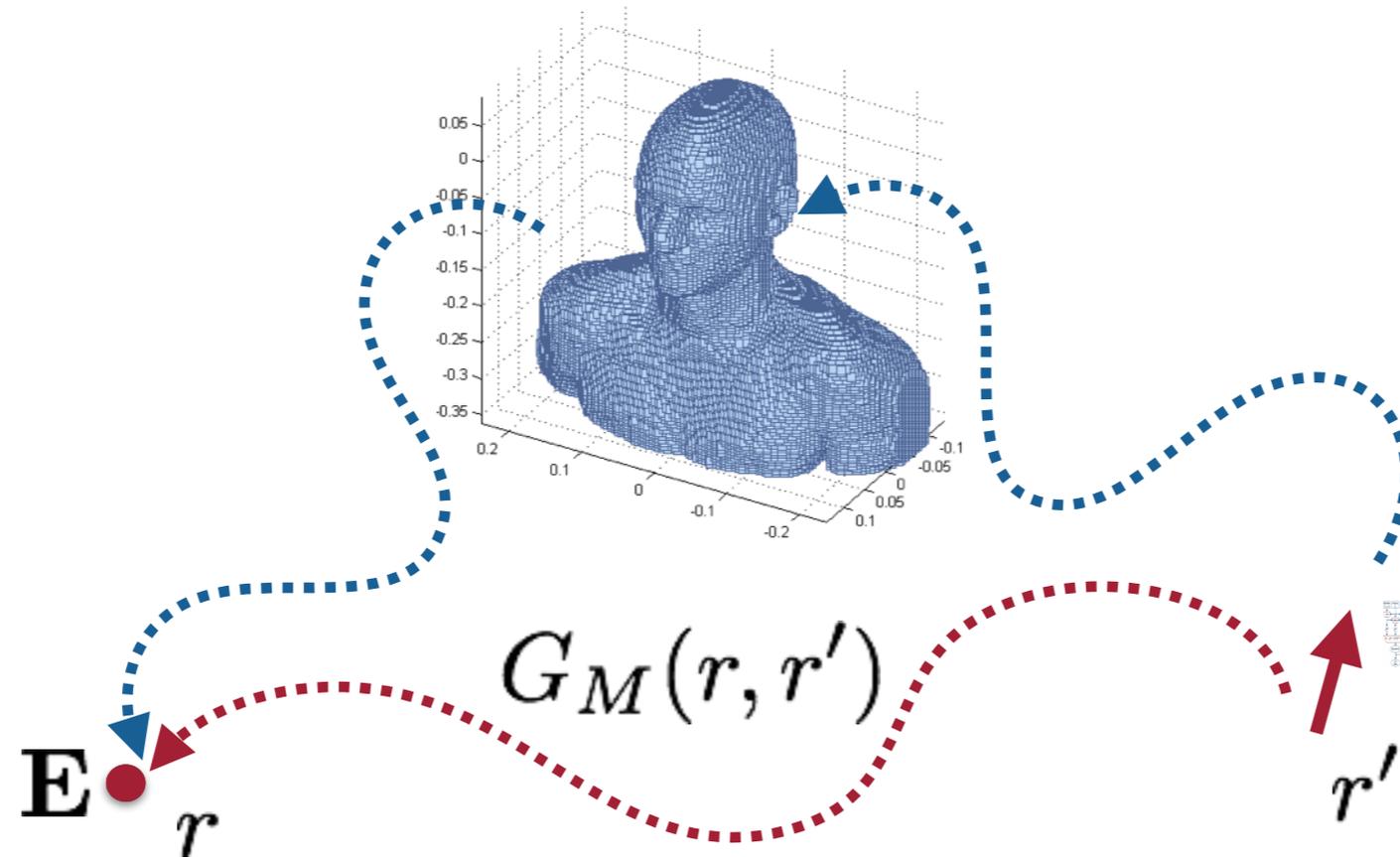


- ◆ **Magnetic Resonance Green function**
 - ◆ fundamental solution of body scattering problem at any point



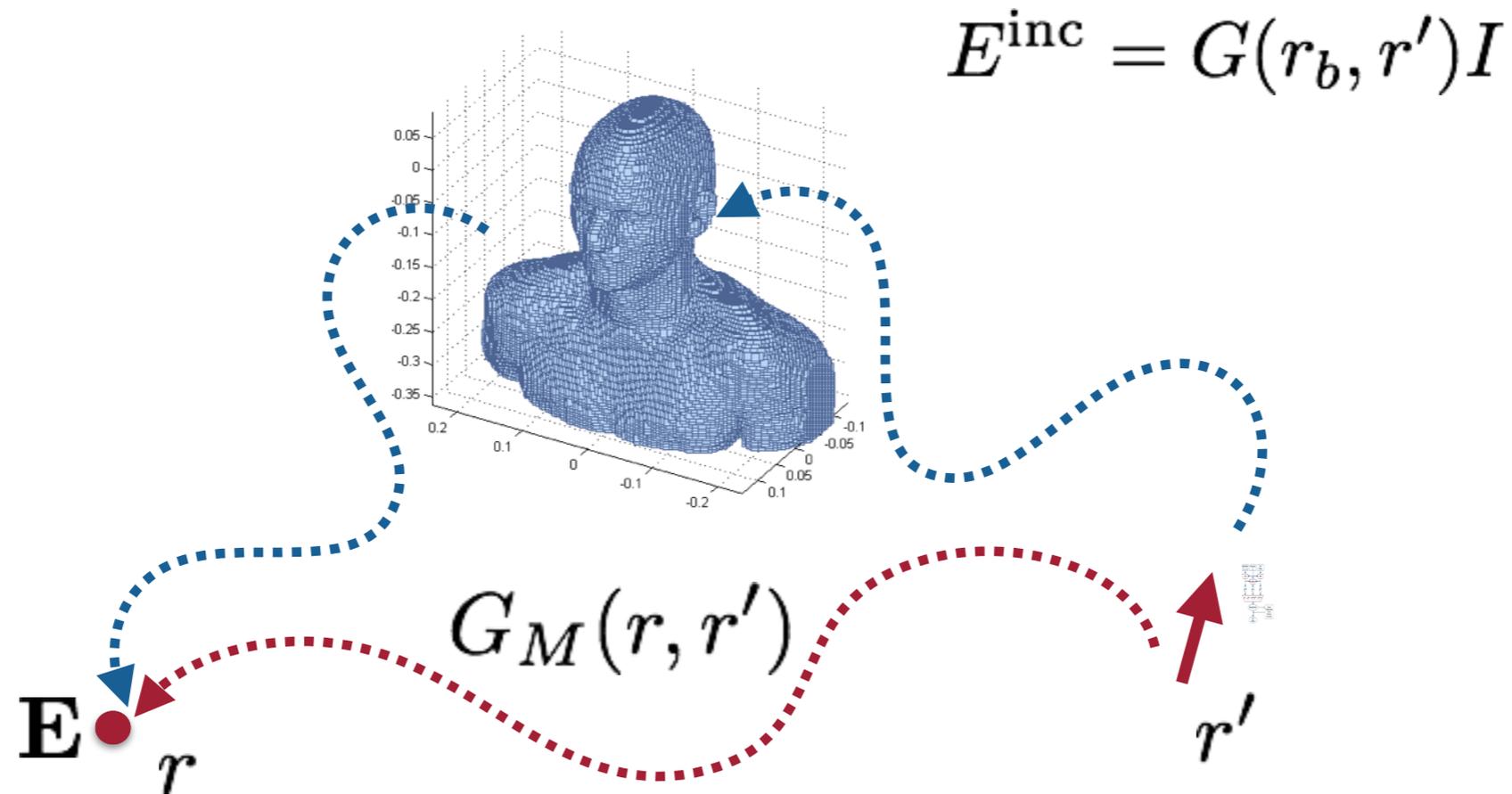
- ◆ **Realistic human body model: too complex**
 - ◆ How to get an analytical function?

- ◆ **Magnetic Resonance Green function**
 - ◆ fundamental solution of body scattering problem at any point

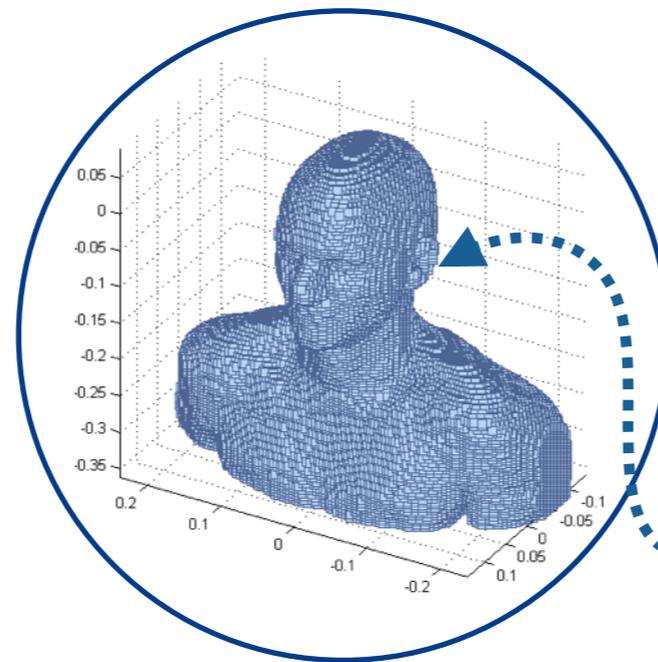


- ◆ **Realistic human body model: too complex**
 - ◆ **Numerical Pre-computation!**
 - ◆ **Solution at any point due to any excitation**

- ◆ How to explore all possibilities?



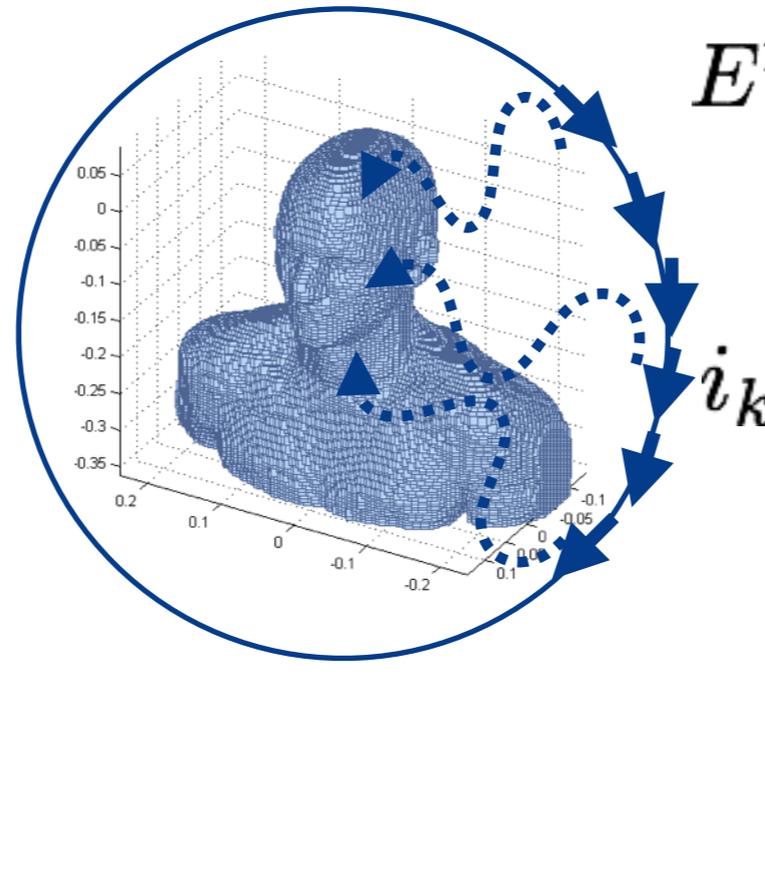
- ◆ Surface enclosing the scatterer



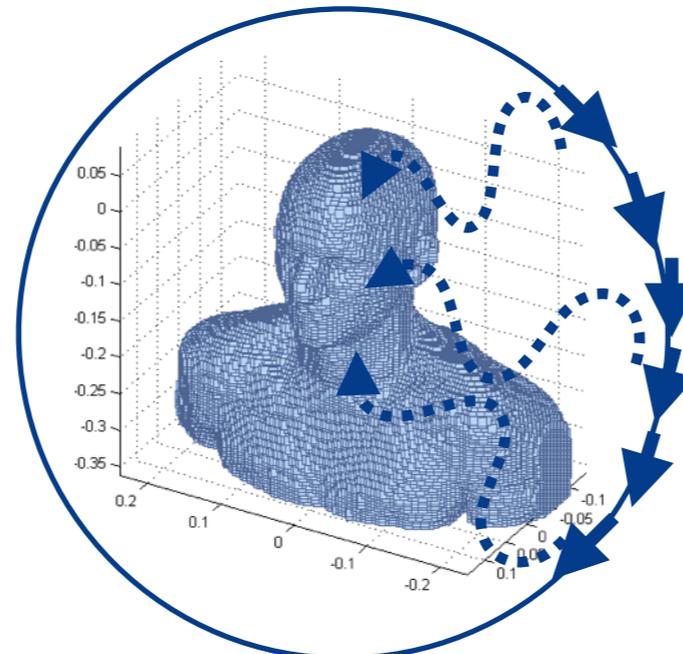
$$E^{\text{inc}} = G(r_b, r')I$$



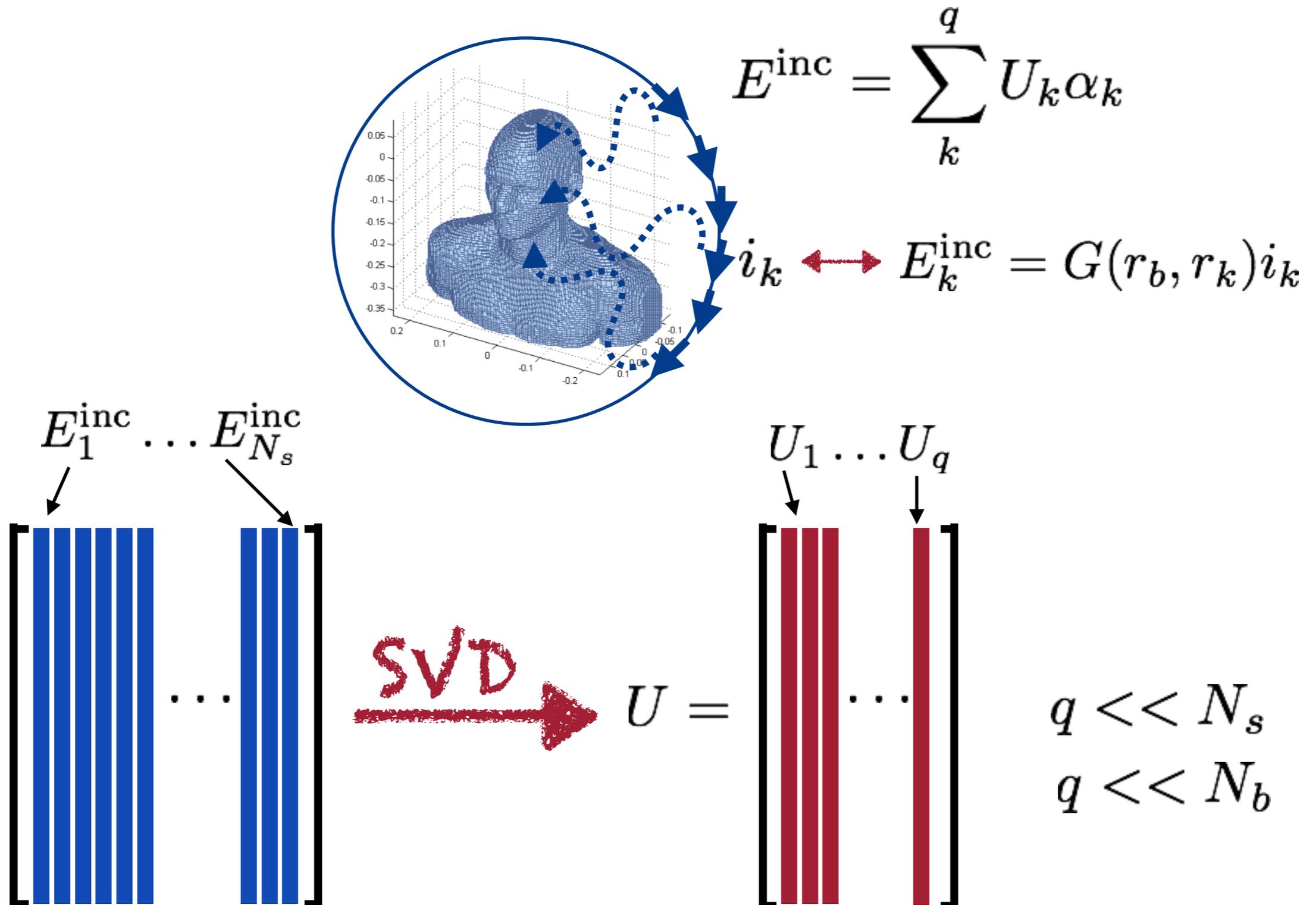
- ◆ Fields from (combination of effect of) currents on the surface


$$E^{\text{inc}} = \sum_k^{N_s} G(r_b, r_k) i_k \alpha_k$$

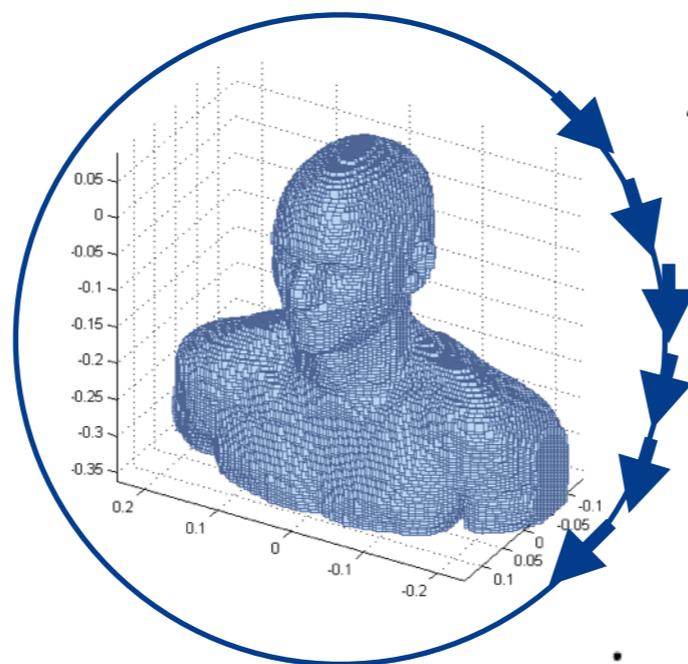
- ◆ Fields from (incident fields due to) currents on the surface


$$E^{\text{inc}} = \sum_k^{N_s} E_k^{\text{inc}} \alpha_k$$
$$i_k \longleftrightarrow E_k^{\text{inc}} = G(r_b, r_k) i_k$$

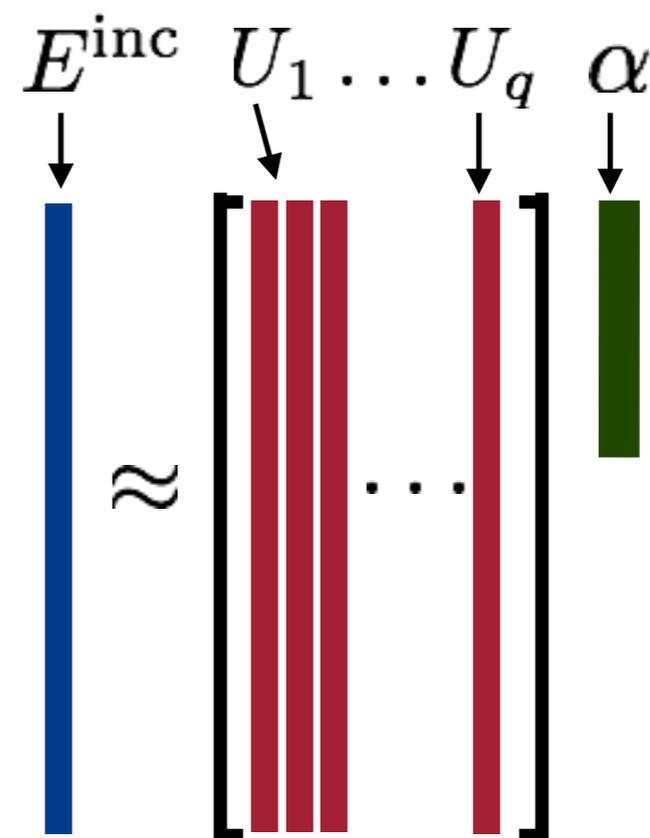
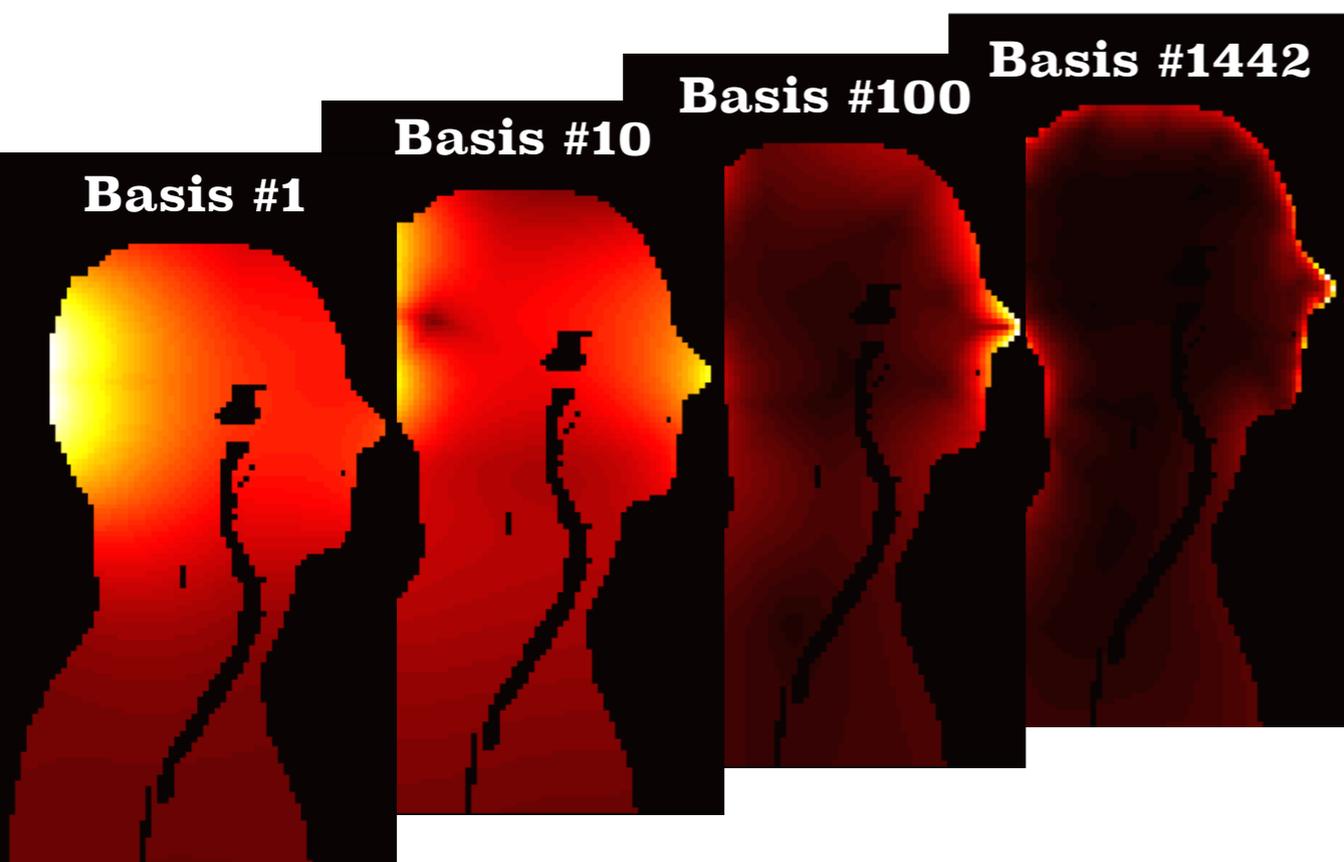

- ◆ Find a basis for the incident fields



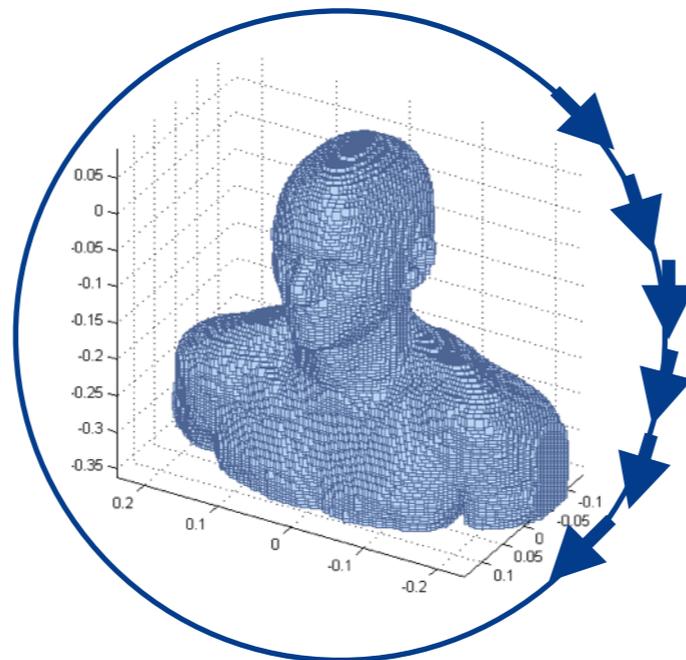
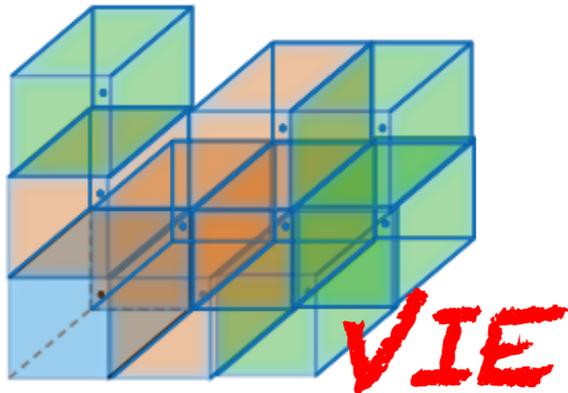
- ◆ Incident field approximated by basis



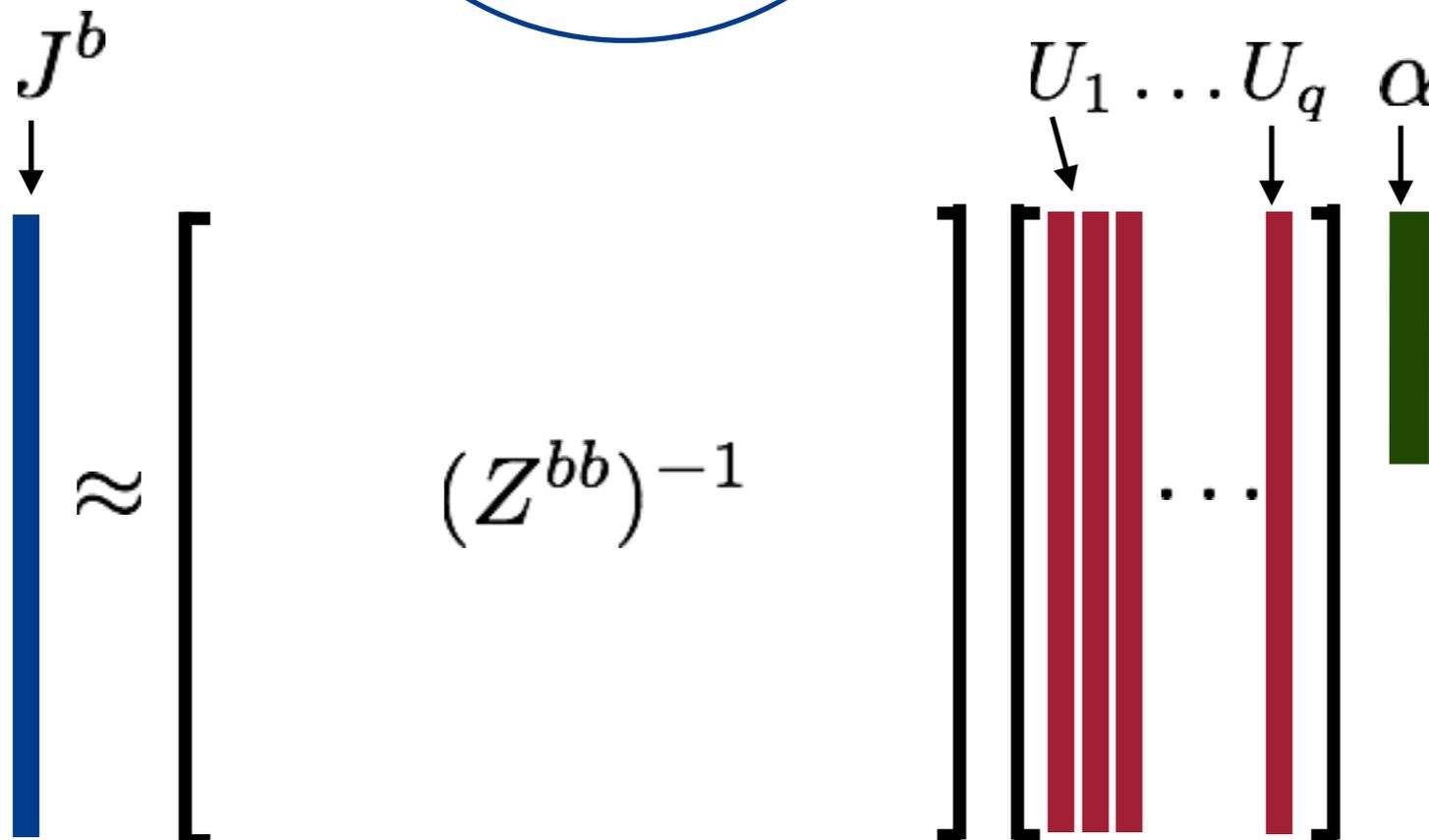
$$E^{\text{inc}} = \sum_k^q U_k \alpha_k$$



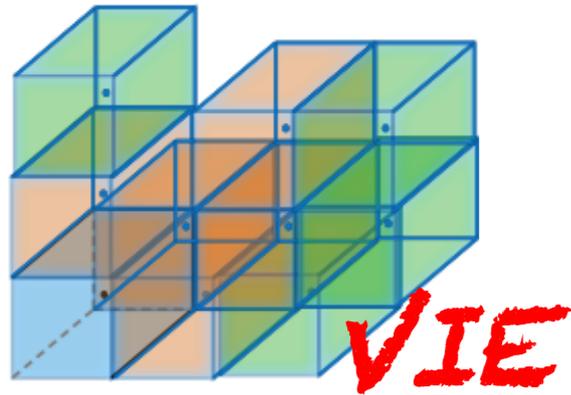
- ◆ Pre-compute the VIE solution



$$J^b = (Z^{bb})^{-1} E^{\text{inc}}$$

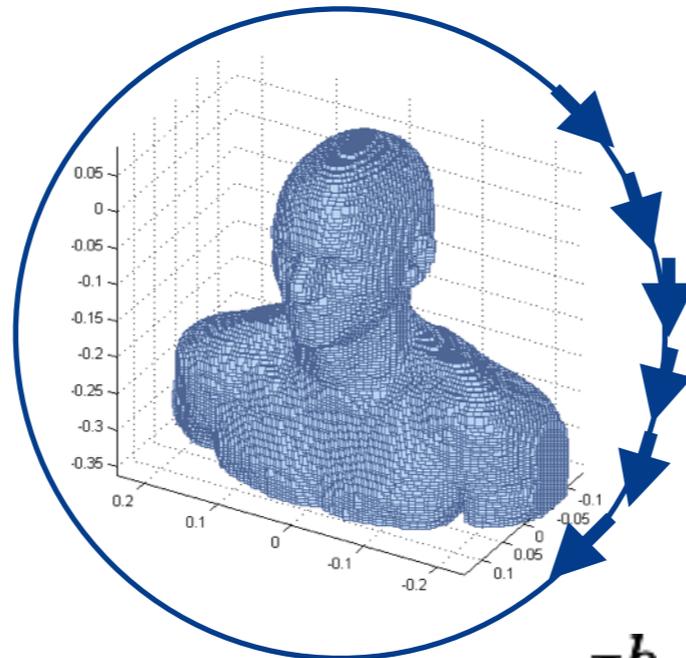


- ◆ Pre-compute the VIE solution for each vector in basis

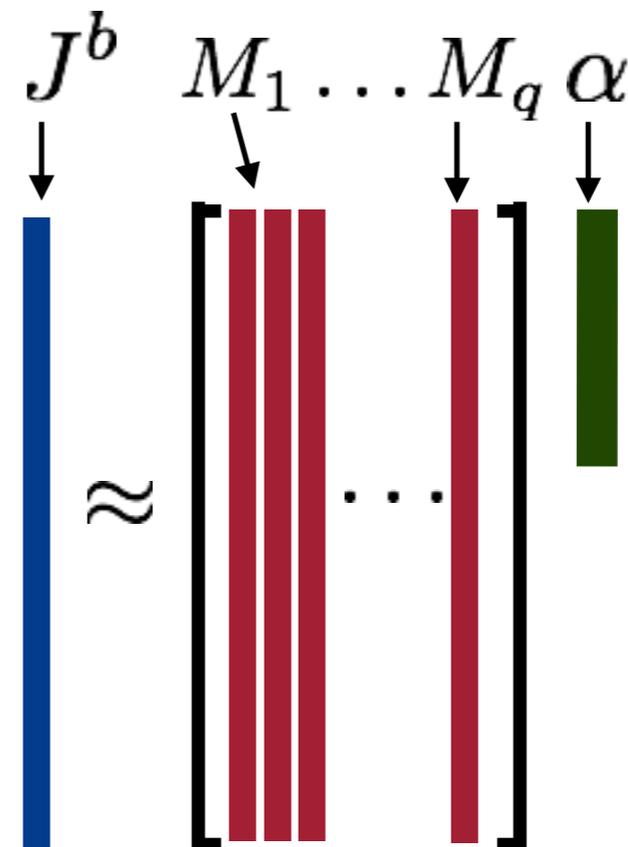
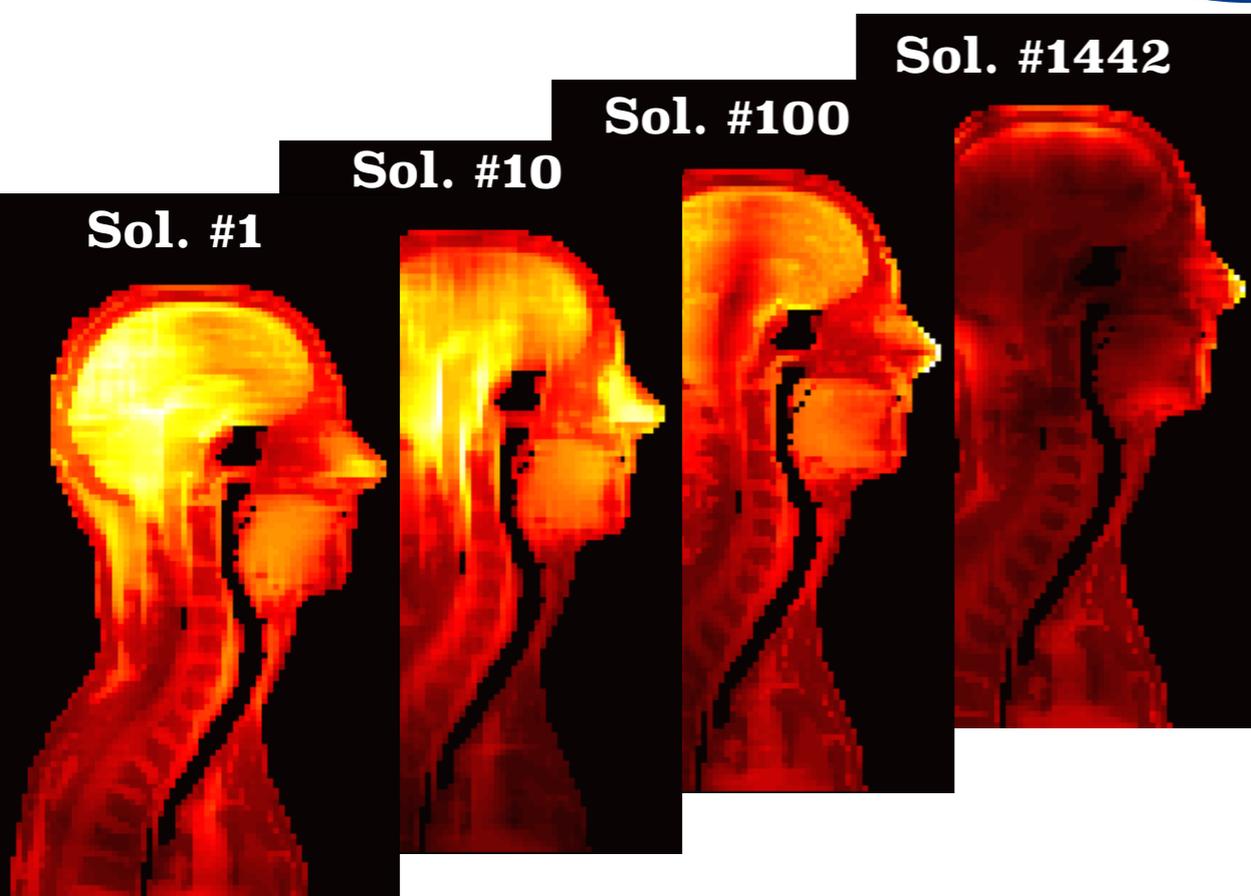


VIE

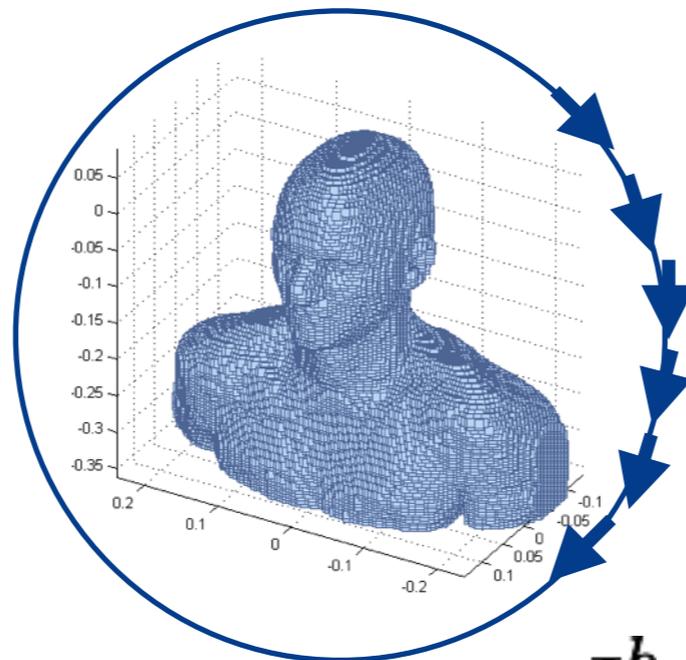
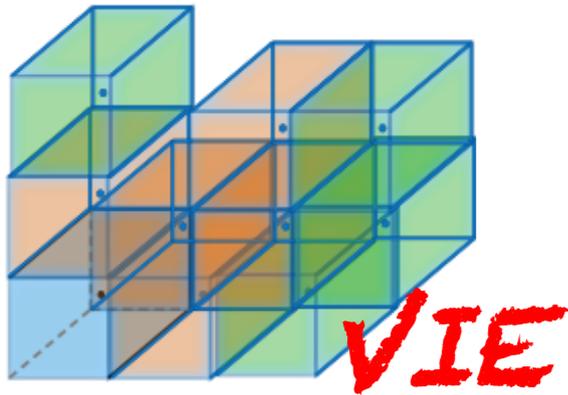
$$M_k = (Z^{bb})^{-1} U_k$$



$$J^b \approx \sum_k^q (Z^{bb})^{-1} U_k \alpha_k$$

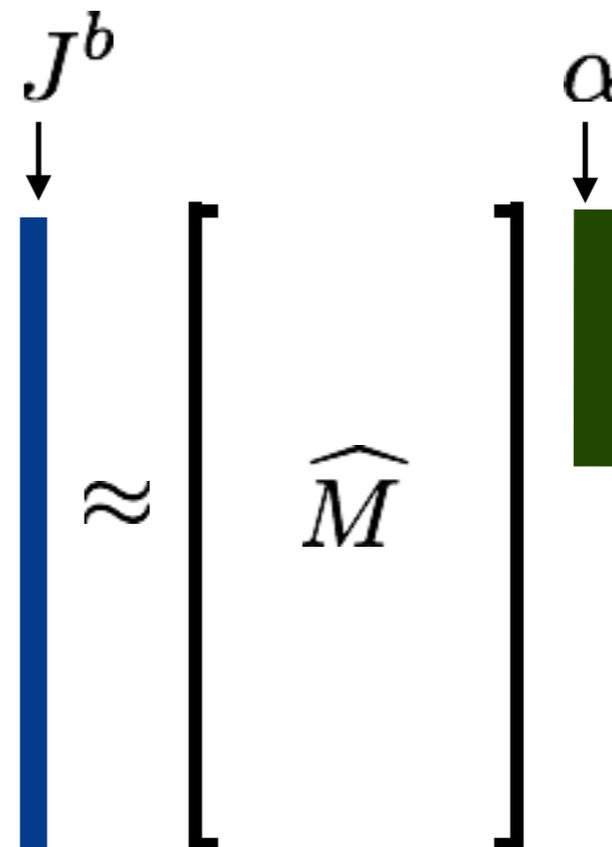


- ◆ Pre-compute the VIE solution **for each vector in basis**

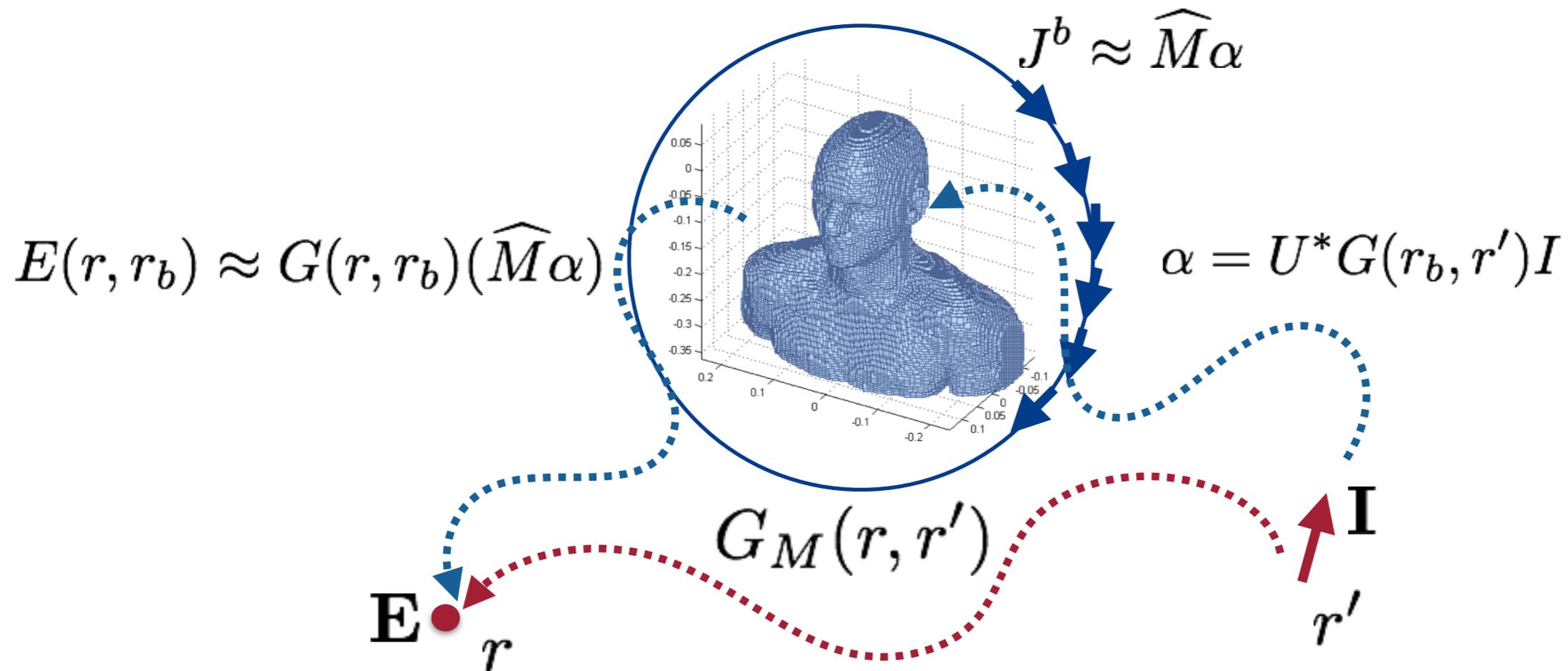


$$J^b \approx \sum_k^q (Z^{bb})^{-1} U_k \alpha_k$$

$$M_k = (Z^{bb})^{-1} U_k$$

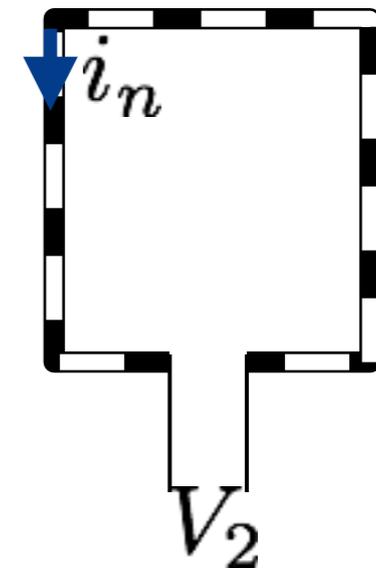
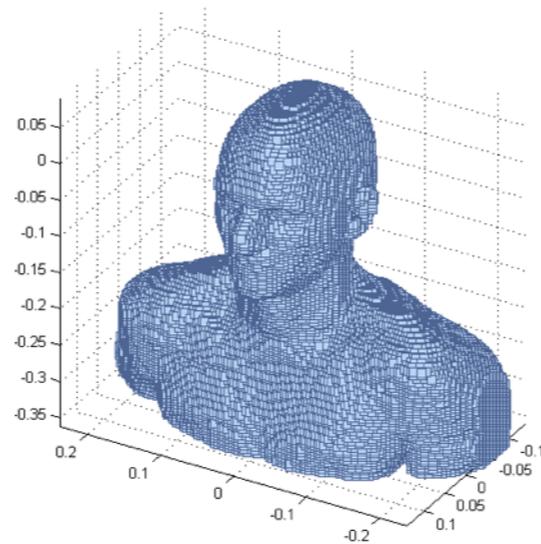
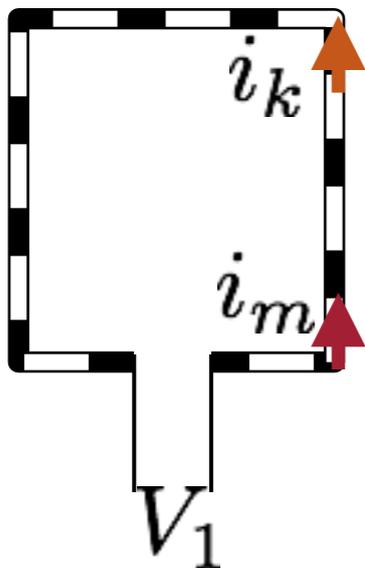


- ◆ Contribution of human body as set of matrix-vector products



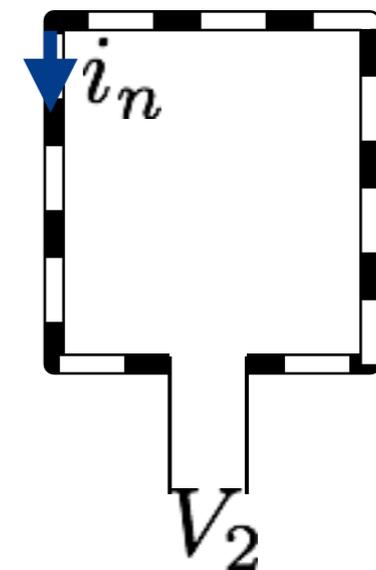
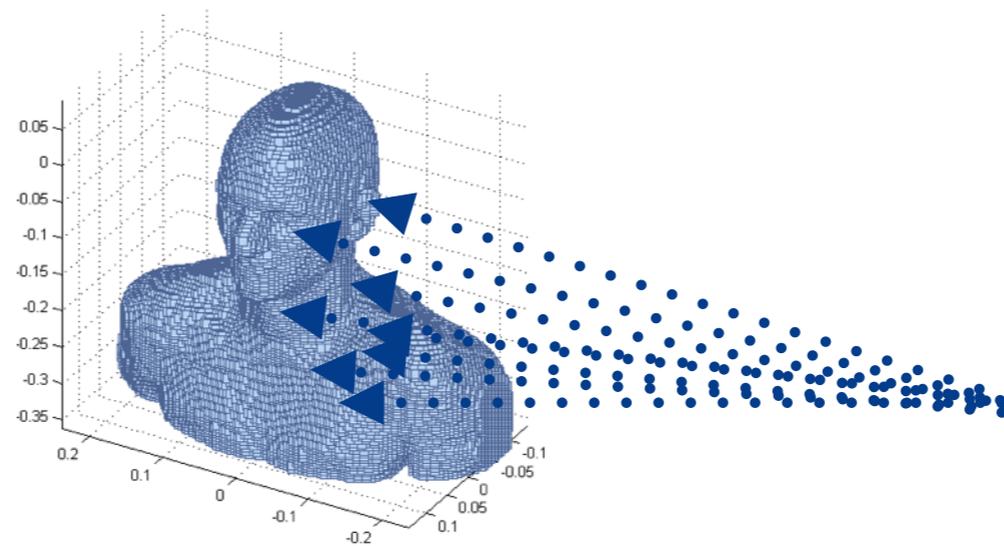
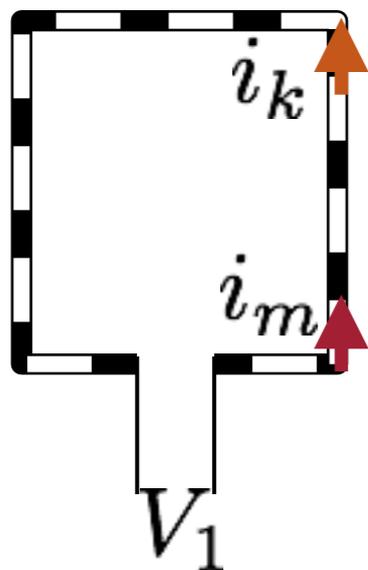
Accelerated integral equation solver

- ◆ Accelerate the integral equation solver

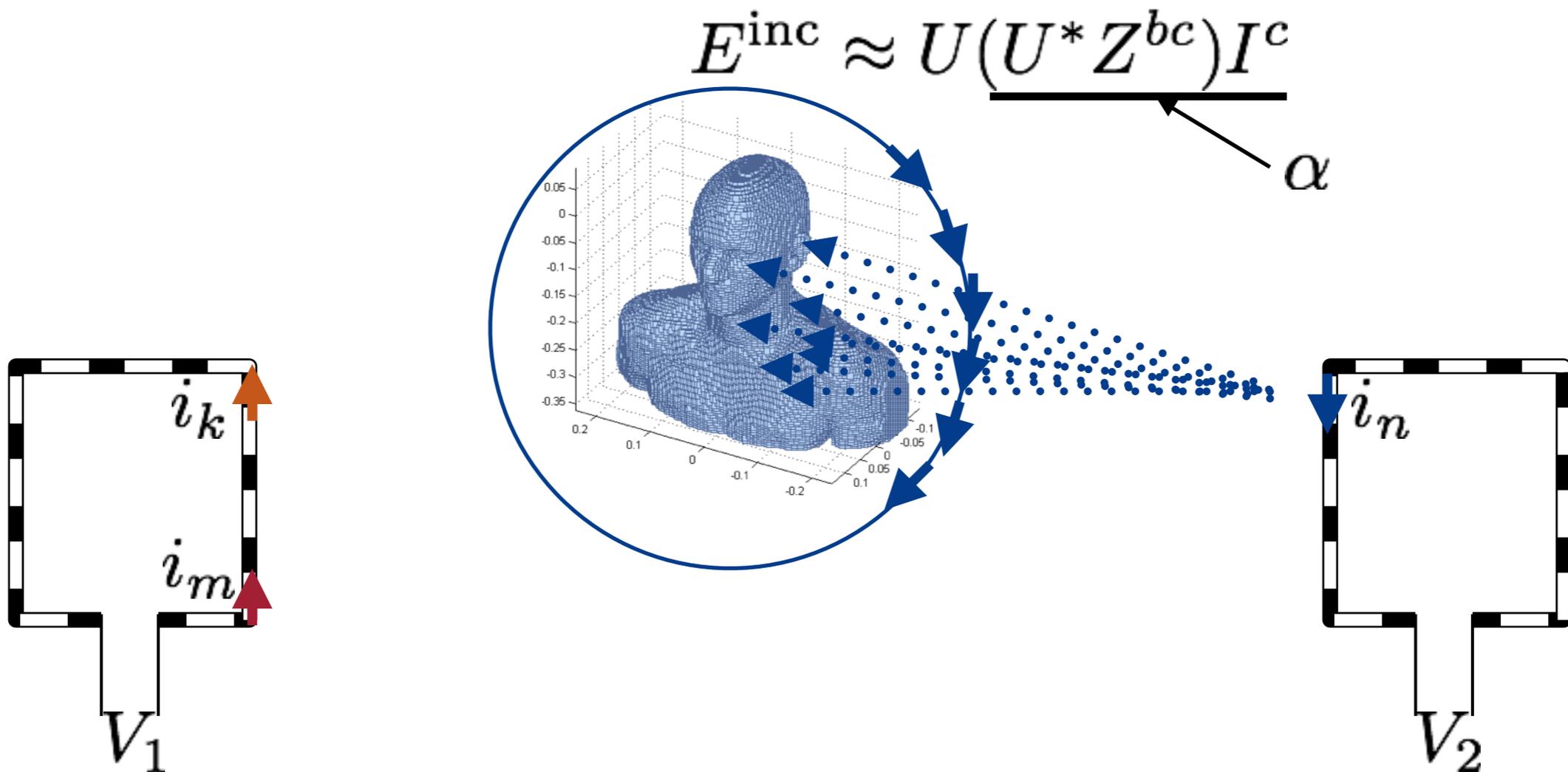


- ♦ Model the body perturbation with MRGFs

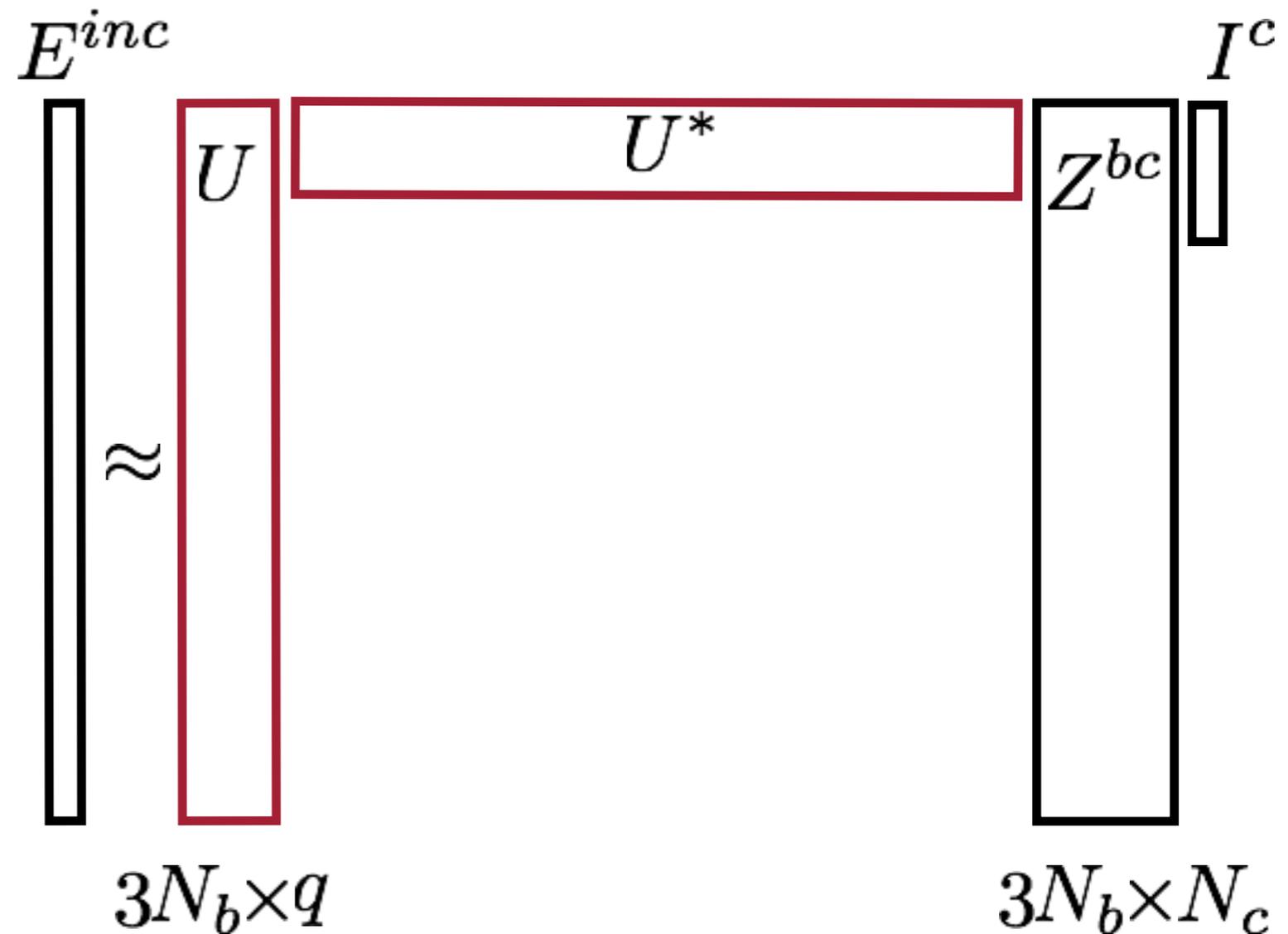
$$E^{\text{inc}} = Z^{bc} I^c$$



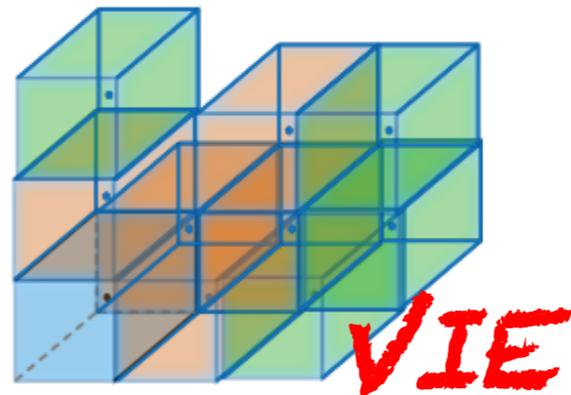
- ♦ Model the body perturbation with MRGFs



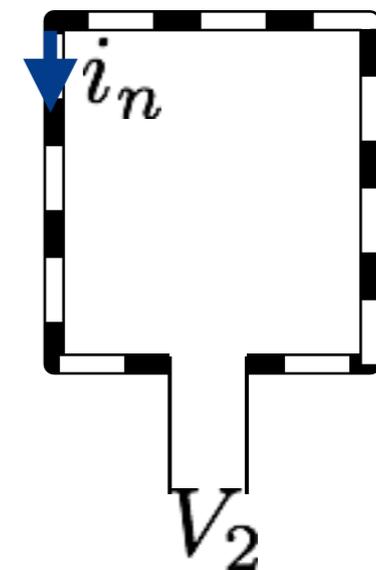
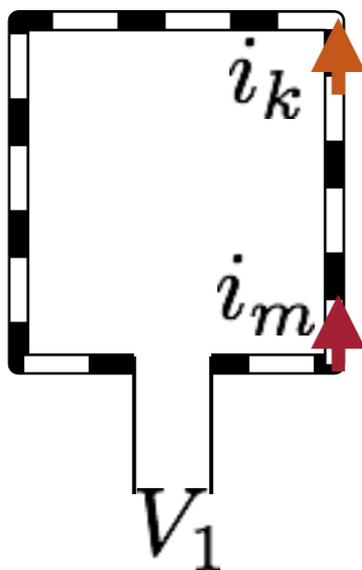
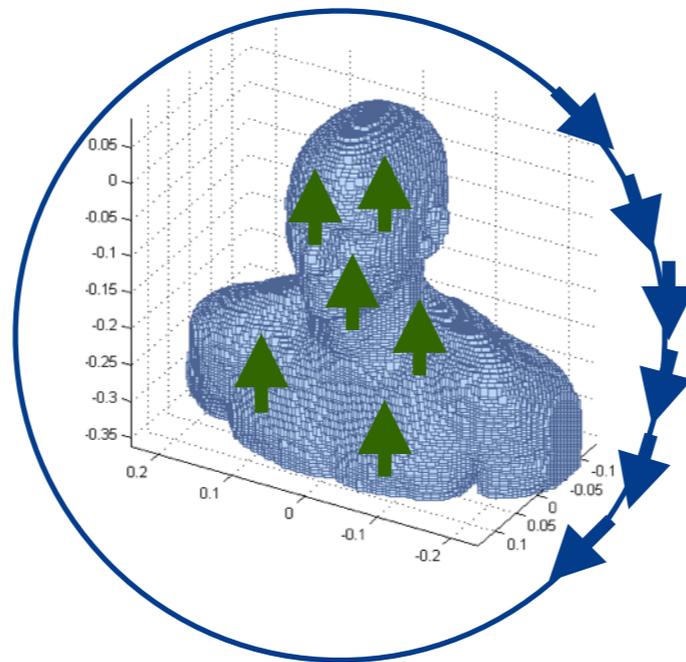
- ◆ **Model the body perturbation with MRGFs**
 - ◆ approximate incident field by basis



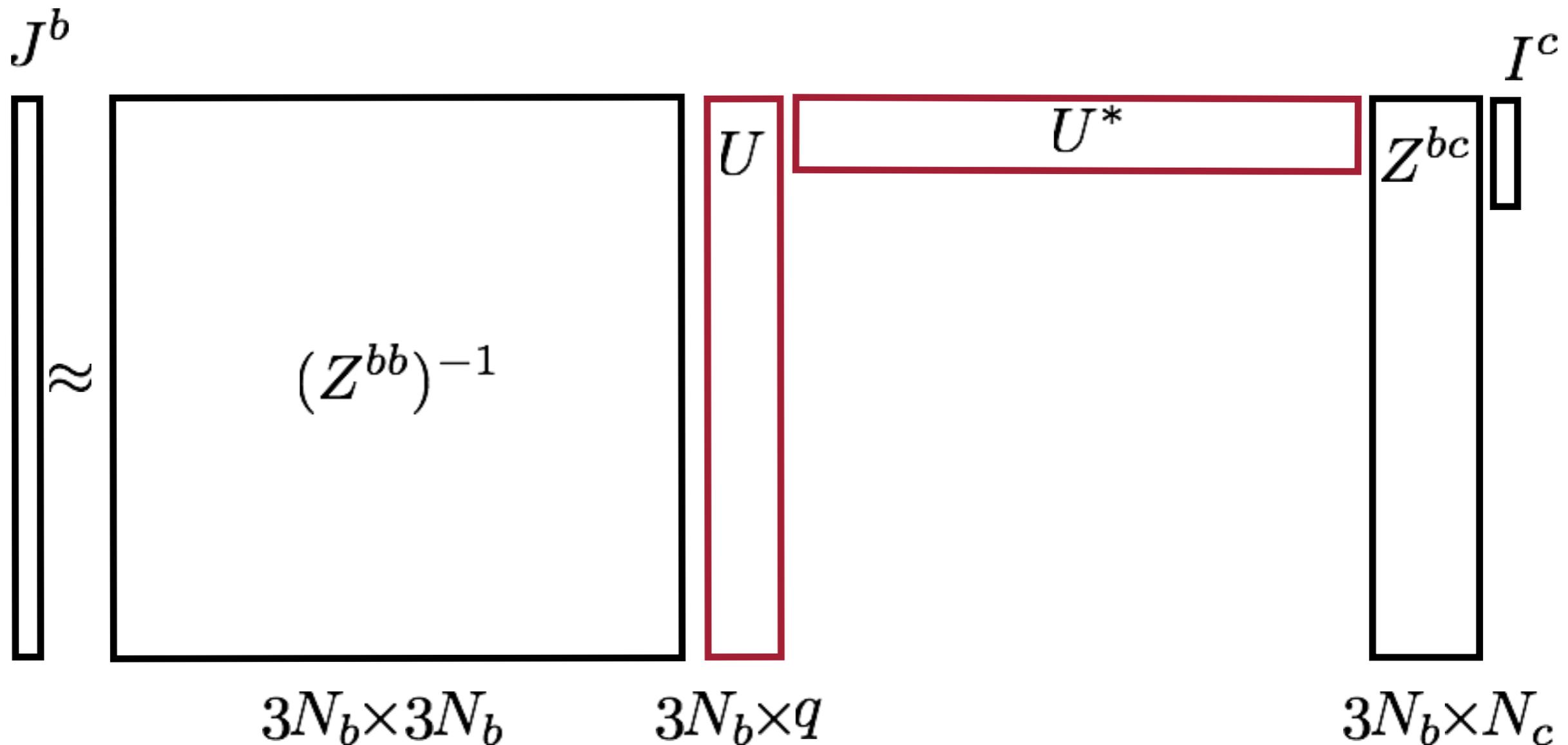
- ♦ Model the body perturbation with MRGFs



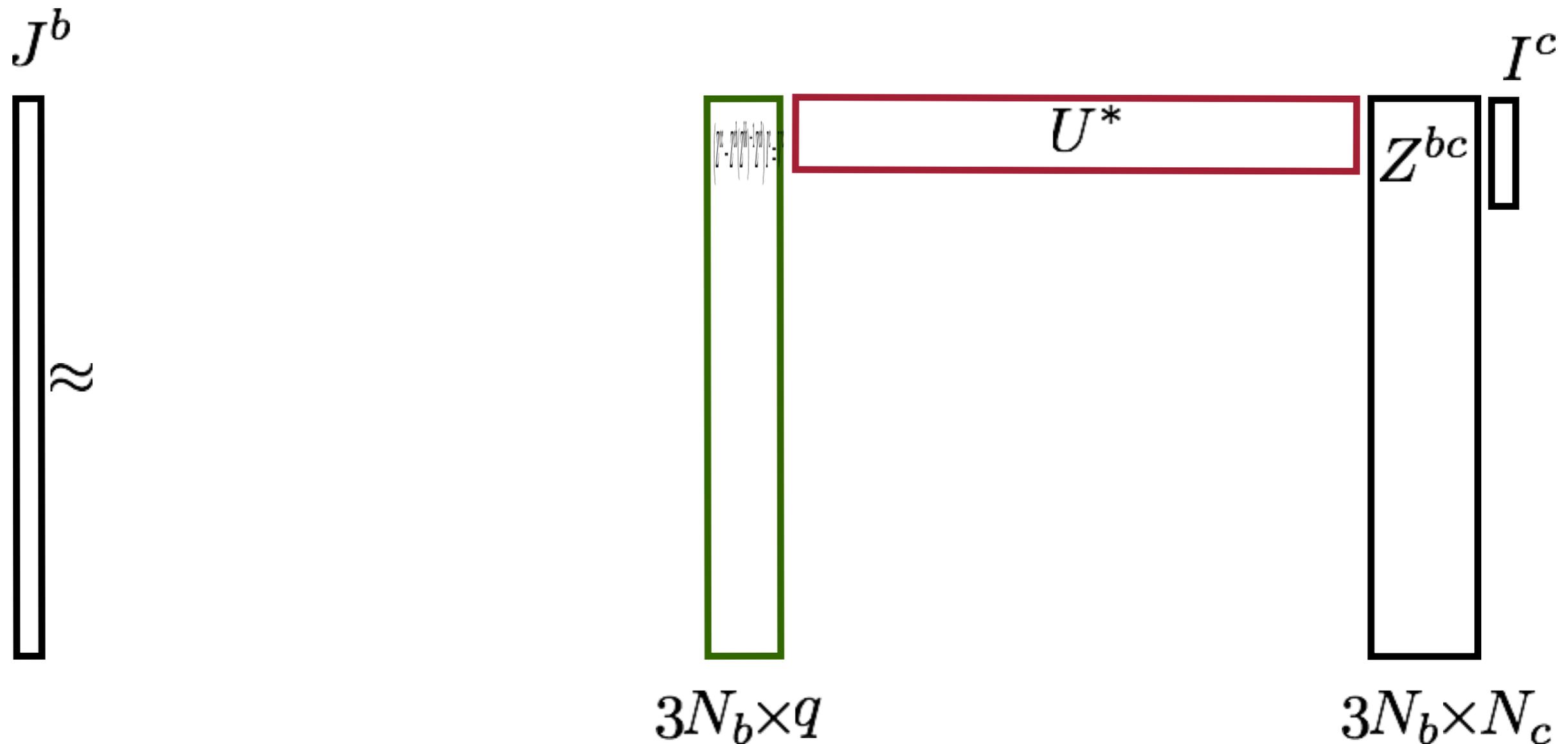
$$J^b = (Z^{bb})^{-1} E^{\text{inc}} \approx \underbrace{(Z^{bb})^{-1} U}_{\widehat{M}} \underbrace{(U^* Z^{bc})}_{\alpha} I^c$$



- ◆ **Model the body perturbation with MRGFs**
 - ◆ instead of applying the VIE solver



- ◆ **Model the body perturbation with MRGFs**
 - ◆ apply the pre-computed solutions

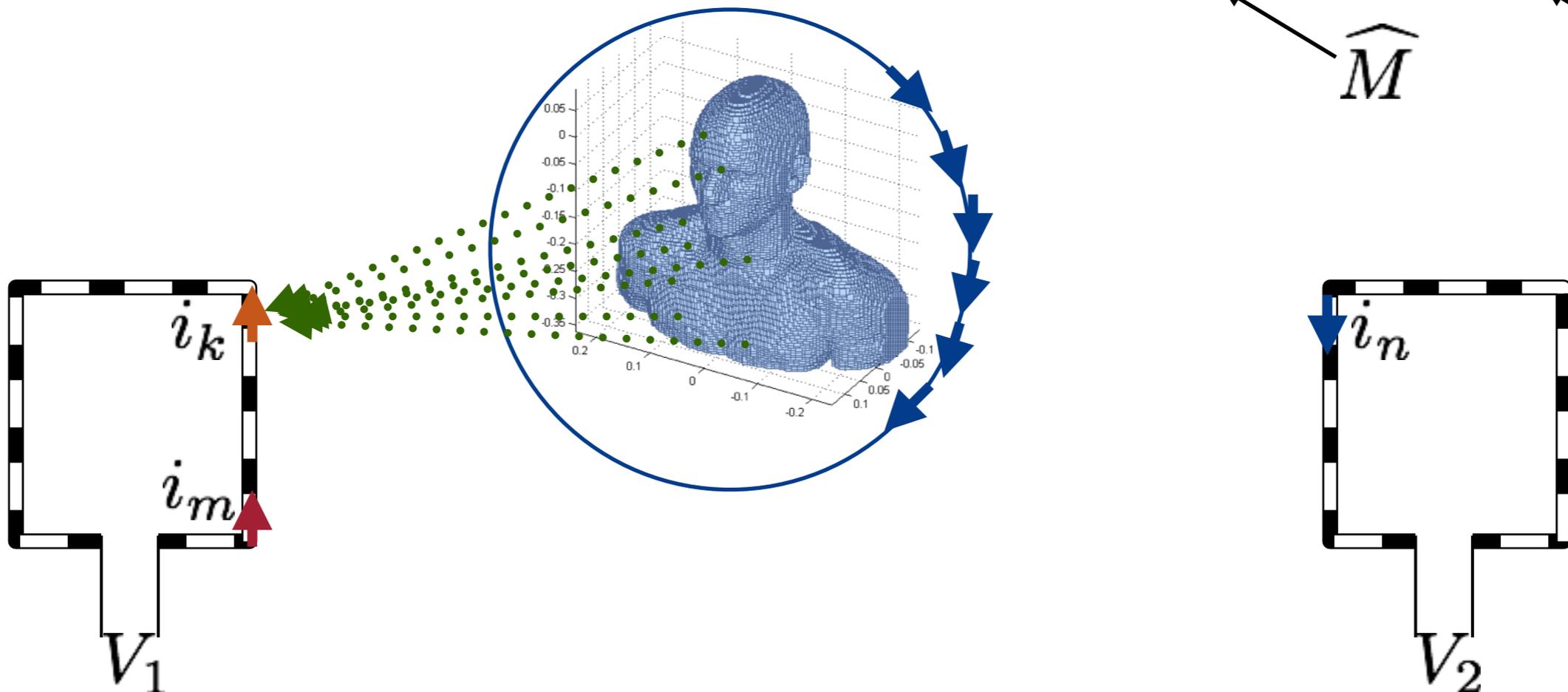


- ♦ Model the body perturbation with MRGFs

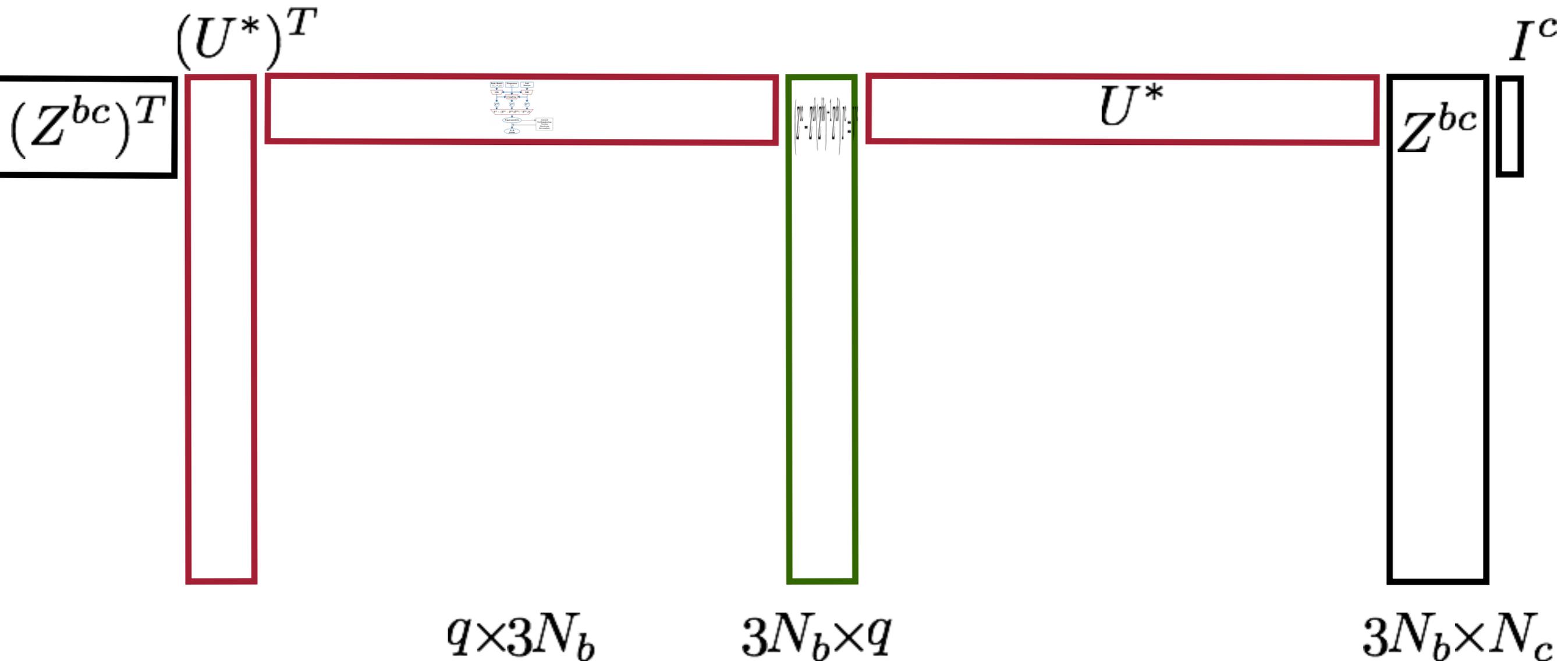
$q \times q$ precomputed matrix

$$\widehat{Z^{bb}}^{-1}$$

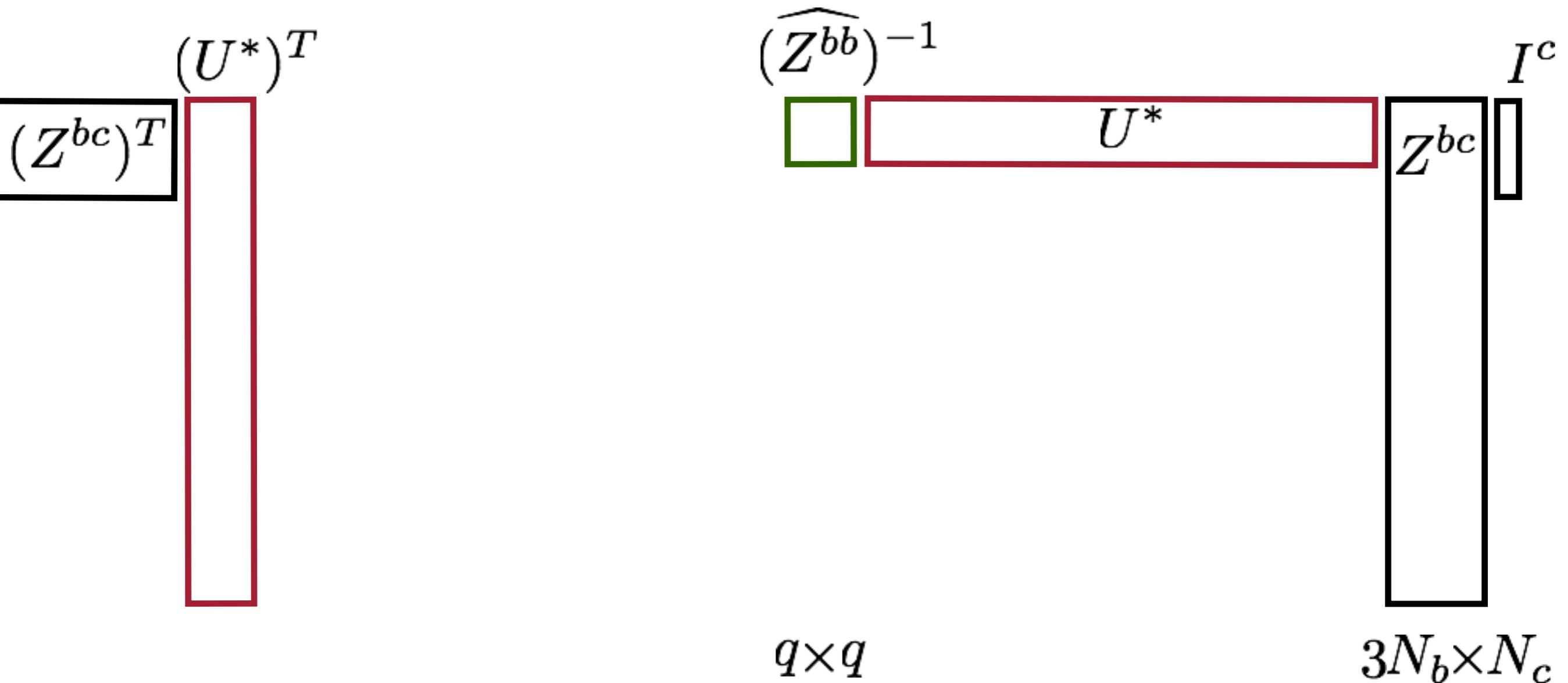
$$Z^p \approx \underbrace{(U^* Z^{bc})^T U^T}_{\widehat{M}} \underbrace{(Z^{bb})^{-1}}_{\alpha} \underbrace{U (U^* Z^{bc})}_{\alpha}$$



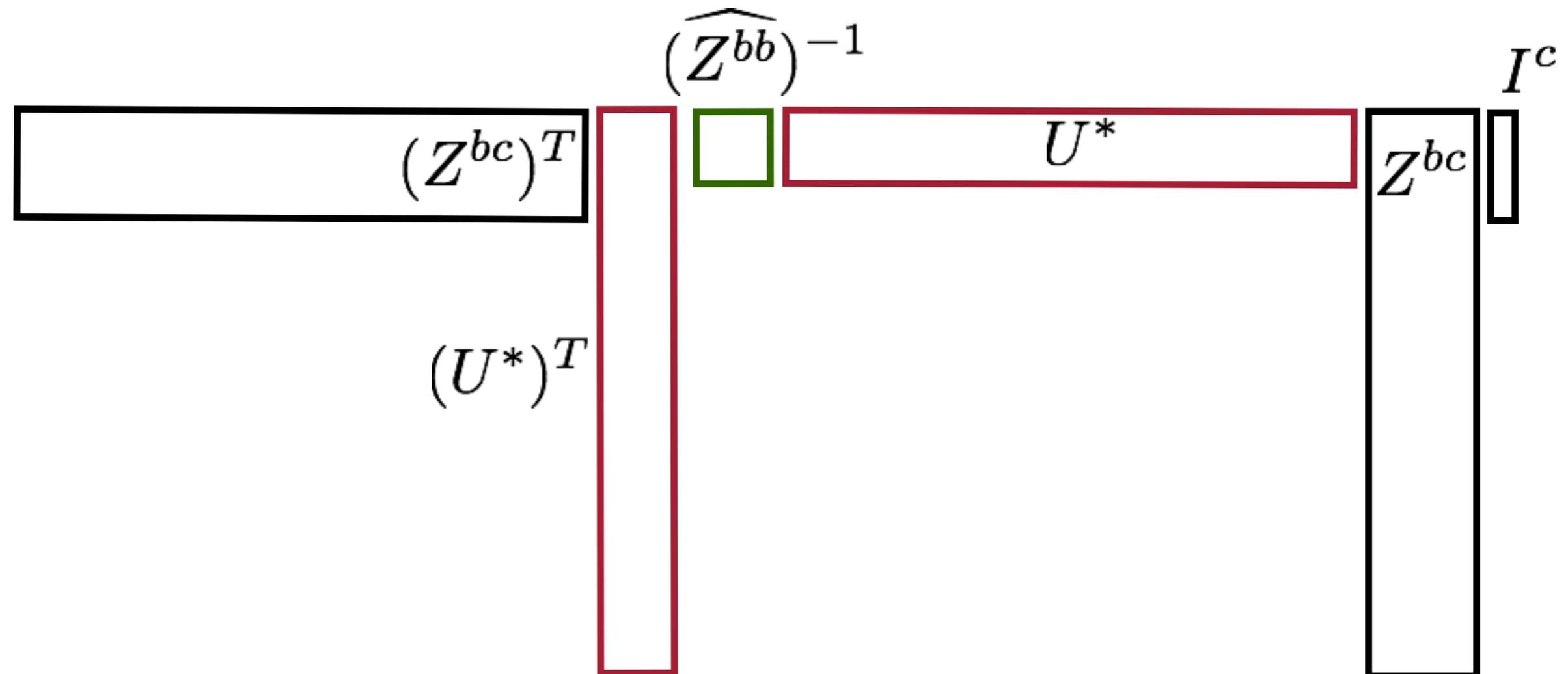
- ◆ **Model the body perturbation with MRGFs**
 - ◆ exploit reciprocity of Green functions on left side



- ◆ **Model the body perturbation with MRGFs**
 - ◆ apply further compression



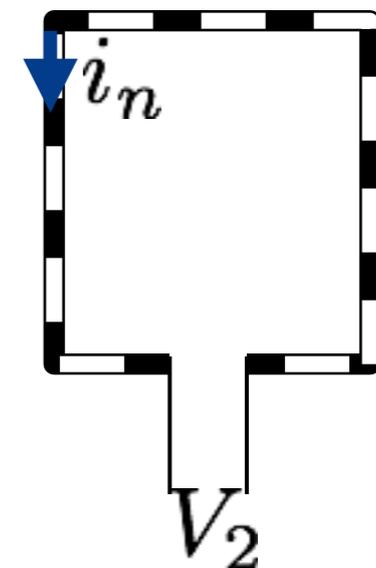
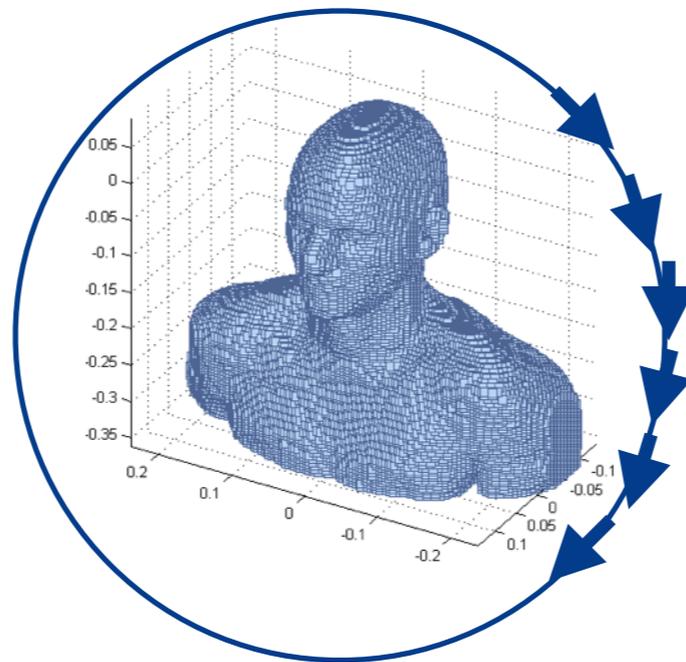
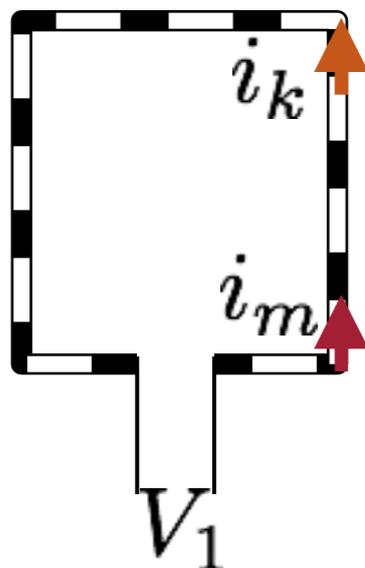
- ♦ **Model the body perturbation with MRGFs**
 - ♦ to generate the perturbation matrix $N_c \times N_c$



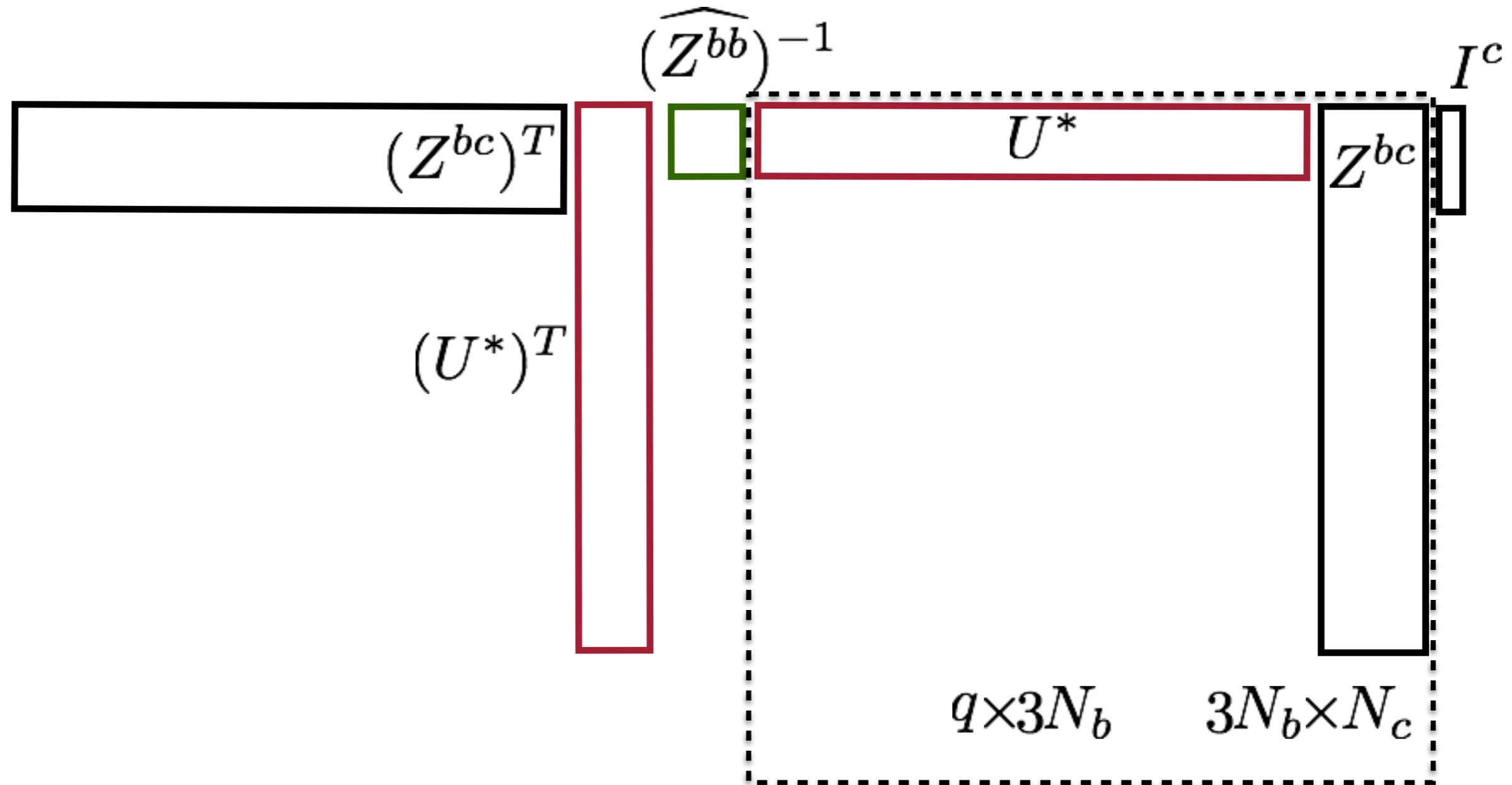
- ◆ **Model the body perturbation with MRGFs**
 - ◆ avoids VIE solver
 - ◆ assemble the perturbation: a set of low-rank matrix-vector products

q x q precomputed matrix

$$\left(Z^{cc} - (U^* Z^{bc})^T \widehat{Z^{bb}}^{-1} (U^* Z^{bc}) \right) I^c = V^c$$

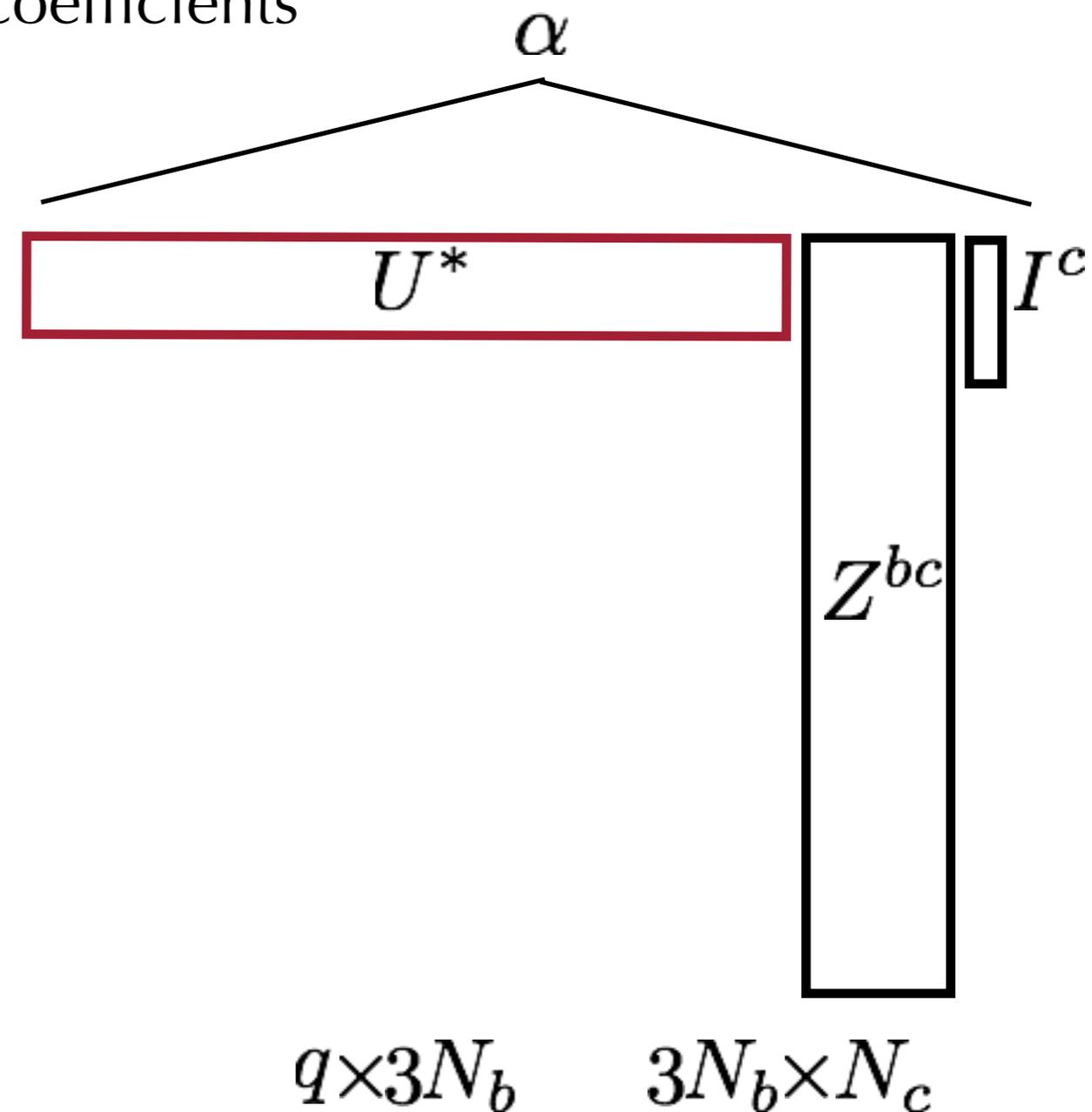


- ◆ Still requires to form and project the coupling block
 - ◆ for every new coil



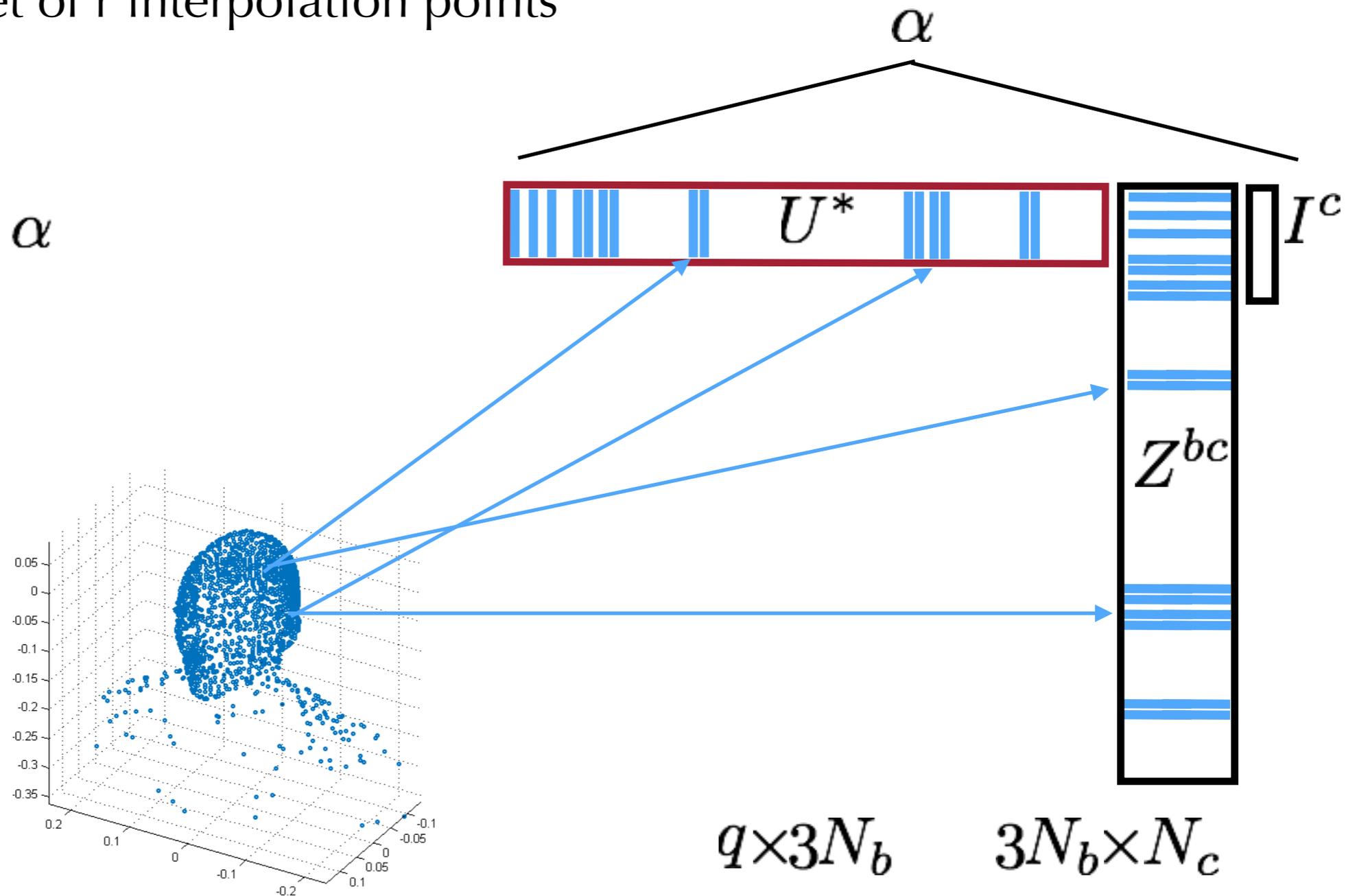
- ◆ **Still requires to form and project the coupling block**
 - ◆ approximate the computation of the coefficients

$$U^* Z^{bc} I^c = \alpha$$



- ◆ Still requires to form and project the coupling block
 - ◆ using a small set of r interpolation points

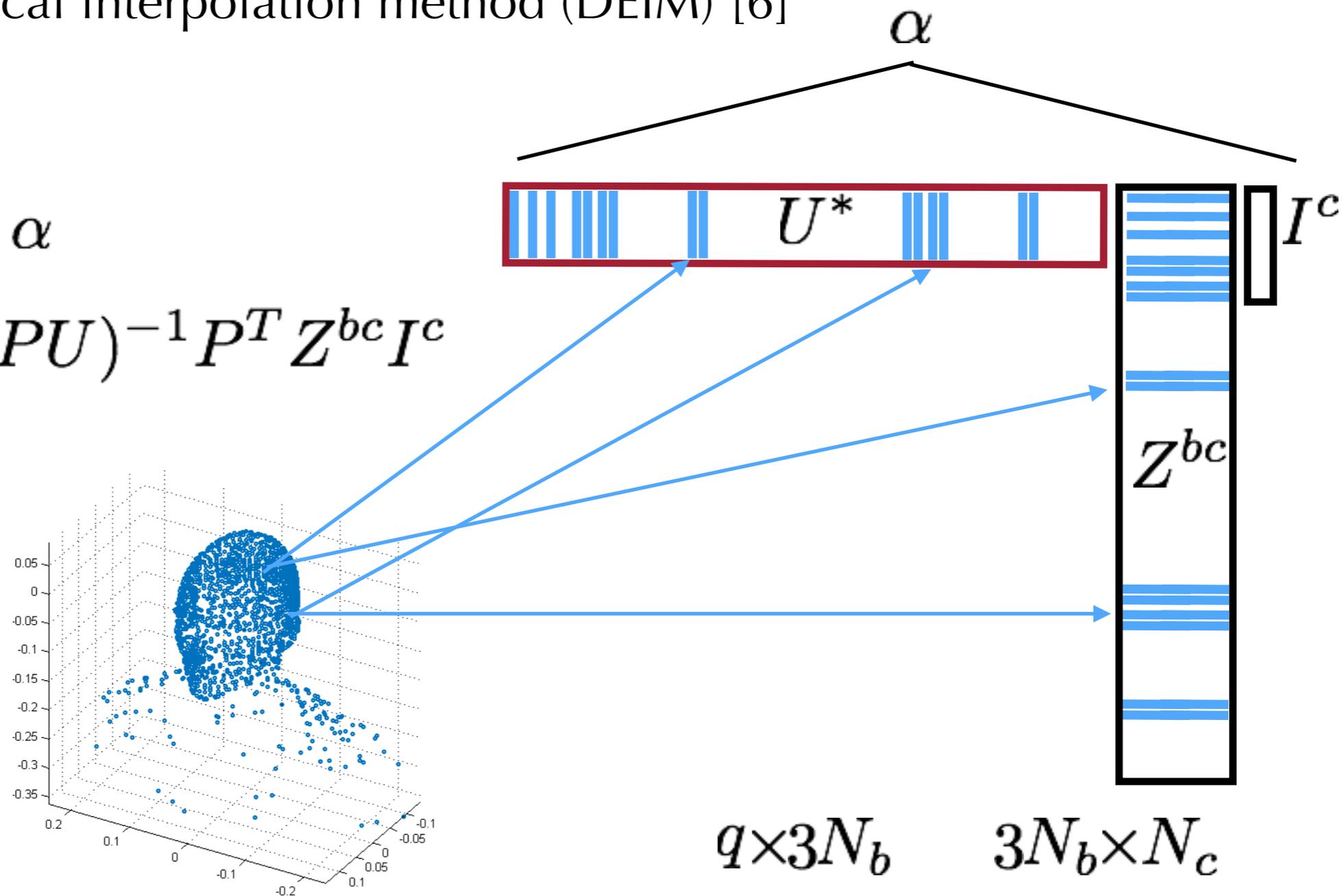
$$U^* Z^{bc} I^c = \alpha$$



- ◆ Still requires to form and project the coupling block
 - ◆ Discrete empirical interpolation method (DEIM) [6]

$$U^* Z^{bc} I^c = \alpha$$

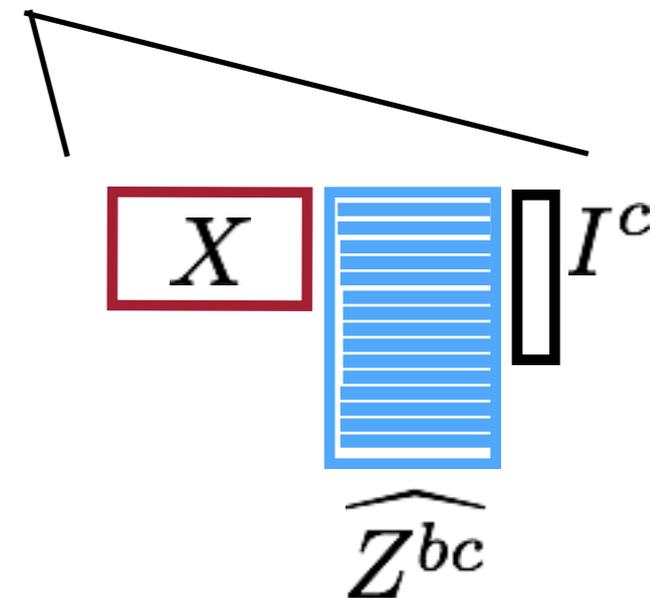
$$\alpha \approx \alpha_p = (PU)^{-1} P^T Z^{bc} I^c$$



- ◆ **Still requires to form and project the coupling block**

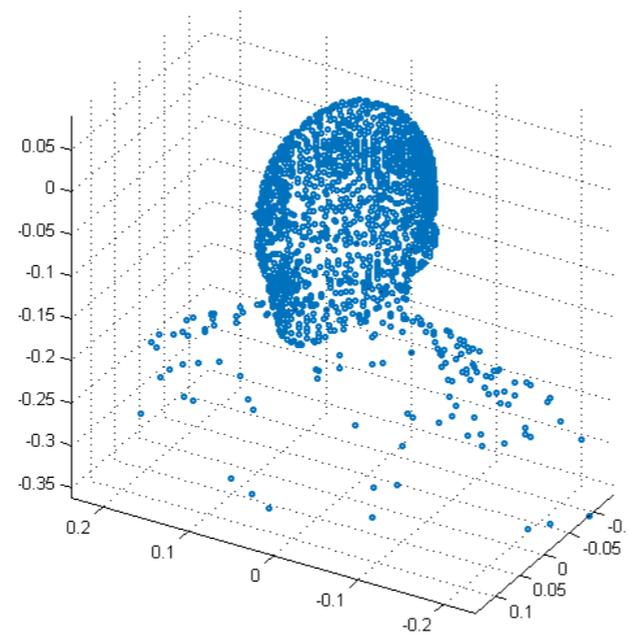
- ◆ pre-compute the matrix X
- ◆ only need to evaluate coupling at r points

$$\alpha \approx \alpha_p = (PU)^{-1} P^T Z^{bc} I^c$$



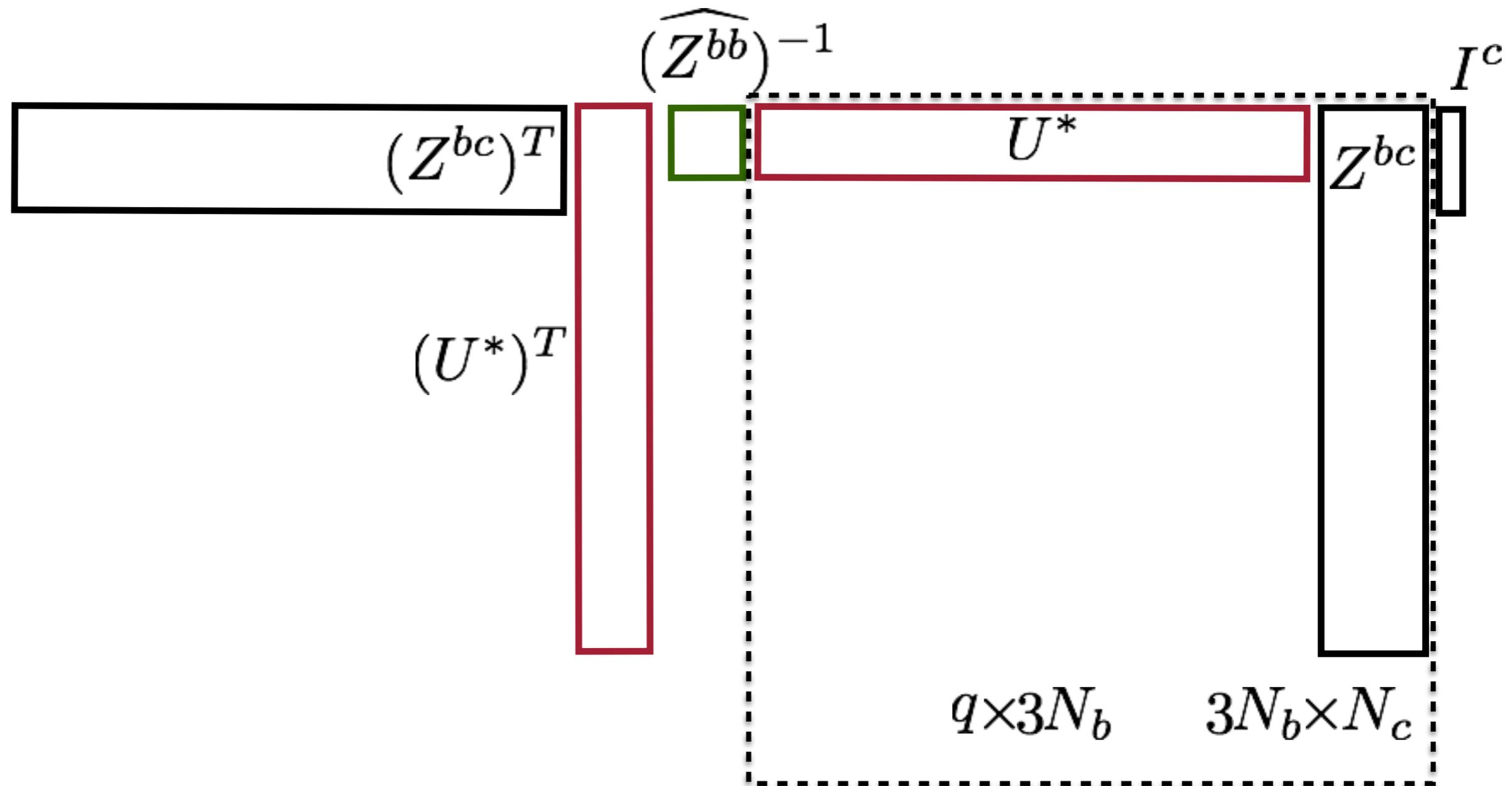
$$X = (PU)^{-1}$$

$$\widehat{Z}^{bc} = P^T Z^{bc}$$

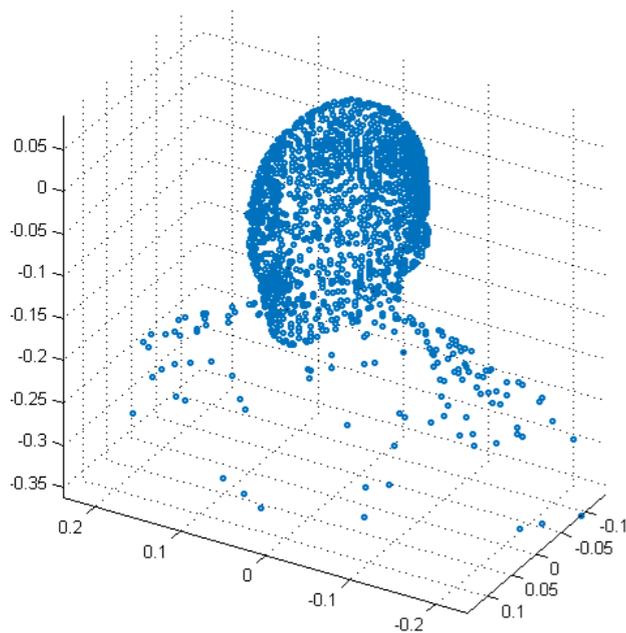
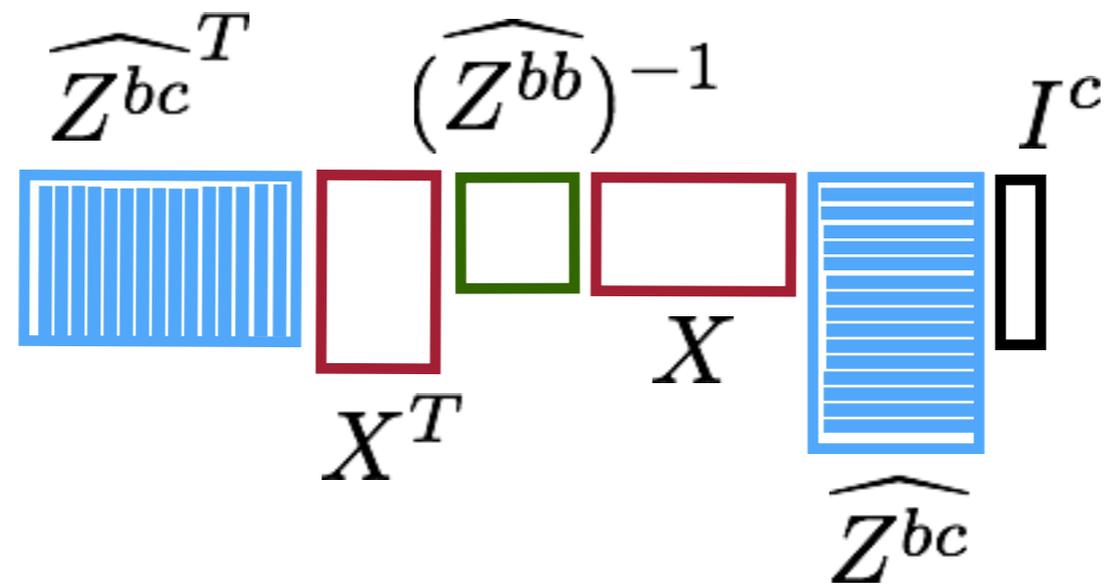


$$q \times r \quad r \times N_c$$

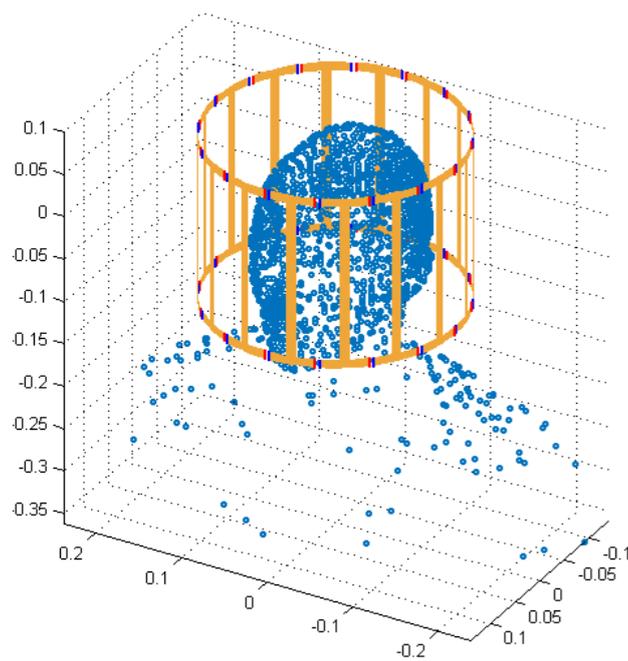
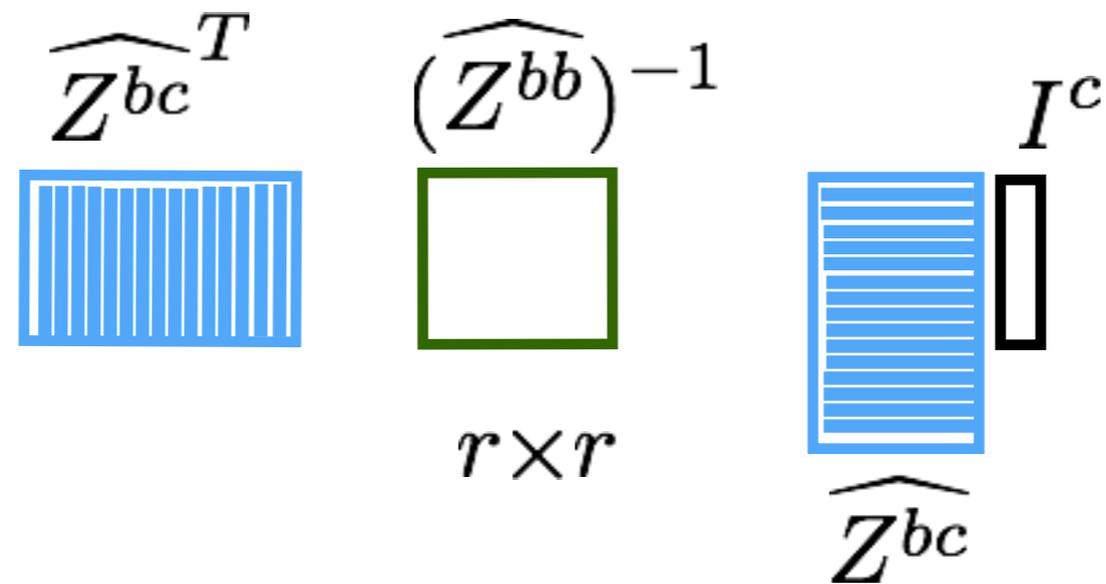
- ◆ Instead of evaluating the coupling in all positions and project



- ◆ Instead of evaluating the coupling in all positions and project
 - ◆ evaluation in r points

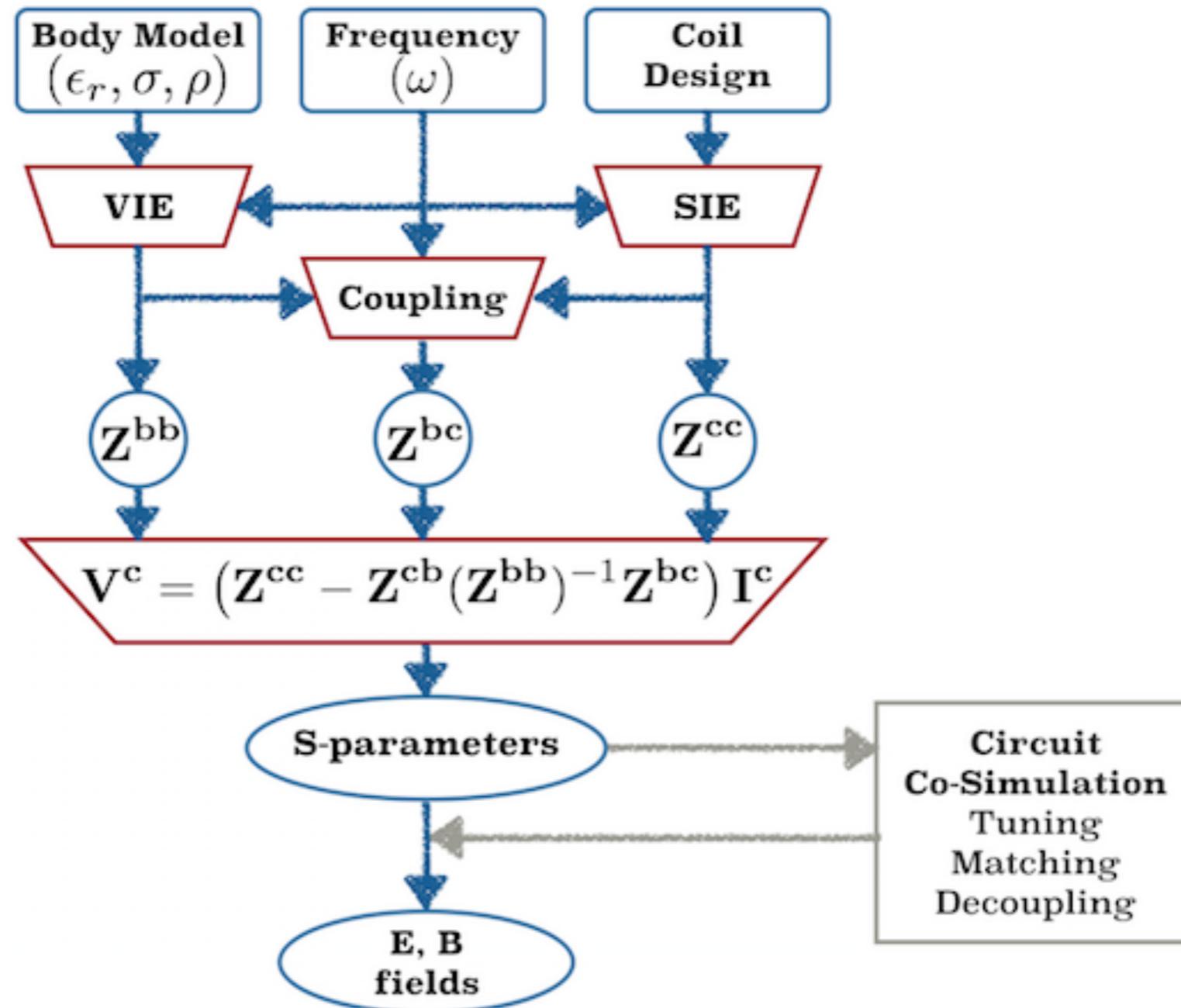


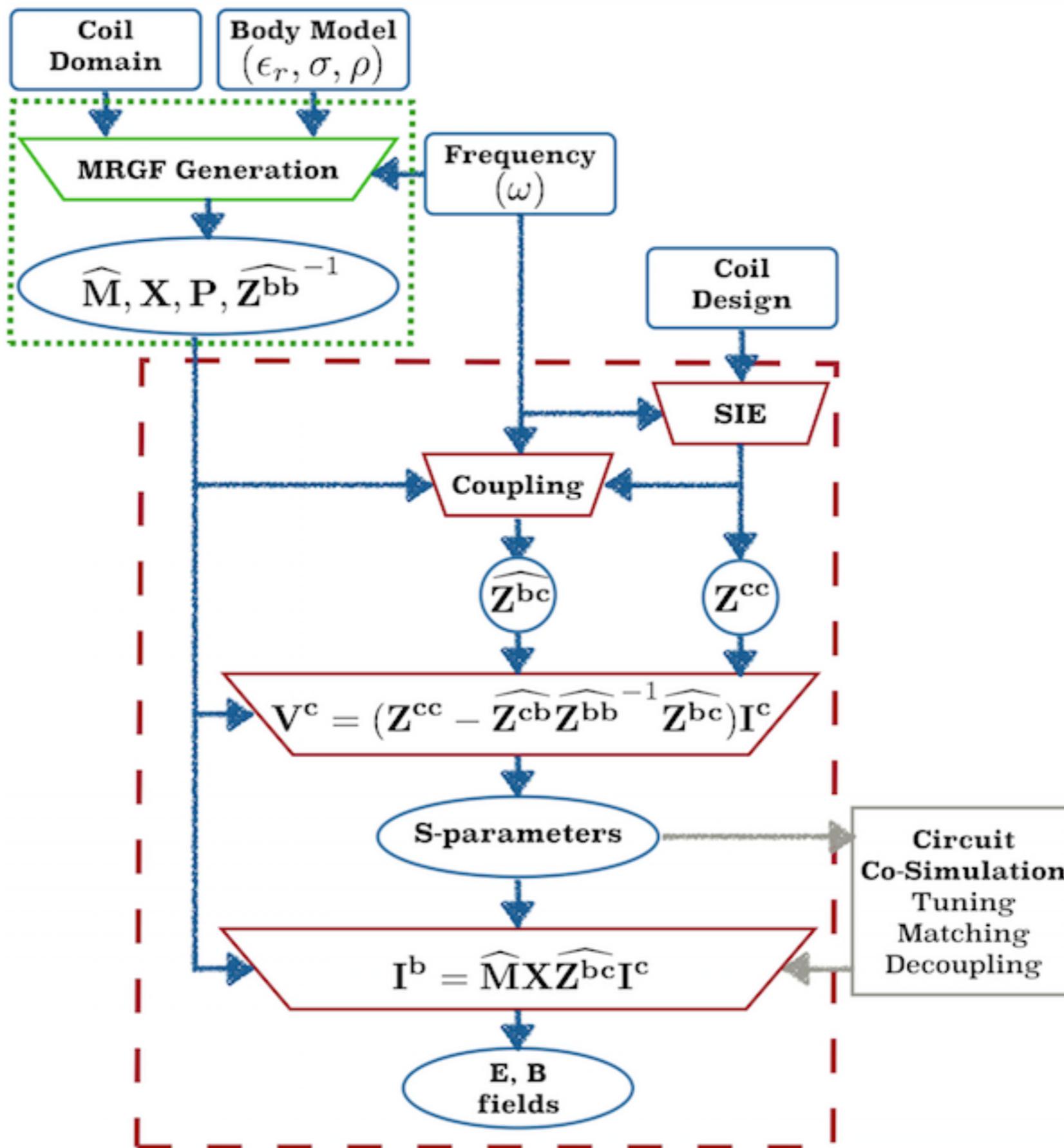
- ◆ Instead of evaluating the coupling in all positions and project
 - ◆ evaluation in r points



$$\left(Z^{cc} - \widehat{Z}^{bcT} \widehat{Z}^{bb}{}^{-1} \widehat{Z}^{bc} \right) I^c = V^c$$

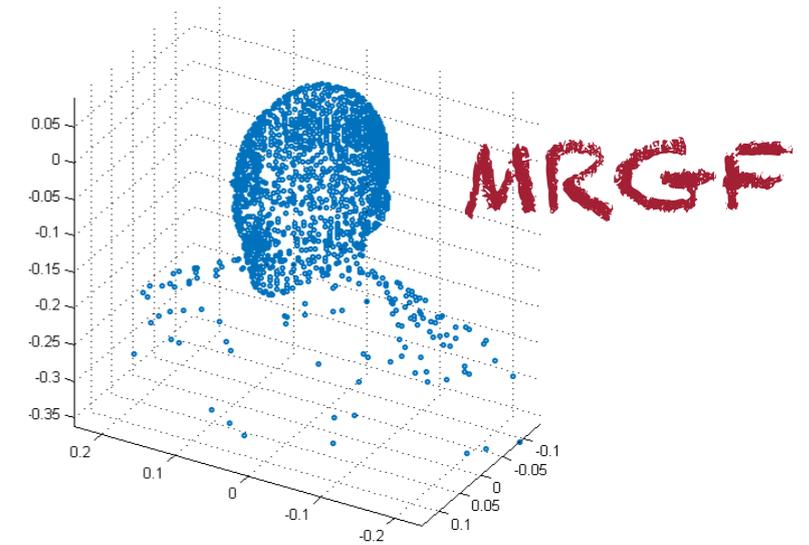
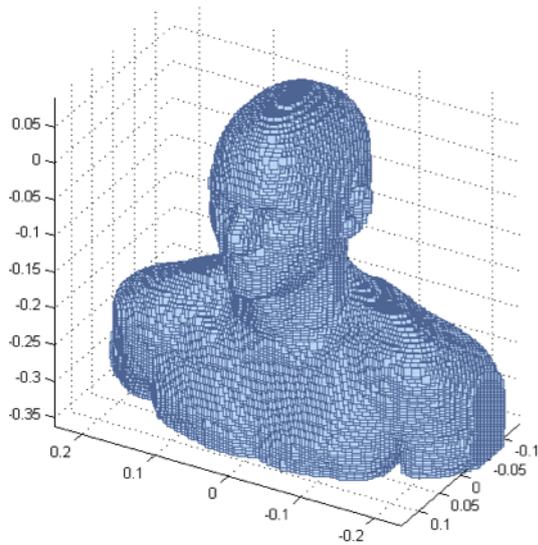
$$N_c \times N_c$$





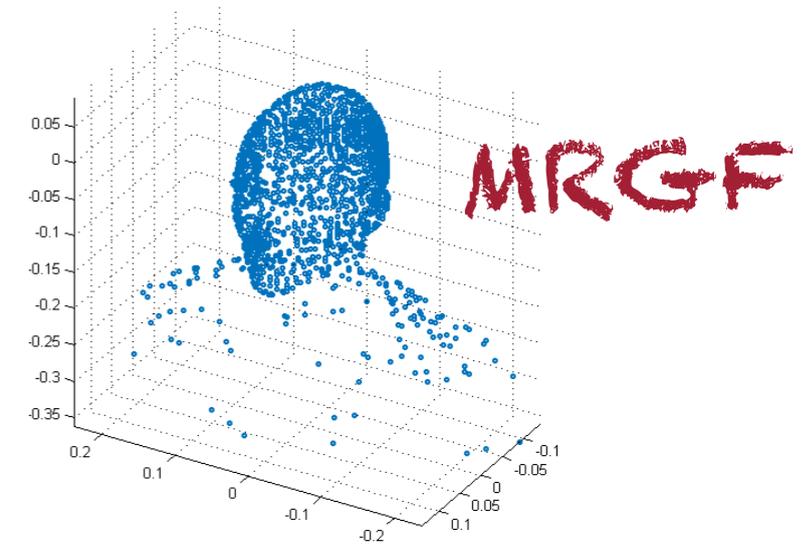
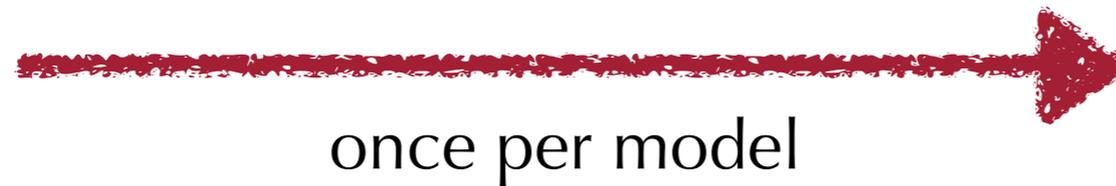
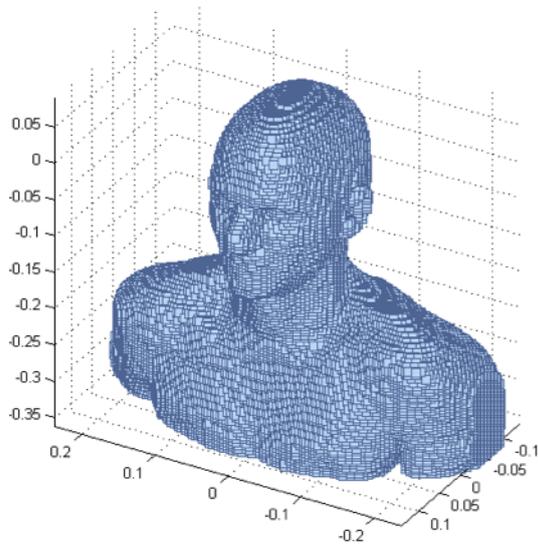
- ◆ Accelerated Integral Equation solver for MRI coils
 - ◆ Off-line phase
 - ◆ On-line phase

- ◆ Accelerated Integral Equation solver for MRI coils
 - ◆ Off-line phase: MRGF pre-computation

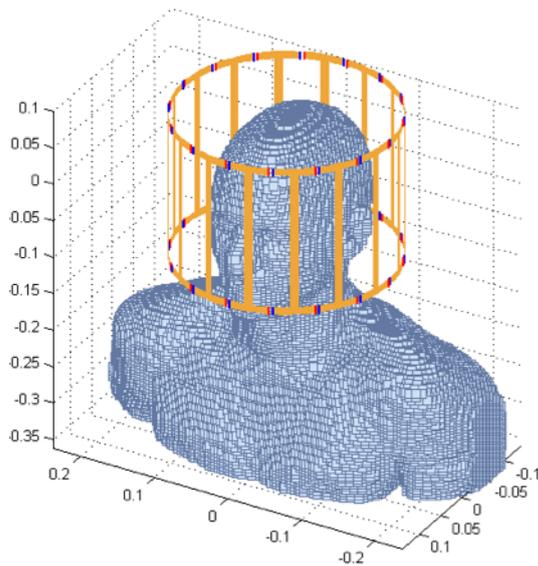


- ◆ On-line phase

- ◆ Accelerated Integral Equation solver for MRI coils
 - ◆ Off-line phase: MRGF pre-computation

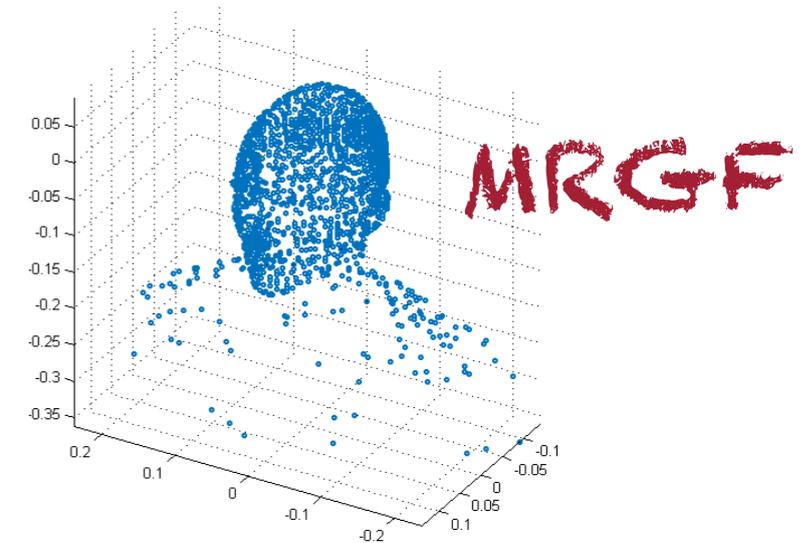
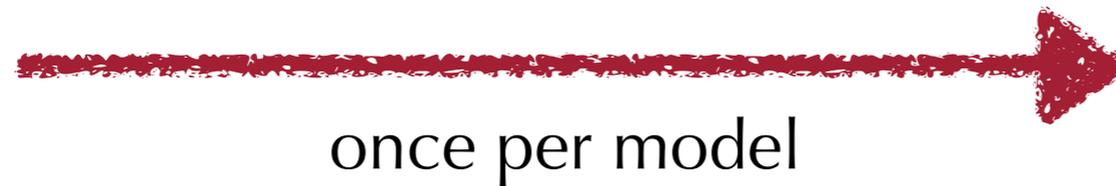
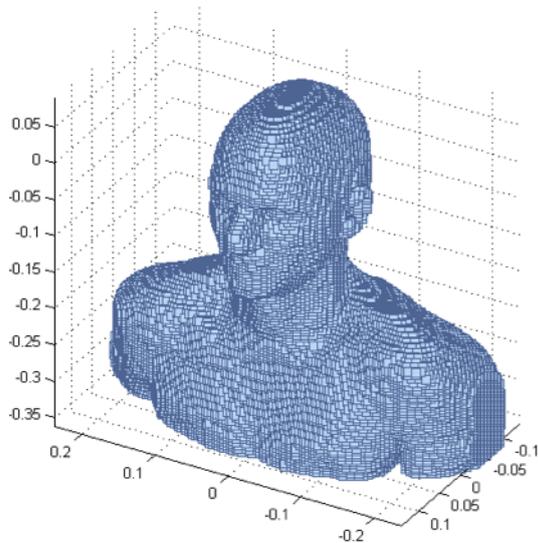


- ◆ On-line phase

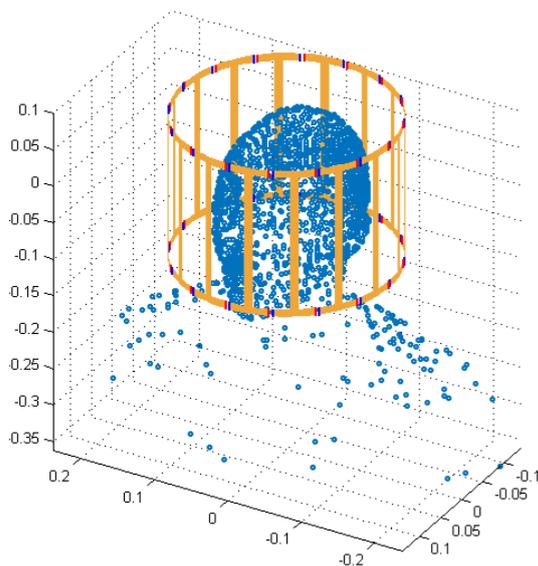


reuse for as many coils as desired
with fixed body model

- ◆ Accelerated Integral Equation solver for MRI coils
 - ◆ Off-line phase: MRGF pre-computation

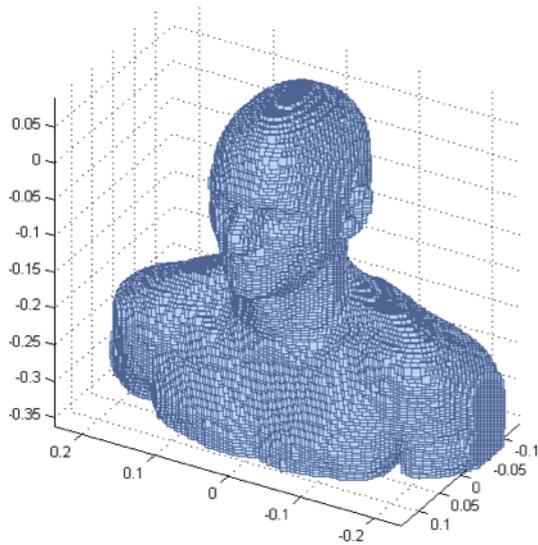


- ◆ On-line phase: MRGF use

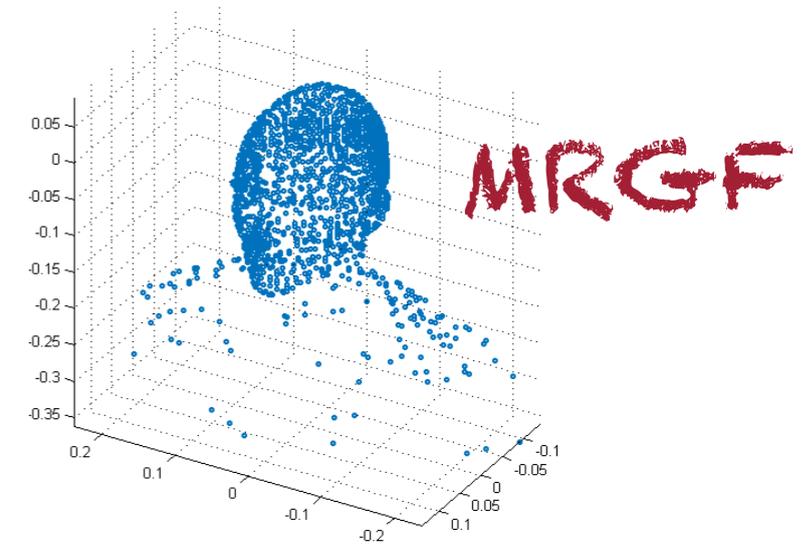


reuse for as many coils as desired
with fixed body model

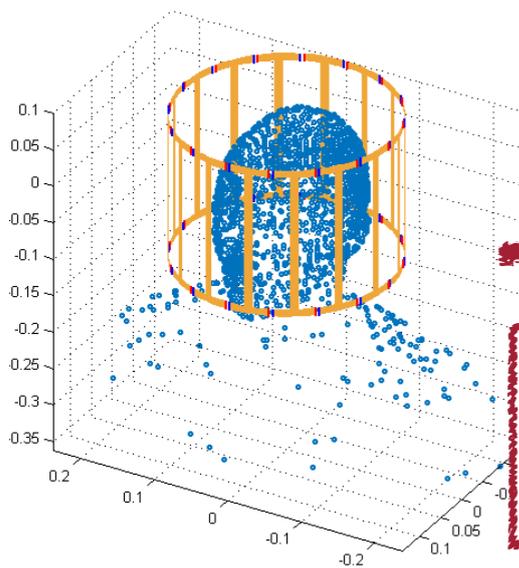
- ◆ Accelerated Integral Equation solver for MRI coils
 - ◆ Off-line phase: MRGF pre-computation



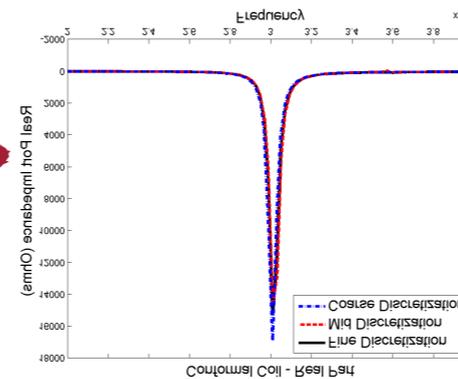
once per model



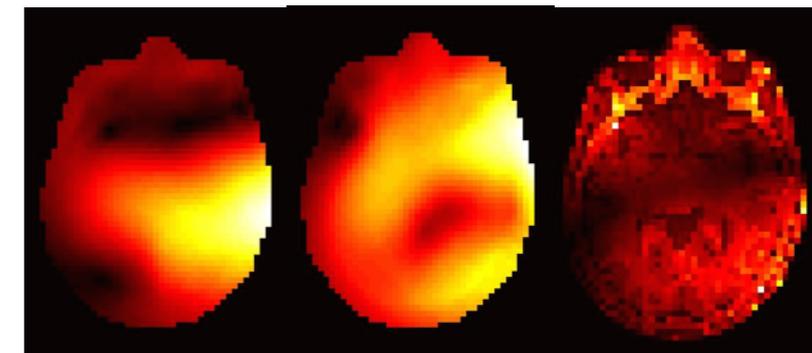
- ◆ On-line phase: MRGF use



Accelerated full-wave EM solver

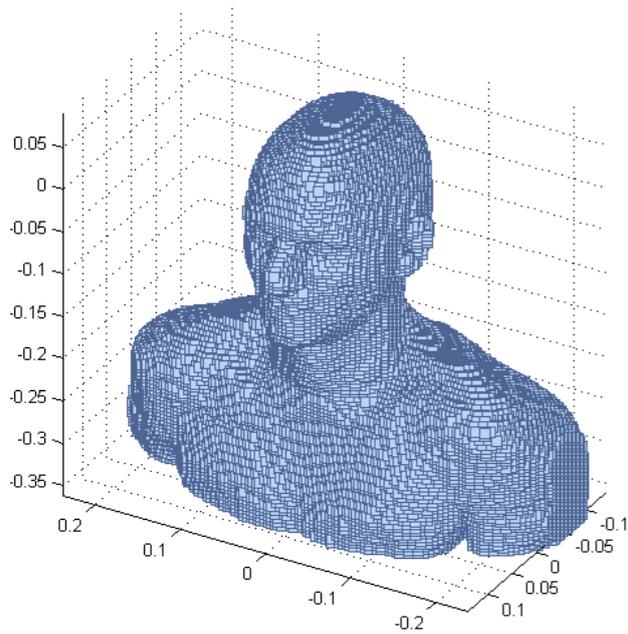


&



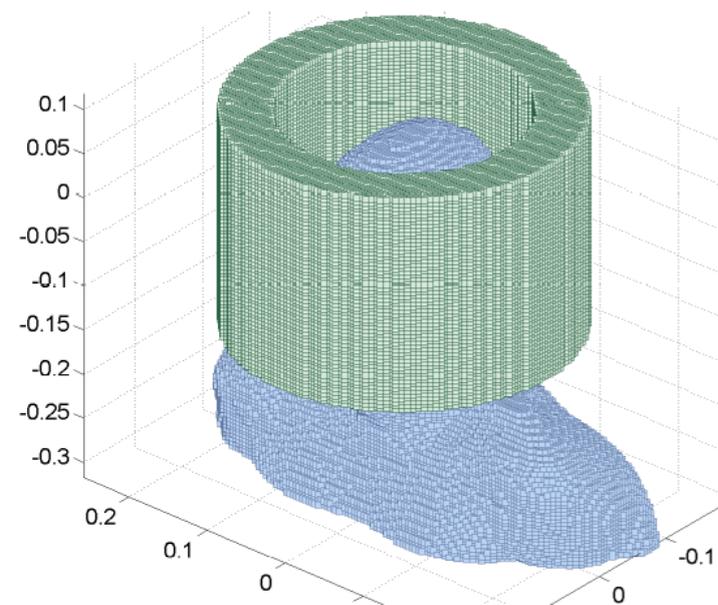
Detailed application on an realistic case

◆ Magnetic Resonance Green Function: Pre-computation



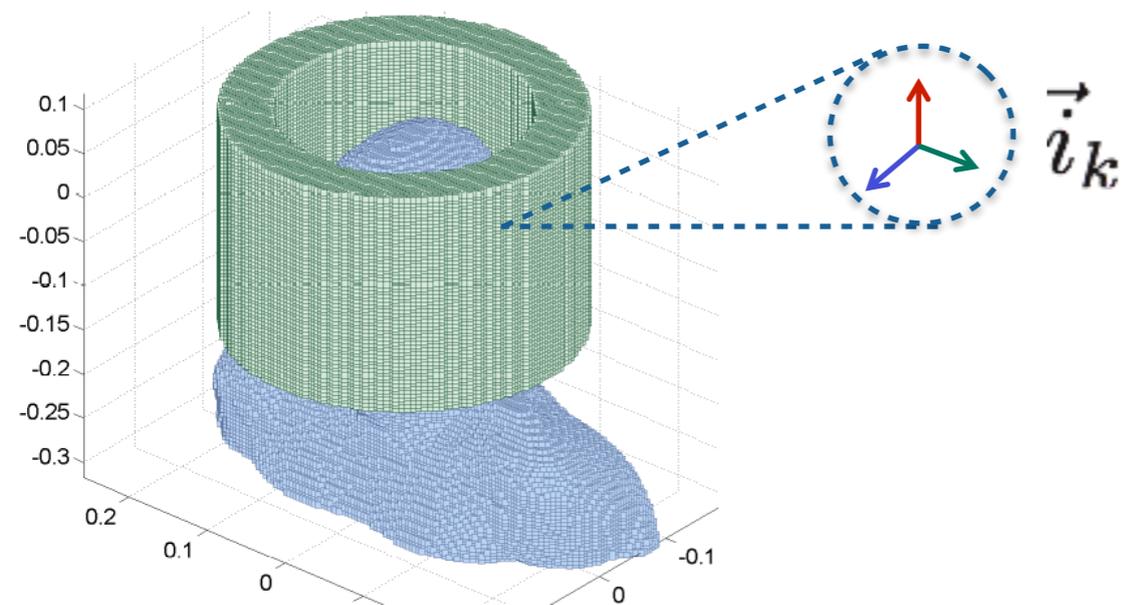
DUKE 4mm @7T
266,019 Voxels

- ◆ **Magnetic Resonance Green Function: Pre-computation**
 - ◆ Coil domain



inner radius 13cm
outer radius 18cm
length 24cm

- ◆ **Magnetic Resonance Green Function: Pre-computation**
 - ◆ Generate the all possible incident fields

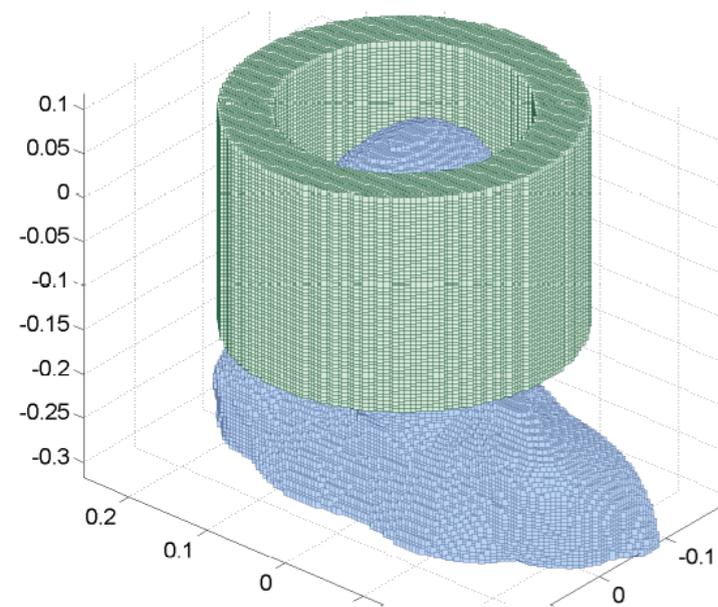


189,000 dipoles

3 components / dipole

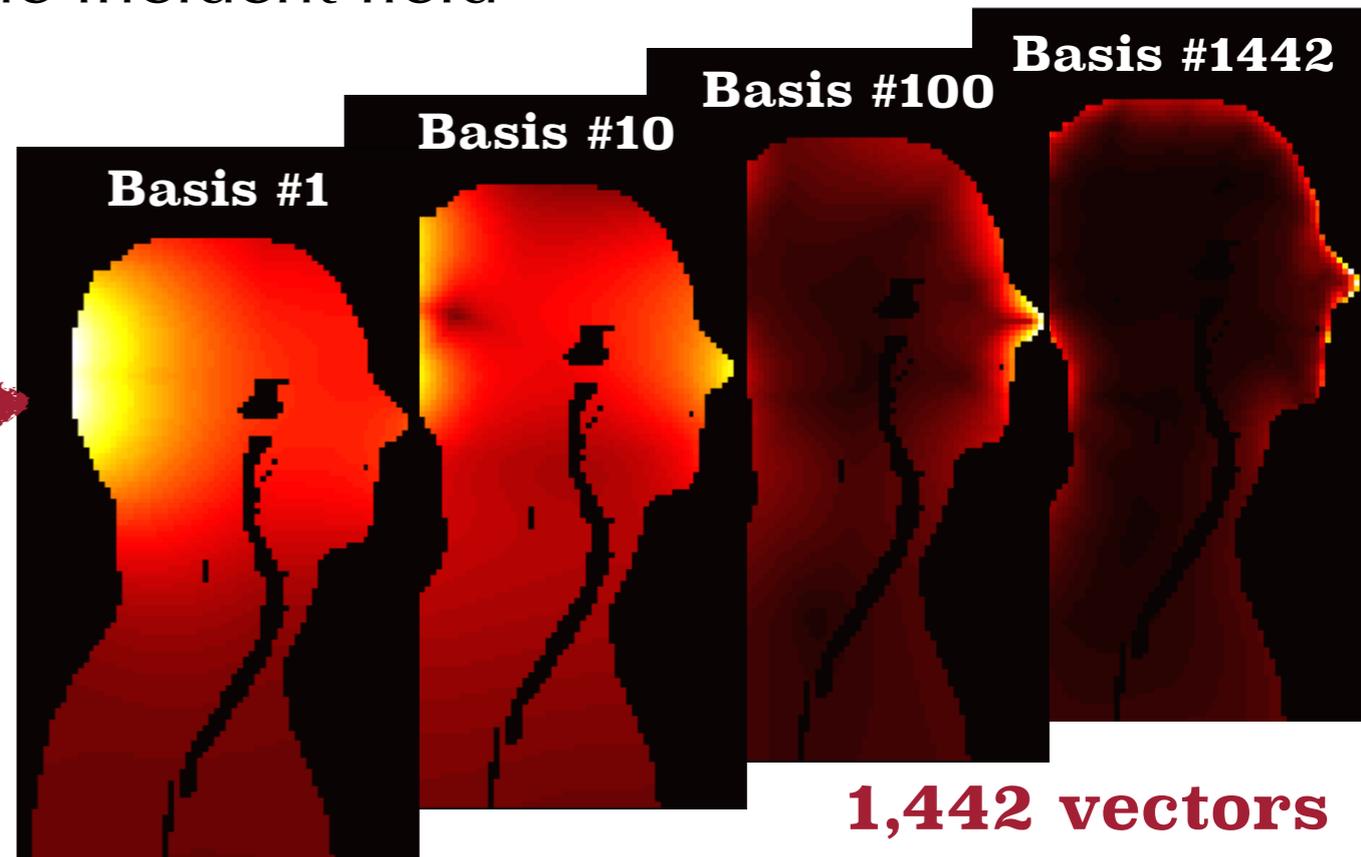
4,000 random excitations

- ◆ **Magnetic Resonance Green Function: Pre-computation**
 - ◆ Generate a compressed basis for the incident field



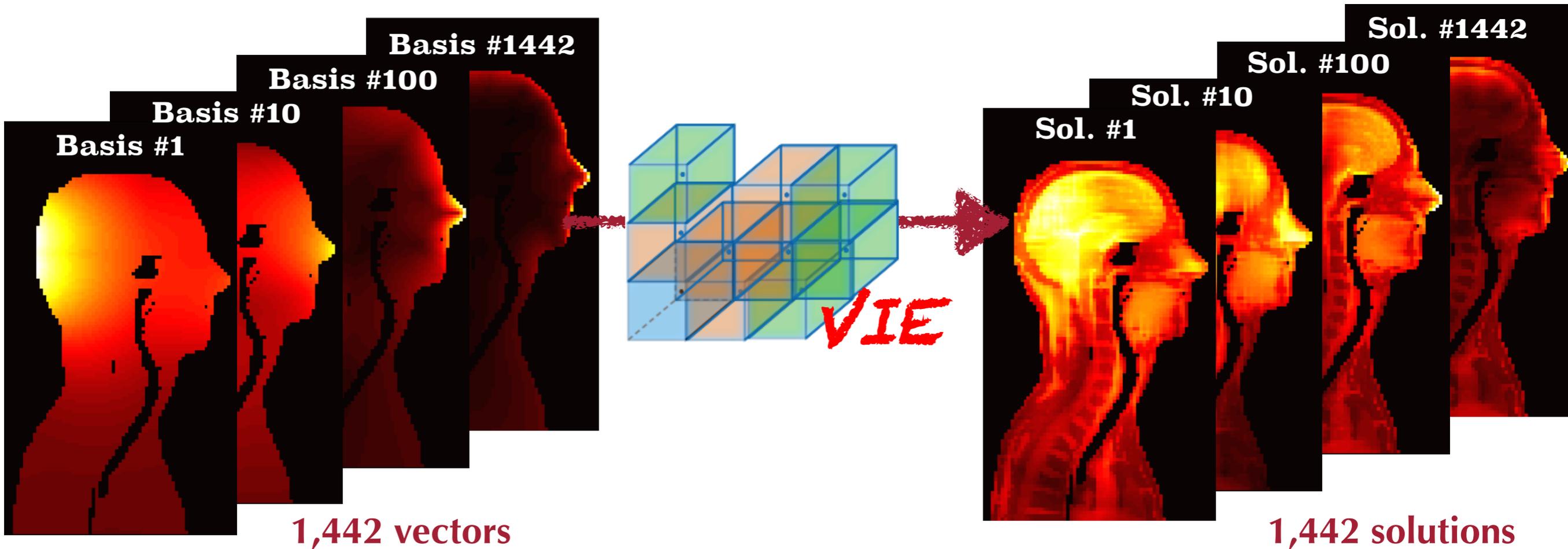
4,000 incident fields

RSVD →

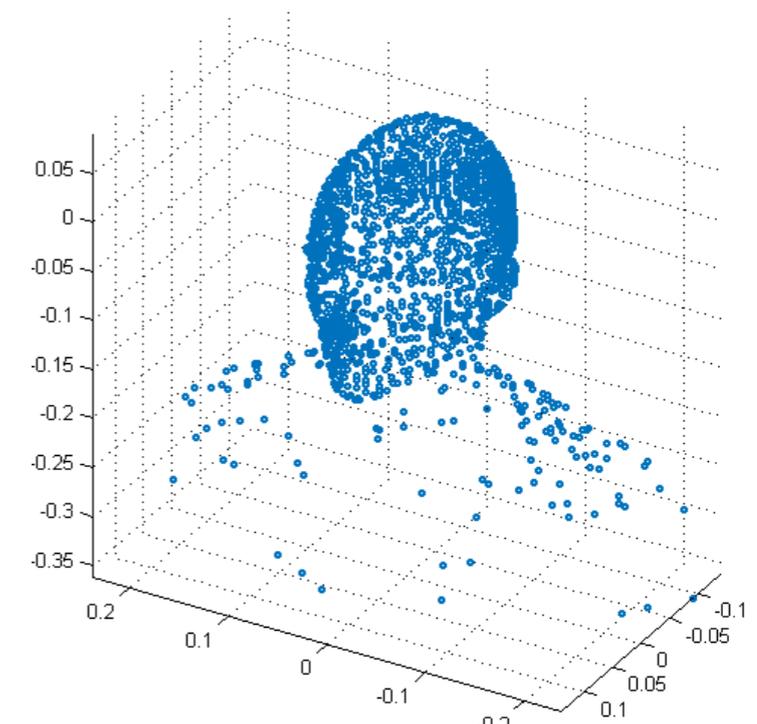


1,442 vectors

- ◆ **Magnetic Resonance Green Function: Pre-computation**
 - ◆ Solve for each vector of the basis



- ◆ **Magnetic Resonance Green Function: Pre-computation**
 - ◆ Generate a reduced set of interpolation points

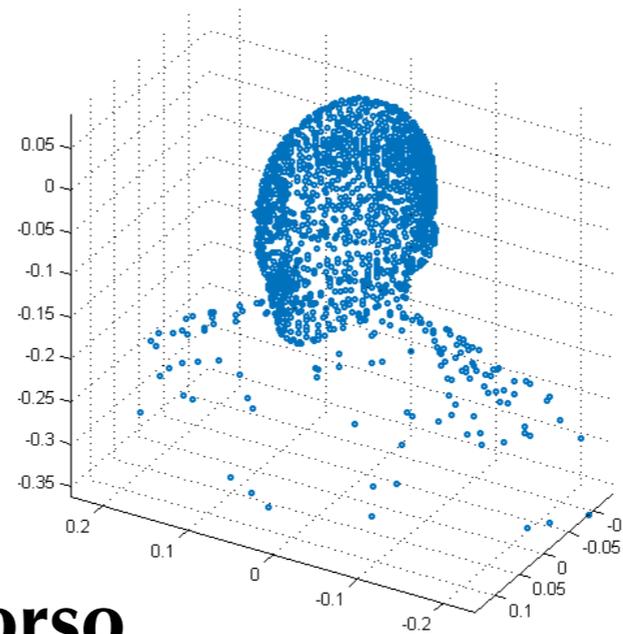


1,609 interpolation points

- ◆ **Magnetic Resonance Green Function**

- ◆ Set of interpolation points in the body
- ◆ Some pre-computed matrices

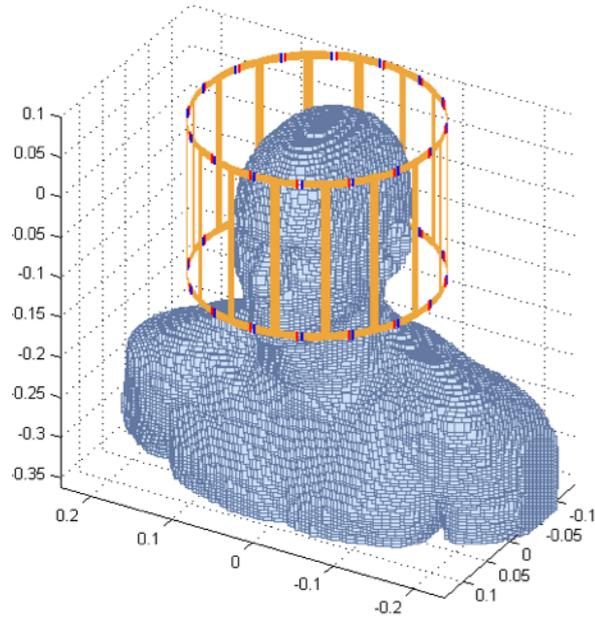
MRGF



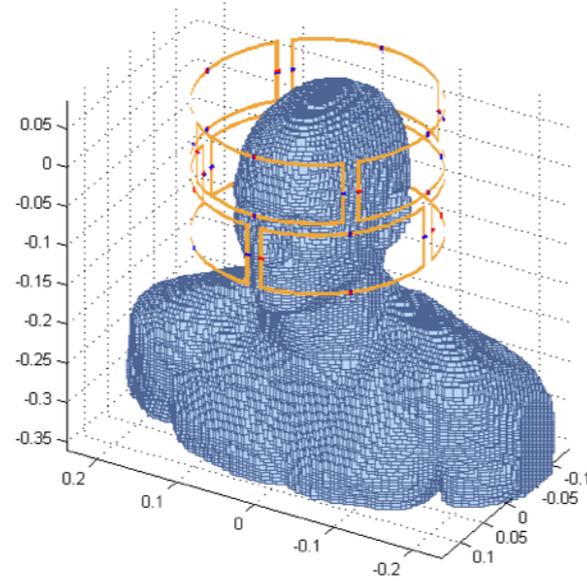
- ◆ **For 4mm DUKE 7T, head and torso**

- ◆ **1609 DEIM points** (initially 266019 voxels)
- ◆ **1442 basis vectors** (from 4000 excitations on 189000 dipoles)
- ◆ Elapsed time **31 h 32 min** (**ONE TIME** for a given model)
- ◆ **~16GB** storage

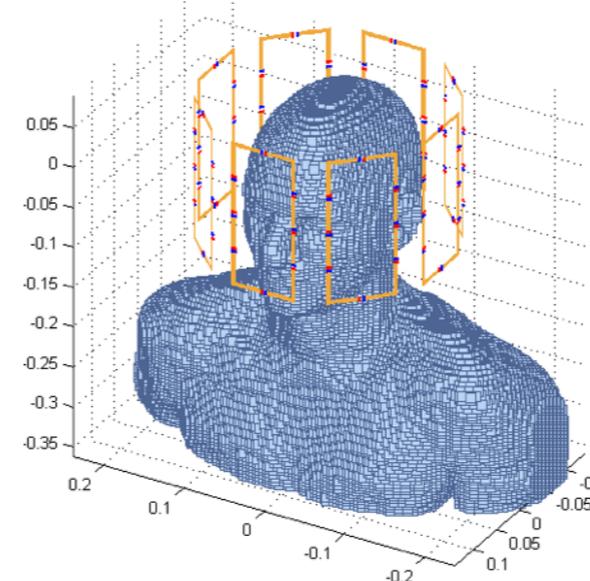
Full wave EM Integral Equation Solver



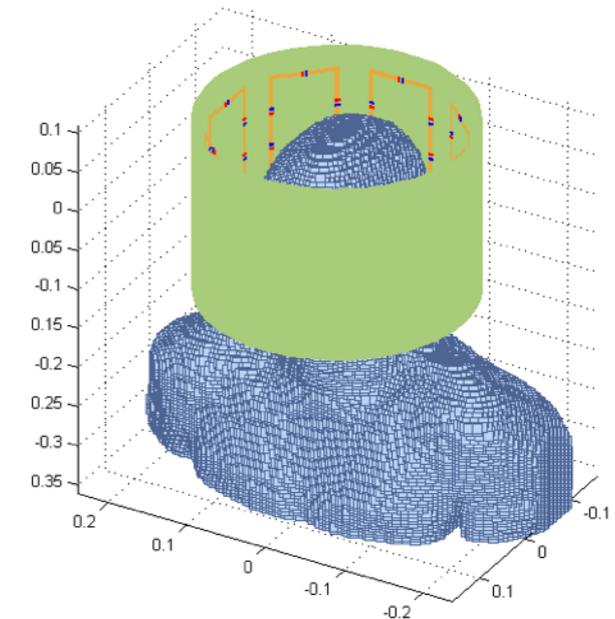
~8h29m overall
(~18 min/port)



~7h30m overall
(~17 min/port)



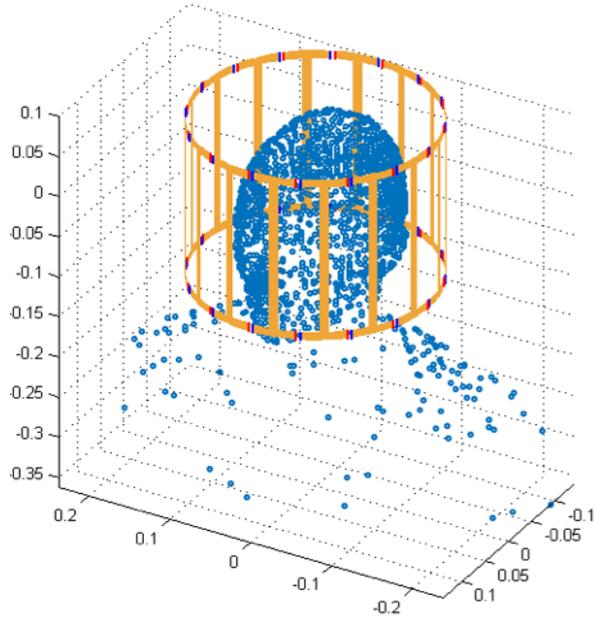
~9h32m overall
(~15 min/port)



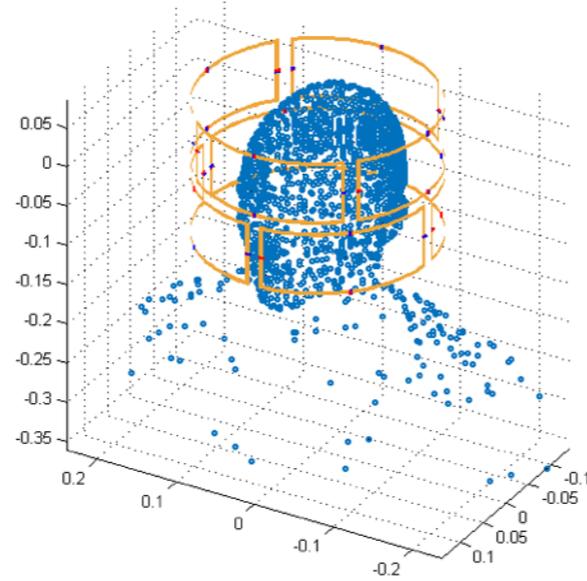
~17h13m overall
(~30 min/port)

MRGF

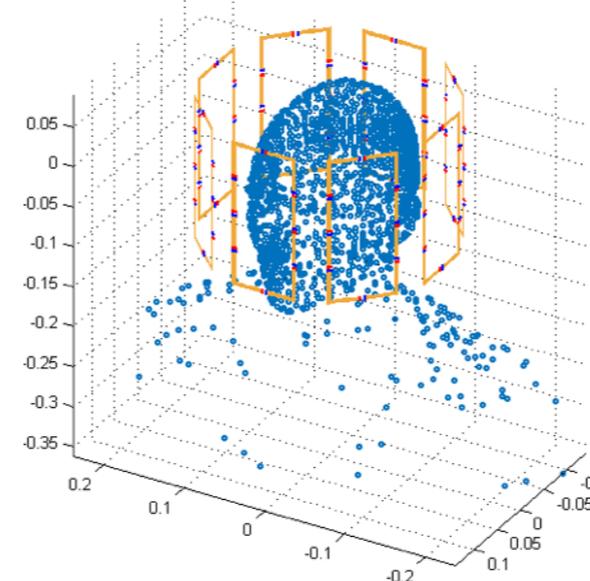
Accelerated Full wave EM Integral Equation Solver



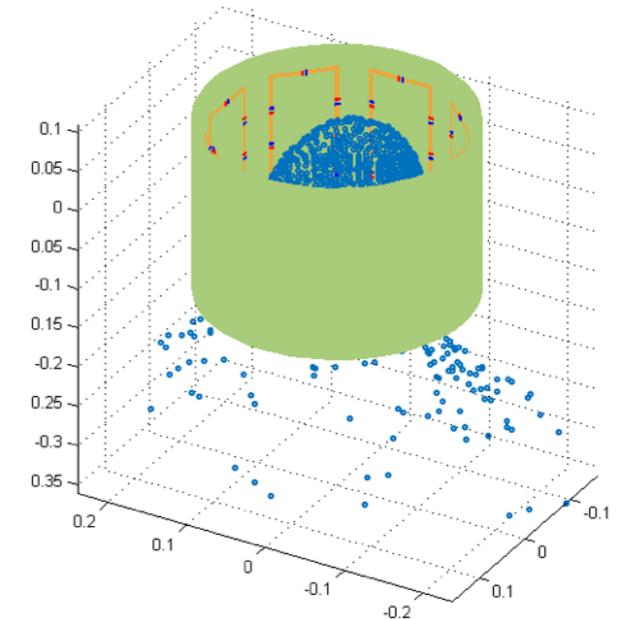
~8h29m overall
(~18 min/port)



~7h30m overall
(~17 min/port)



~9h32m overall
(~15 min/port)



~17h13m overall
(~30 min/port)



~1min overall



~2min overall



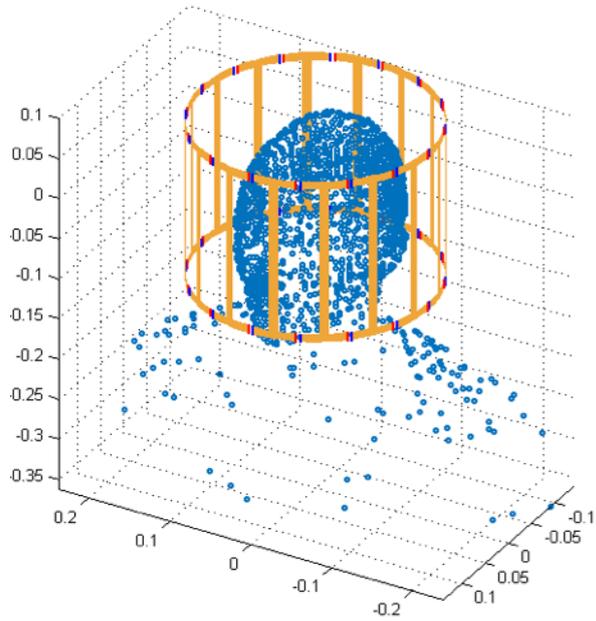
~2min overall



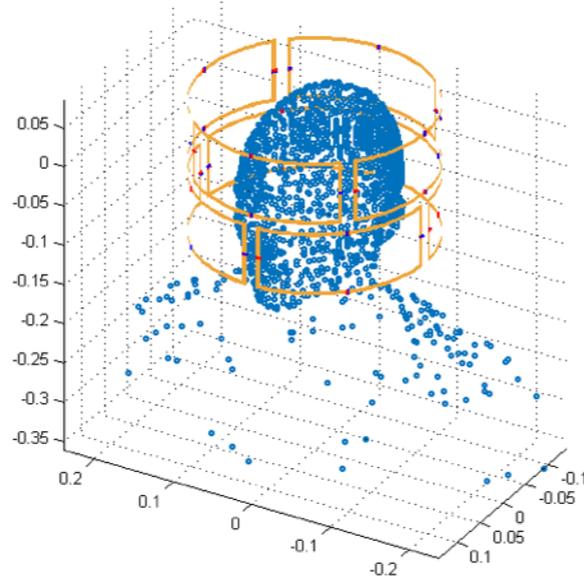
~7min overall

MRGF

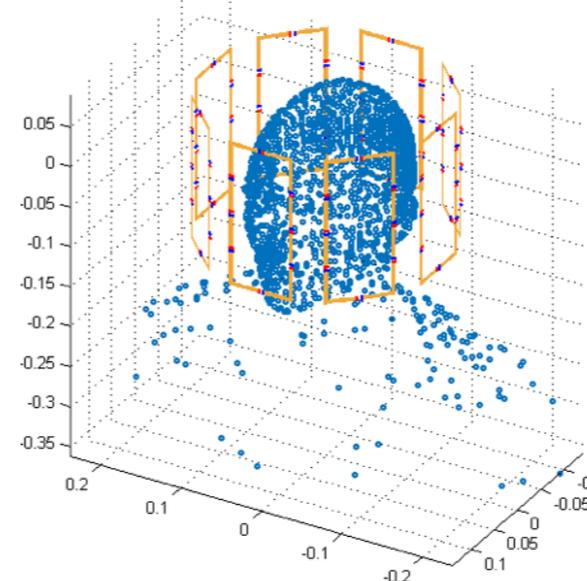
**Accelerated Full wave EM
Integral Equation Solver**



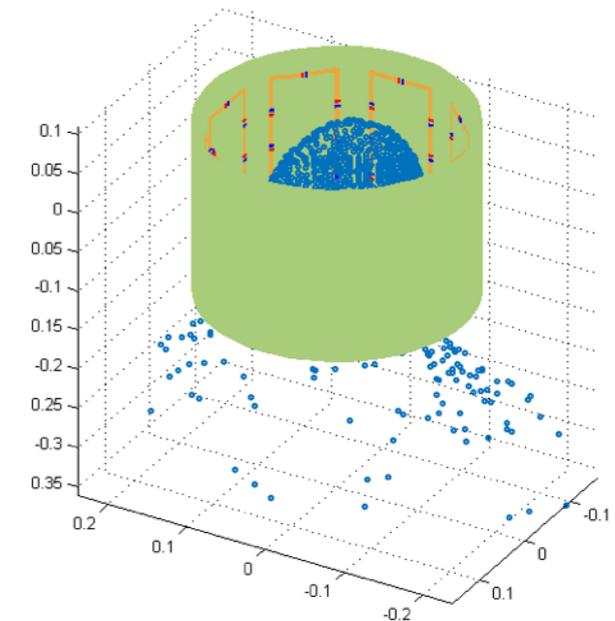
~8h29m overall
(~18 min/port)



~7h30m overall
(~17 min/port)



~9h32m overall
(~15 min/port)



~17h13m overall
(~30 min/port)

~462X

~230X

~298X

~154X

~1min overall

~2min overall

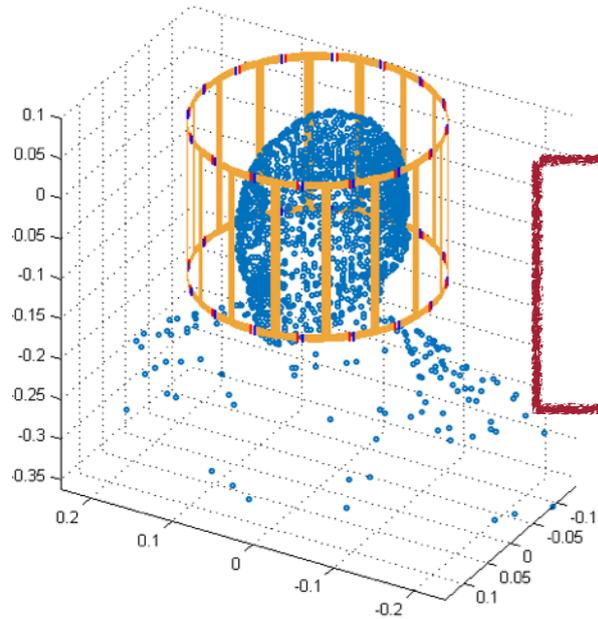
~2min overall

~7min overall

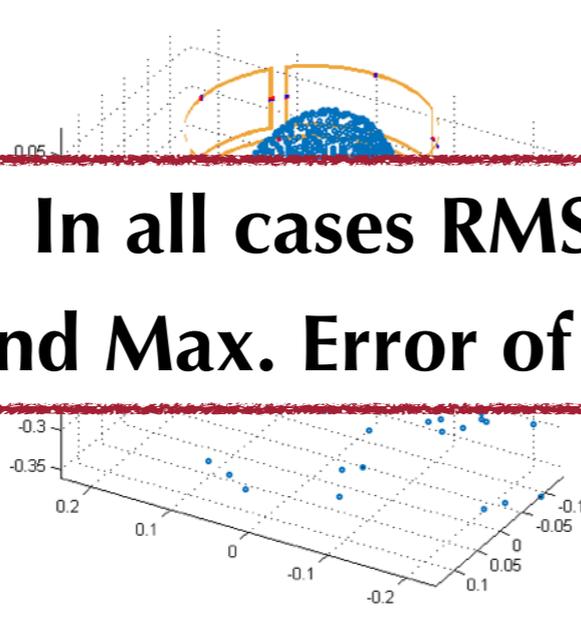
MRGF

Accelerated Full wave EM
Integral Equation Solver

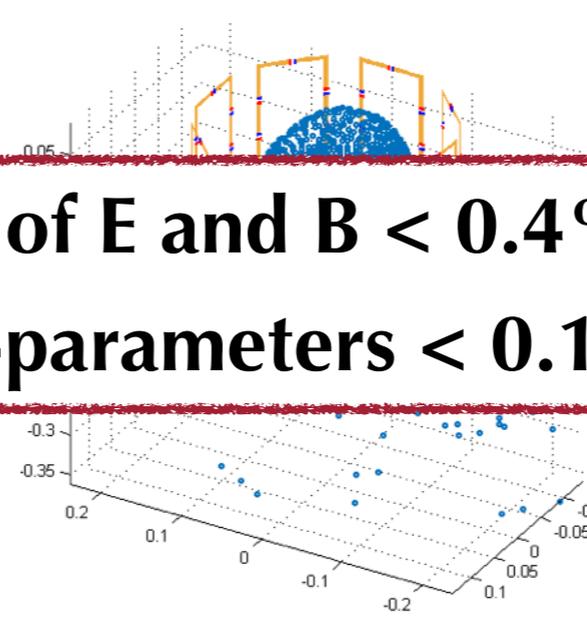
In all cases RMSE of E and B < 0.4%
and Max. Error of S-parameters < 0.17%



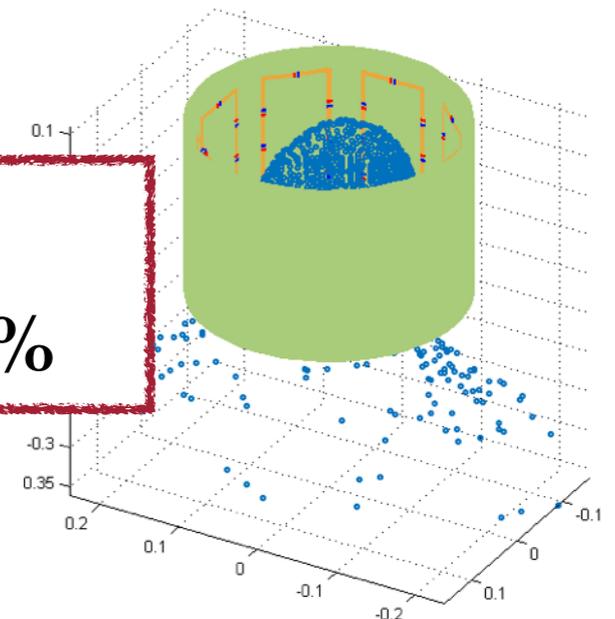
~8h29m overall
(~18 min/port)



~7h30m overall
(~17 min/port)



~9h32m overall
(~15 min/port)



~17h13m overall
(~30 min/port)

~462X

~230X

~298X

~154X

~1min overall

~2min overall

~2min overall

~7min overall

- ◆ **By applying MRI customized simulation tools**
 - ◆ Domain decomposition and Integral Equation solvers
 - ◆ Slow **Off-Line** stage model pre-computation
 - ◆ Can be done for multiple models and frequencies
 - ◆ Fast **On-Line** stage model use
- ◆ **we can analyze a wide variety of coil array designs**
 - ◆ S-parameter matrix (with body)
 - ◆ Body E and B field distribution
 - ◆ **within minutes**
- ◆ **Enable technology for optimal coil design?**

- ♦ **J. Fernández Villena et al,**
"Fast Electromagnetic Analysis of MRI Transmit RF Coils based on Accelerated Integral Equation Methods",
submitted to Physics in Medicine and Biology.

- ♦ **A. Hochman et al,**
"Reduced-Order Models for Electromagnetic Scattering Problems",
IEEE Transactions on Antennas and Propagation, 2014

- ♦ **A. Polimeridis et al,**
"Stable FFT-JVIE solvers for fast analysis of highly inhomogeneous dielectric objects",
Journal of Computational Physics, 2014.

- ♦ **SUPPORT:**
 - ♦ MIT Skoltech initiative
 - ♦ National Institute of Health
 - ♦ National Swiss Foundation

- ♦ **Contact:** jvillena@mit.edu <http://web.mit.edu/jvillena/www>